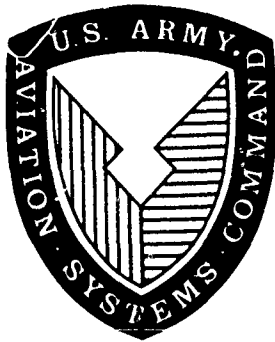


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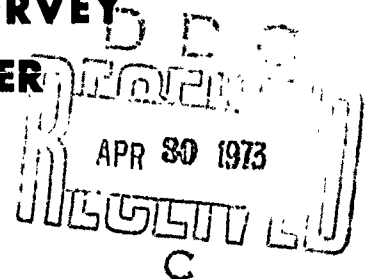
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RDTE PROJECT NO.
AVSCOM PROJECT NO. 70-15-2
USAASTA PROJECT NO. 70-15-2

VIBRATION AND TEMPERATURE SURVEY PRODUCTION UH-1H HELICOPTER

FINAL REPORT



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JANUARY 1973

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UNITED STATES ARMY AVIATION SYSTEMS TEST ACTIVITY
EDWARDS AIR FORCE BASE, CALIFORNIA 93523

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ABSTRACT

Vibration and temperature measurement tests were conducted on a production UH-1H helicopter to define the vibration and temperature environment for instruments, avionics, pilot station, and other component parts during firing and nonfiring flight. Testing was performed by the United States Army Aviation Systems Test Activity, Edwards Air Force Base, California, between 24 March and 16 June 1972. The testing consisted of 19 flights totaling 20 productive testing hours. Vibration data were recorded from 49 accelerometer locations for 55 flight conditions, and narrow-band spectral analyses were performed on the vibration data. The results of the spectral analyses were summarized by use of statistical methods. The primary source of low-frequency vibrations was the main rotor. Gunfire-induced vibrations were less than main rotor-induced vibrations. The highest vibration levels were recorded at the 42-degree gearbox and gear mesh frequencies. There were three shortcomings: amplification of main rotor-induced vibrations by avionics vibration isolation mounts, pilot station vibrations in excess of the military specification limits, and excessively high Wet Bulb Globe Temperature index at the pilot station under certain environmental conditions.



FOREWORD

The United States Army Air Mobility Research and Development Laboratory, Eustis Directorate, Fort Eustis, Virginia, provided data reduction technical support through a contract with Northrop Corporation, Electronics Division, Palos Verdes Peninsula, California. The United States Army Air Mobility Research and Development Laboratory also provided instrumentation installation, calibration, and maintenance support. The dental work required to construct the pilot's bite block was provided by the Air Force Flight Test Center Dental Laboratory, Edwards Air Force Base, California. Wet Bulb Globe Temperature measurement equipment was obtained from the United States Army Medical Equipment Research and Development Laboratory, Fort Totten, New York. Technical advice on the measurement of pilot vibrations was obtained from the United States Army Aeromedical Research Laboratory, Fort Rucker, Alabama.

TABLE OF CONTENTS

	<u>Page</u>
INTRODUCTION	
Background	1
Test Objective	1
Description	1
Scope of Test	2
Methods of Test	2
Chronology	4
RESULTS AND DISCUSSION	
General	5
Vibration Data	5
Data Relevancy	5
Data Presentation	6
Instruments and Avionics Vibration	11
Comparison with the Military Standard	11
Isolation Mount Characteristics	13
Pilot Station Vibrations	13
Selected Component Vibration Characteristics	19
Comparison with OH-58A Test Data	19
Temperature Data	19
Component Air Temperatures	19
Wet Bulb Globe Temperature Index	20
CONCLUSIONS	
General	24
Shortcomings Affecting Mission Accomplishment	25
RECOMMENDATIONS	26

Page

APPENDIXES

A. References	27
B. General Aircraft Information	28
C. Test Configurations	33
D. Test Instrumentation	37
E. Instrumentation Photographs	43
F. Data Reduction Methods	66
G. Test Data	74
H. Helicopter Vibration Sources	127

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INTRODUCTION

BACKGROUND

1. The failure rates of helicopter components such as instruments, avionics, gearboxes, bearings, pumps, etc., have reduced mission accomplishment and have increased the logistic support effort required to keep Army helicopters at the necessary level of operational capability. It is suspected that many component failures result from an excessive vibration and temperature environment and that the helicopter vibration and temperature environment may degrade pilot performance. However, there are insufficient data available to verify these suspicions. To obtain the data necessary to define the vibration and temperature environment of helicopter components and the pilot station, the United States Army Aviation Systems Test Activity (USAASTA) was directed (ref 1, app A) by the United States Army Aviation Systems Command (AVSCOM) to conduct a vibration and temperature survey on present-day Army helicopters.

2. This report on the UH-1H helicopter is the second of a planned series of seven reports which will define the vibration and temperature environment of the OH-58A (ref 2, app A), UH-1H, CH-54B, OH-6A, CH-47C, AH-1G, and UH-1C helicopters.

TEST OBJECTIVE

3. The objective of the entire environmental test project is to determine a representative vibration and temperature environment for all present-day Army helicopters. The objective of the UH-1H environmental survey was to determine the vibration and temperature environment of the UH-1H instruments, avionics, selected components, and the pilot station under all normal operating conditions.

DESCRIPTION

4. The UH-1H is a gas turbine-powered utility helicopter with a maximum gross weight of 9500 pounds. The single main rotor is of the two-bladed, semirigid, teetering type. The tail rotor is also of the two-bladed, semirigid, teetering type with delta-three coupling. The cockpit provides side-by-side seating for a crew of two (pilot and copilot) and the aft compartment has provisions for up to 11 passengers or cargo. The cyclic, collective, and pedal controls are hydraulically boosted and irreversible. The main landing gear is of the fixed, energy-absorbing skid type and the helicopter is powered by a single Lycoming T53-L-13 free gas turbine engine rated at 1400 shaft horsepower (shp) at sea-level, standard-day, uninstalled conditions. The engine is derated to 1100 shp due to the maximum torque limit of the main transmission. The helicopter may be armed with the M23 armament subsystem (two flexible door-mounted 7.62mm M60D machine guns)

or the XM59 armament subsystem (one flexible door-mounted 7.62mm M60D machine gun and one flexible door-mounted 50-caliber AN-M2 machine gun). The approximate rate of fire of the M60D machine gun is 500 rounds per minute and the approximate rate of fire of the AN-M2 machine gun is 700 rounds per minute. The instruments are rigidly mounted to the fuselage. Selected avionics items are mounted on vibration isolators. Detailed aircraft, flight instruments, and avionics information may be found in appendix B and in the operator's manual (ref 3, app A).

SCOPE OF TEST

5. Vibration data were recorded during steady flight, maneuvering flight, and weapons-firing flight from 43 triaxial accelerometer locations, 5 biaxial accelerometer locations, and 1 uniaxial accelerometer location for 55 flight conditions. Three configurations were tested: light weight, 7000 pounds; heavy weight, 9000 pounds; armed, M23 armament subsystem. For the heavy-weight configuration, ballast was distributed to simulate a troop loading. The flight conditions and configurations tested are listed in table 1 and appendix C, respectively. Temperature data were recorded at 20 locations in flight and during static hot soaks in the sun. The nose of the helicopter was pointed toward the sun for all temperature measurements. The accelerometer and thermocouple locations are described in appendix D and photographs of these locations are presented in appendix E. A total of 19 flights were conducted, consisting of 20 productive testing hours, at Edwards Air Force Base, California. A comparison with selected OH-58A vibration data was made. The flight restrictions and operating limitations observed during this evaluation were as specified in the operator's manual (ref 3, app A). The flight conditions and configurations which will be used for future helicopter environmental testing are contained in the test plan (ref 4).

METHODS OF TEST

6. The test UH-1H helicopter (S/N 67-17145) was instrumented to record vibration data on a frequency multiplexed-frequency modulated (FM-FM) magnetic tape system. One hundred forty channels of acceleration vibration data were recorded from accelerometers mounted on the instrument panel, avionics, pilot station, and other selected components. The instrumentation was limited to recording data from 12 accelerometers simultaneously with eight manual switching groups. This switching enabled a total of 96 channels of vibration data to be recorded for each flight condition by repeating each flight condition seven times. To record the total of 140 channels, the accelerometers were relocated and all flight conditions were repeated eight more times. Twenty channels of temperature data were hand-recorded from a single temperature display by manually switching to the desired temperature pickup. The parameters required to define the flight condition were hand-recorded from calibrated ship's standard instruments.

Table 1. UH-1H Vibration Test Conditions.¹

Test	Conditions	Average Gross Weight (lb)	Configuration	Average Density Altitude (ft)	Average Temperature (~ °C)
Hover	In ground effect, out of ground effect			3300	18
Level flight	V_H (122 KCAS) ² , $0.9V_H$, $0.9V_H$, $0.7V_H$, V_{loiter} (60 KCAS); 7000-lb GW	7000 and 9000	Clean (doors closed)	5000	11
	V_H (102 KCAS), $0.9V_H$, $0.8V_H$, $0.7V_H$, V_{loiter} (60 KCAS); 9000-lb GW				
Climb	$V_{best R/C}$ (55 KCAS), 7000-lb GW; $V_{best R/C}$ (60 KCAS), 9000-lb GW; maximum power			5000	11
	$V_{cruise R/C}$ (80 KCAS), 7000-lb and 9000-lb GW, maximum power				
Descent	$V_{min R/D}$ (49 KCAS), 7000-lb GW; $V_{min R/D}$ (55 KCAS), 9000-lb GW; minimum power			5000	11
	$V_{cruise R/D}$ (80 KCAS), 500 ft/min				
	Normal (A), level acceleration (B); from 3-ft hover				
Takeoff (T/O)	Normal (A), steep (B), shallow (C); to 3-ft hover			3300	15
Landing (LDG)	90° turns at constant altitude; 15°, 30°, and 45° bank angle, right and left; 100 KCAS entry airspeed			3300	15
Maneuvering flight	Flight idle (324 rpm), ground idle (220 rpm), wind speed 15 to 20 knots			5000	12
Ground run	Right gun fwd, mid, aft; left gun fwd, mid, aft; both guns fwd, mid, aft; 80 KCAS			2700	14
Weapons firing		8100	Armed (doors open) M23 armament subsystem	4700	17

¹Coordinated flight maintained at level flight, climb, descent, and maneuvering flight test conditions.

²Knots calibrated airspeed.

7. A total of 7837 vibration data records were recorded and narrow-band spectral analyses were performed on 7544 of these data records. To present the results of the spectral analysis in a form which could be more easily comprehended than the 7544 spectral analysis plots, a statistical method of summarizing the data on a digital computer (referred to as data compression) was developed. The data were compressed by selecting groups of the 7544 spectral analysis plots and summarizing each of these groups in two compressed data plots. These two compressed data plots show the maximum acceleration and the mean plus 3-standard-deviation (3-sigma) acceleration with the mean acceleration in the form of a frequency spectrum similar to the individual spectral analysis plots. The mean plus 3-sigma acceleration value is that acceleration below which 99.87 percent of all data recorded fell. Data compression was accomplished by taking the acceleration value at each of the 500 frequencies which were output by the spectral analyzer for all spectral analysis plots in a compression group and finding the maximum and minimum acceleration, the mean acceleration, and the mean plus 3-sigma acceleration. With the data compression plots which present the maximum acceleration values, a table is provided which lists the flight condition, accelerometer location, and axis at which each maximum acceleration occurred. The equations used to calculate the mean and standard deviation and a block diagram of the spectral analysis and data compression systems are presented in appendix F.

8. The flight conditions selected for the vibration testing were intended to cover all normal flight conditions encountered in operational use of the UH-1H helicopter. The first pass of the data compression grouped the data according to flight condition. The second and third data compression passes combined all of the flight conditions in proportion to the number of columns each flight condition occupies in the data array (figs. 1 through 3, app G). For example, landings comprise 6 out of 46 nonfiring columns or 13 percent of the data which, in the compressions that combine flight conditions, represents a flight during which 13 percent of the flight time is spent in landings. The first-pass data compressions may be used to combine flight conditions in any proportion desired.

CHRONOLOGY

9. The chronology of testing was as follows:

Test request received	14	September	1970
Test aircraft available	12	January	1972
Test flying initiated	24	March	1972
Test flying completed	9	June	1972

RESULTS AND DISCUSSIONS

GENERAL

10. The UH-1H instruments and avionics nonfiring vibrations were found to be primarily sinusoidal with a random variation of amplitude with time at each discrete frequency at steady flight conditions. The primary source of low-frequency vibrations was the main rotor, with a maximum mean plus 3-standard-deviation (3-sigma) vibration acceleration value of 0.94g at the main rotor six-per-rotor-revolution (6/rev) frequency of 32.4 hertz (Hz). Instruments and avionics vibrations during firing were primarily broadband with little discrete frequency content. Gunfire-induced vibrations were less than main rotor-induced vibrations with a maximum mean plus 3-sigma vibration acceleration value of 0.24g at 466 Hz. The pilot seat pad did not attenuate vibrations in the frequency range of main rotor-induced vibrations; however, the pilot's body attenuated vibrations above 10 Hz. Pilot station vibrations were more objectionable at 7.3 Hz (main rotor 2/rev frequency at ground idle) than at 32.4 Hz at equal amplitudes and exceeded the limits of military specification MIL-H-8501A. Instrument and avionics vibration levels were well below the laboratory qualification vibration levels of MIL-STD-810B. The main rotor-induced vibrations in the OH-58A and UH-1H helicopters reached their highest levels at the main rotor 4/rev and 6/rev frequencies in both helicopters. However, the magnitude of the UH-1H main rotor-induced vibrations was about twice that of the OH-58A main rotor-induced vibrations. The maximum mean plus 3-sigma vibration acceleration level for all locations tested was 44g at 1920 Hz at the 42-degree gearbox. The highest instrument and avionics temperatures were recorded in the forward cabin area under static conditions and decreased in forward flight. Under certain environmental conditions, the Wet Bulb Globe Temperature (WBGT) index is excessively high at the pilot station. The results of this test project indicate the following: Data in this and previous environmental test reports could be applied to revising the appropriate military environmental specifications; improved vibration isolation methods should be developed; consideration should be given to specifying the pilot station vibration limits in MIL-H-8501A as a function of frequency below 32 Hz; consideration should be given to use of a seat cushion to attenuate main rotor vibrations; and consideration should be given to installing an environmental control system for use in extreme environmental conditions.

VIBRATION DATA

Data Relevancy

11. Qualitative pilot evaluation indicates that there is a wide variation in the vibration level of different helicopters of the same model due to differences in the mechanical condition of each helicopter. Thus, if vibration levels are to be measured which are representative of those encountered in a particular model of

helicopter, then a sample of several units of this model of helicopter must be tested. All of the data in this report are from one UH-1H helicopter, S/N 67-17145, which was obtained from Bell Helicopter Company (BHC) by USAASTA with 530 flight hours and accumulated 120 additional flight hours at USAASTA before this vibration test was conducted. It is not known what the vibration level of a UH-1H with a similar number of hours in hard operational use would be; however, it is probable that there are UH-1H helicopters with higher vibration levels than the helicopter tested.

Data Presentation

12. The data were summarized in three data compression passes and in 8 transmissibility compressions. Each data compression is presented as two plots: maximum acceleration recorded versus frequency, and mean with mean plus 3-sigma acceleration versus frequency. The mean plus 3-sigma acceleration values are felt to best represent the test data, since accelerations in excess of the mean plus 3-sigma limit were recorded less than 0.13 percent of the time. This result indicates that accelerations in excess of the mean plus 3-sigma limit would be only rarely encountered in operational use of the helicopter. The data grouping used in each compression pass is summarized in table 2, with details of the data compression shown in the data arrays - figures 1, 2, and 3, appendix G. In the data array, each square represents a spectral analysis data point. The numbers assigned to each group of squares in the data array represent a compression group, with squares with like numbers belonging to the same compression group. This compression group number is written on each compressed data plot for identification. The transmissibility compressions combine all axes and nonfiring flight conditions for the input and output accelerometer locations of interest. The specific locations compressed are indicated on each transmissibility plot.

13. The instrument and avionics nonfiring third-pass compression results are presented in table 3 and in figures A and B in the body of this report. The instruments and avionics third-pass firing compression results are presented in figures 40 and 41, appendix G. The second-pass nonfiring compressions and the first-pass firing compressions are presented in appendix G for all accelerometer locations. Only the instruments, avionics, and pilot station compressions are presented in appendix G for the first-pass nonfiring conditions. The first-pass compressions for the other locations are available from USAASTA. For the first-pass firing and second and third compression passes nonfiring, a table is presented with the plot of the maximum accelerations which lists the accelerometer location, axes, and flight condition at which each significant peak occurred. For the nonfiring third-pass compression, this table is expanded to include the source of the significant accelerations. The acceleration values which are presented in this report are one-half of the peak-to-peak value. The individual spectral analysis data, on digital magnetic tape, are available from USAASTA.

Table 2. Data Compression Grouping.

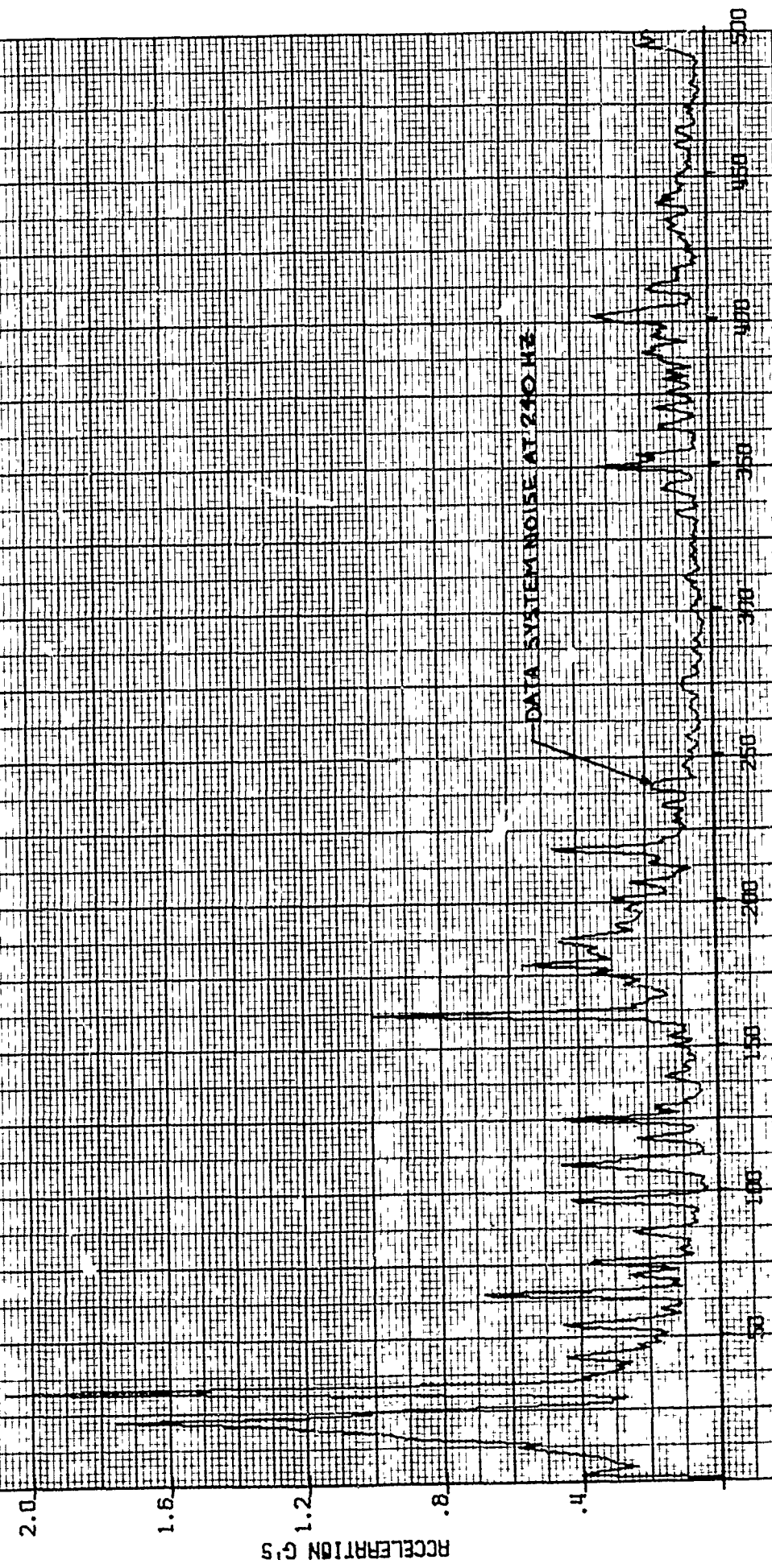
Compression Pass	Group ¹	Group Elements (location number)	Number of Group Elements	Number of Compressions
1st	Equipment	Instrument panel (1, 2, 3, 4, 5) Avionics equipment (6, 7, 8, 9, 10) Pilot input (11, 12, 13, 14, 15) Pilot output (16, 17) Transmission mounts (18, 19, 20, 21) Tail boom attach points (22, 23) Engine deck (24, 25) Engine firewall (26, 27) Engine mounts (28, 29, 44) Tail rotor servo (30) Oil cooler (31) 42° and 90° gearboxes (32, 33) Hydraulic servo (34) Fuel boost pumps (35, 45) Tach generators (36, 37, 38) Hanger bearings (39, 40, 41, 42) Engine (46, 47, 48) Lift link (43) Gun mount ² (49)	19	145
	Flight conditions ³	Hover Level flight Climb Descent Takeoff and landing Turns Ground run Weapons firing ²	8	
2nd	Equipment	Same as 1st pass with gun mount omitted	18	18
	Flight conditions	All nonfiring	1	
3rd	Equipment	Instruments and avionics (1, 2, 3, 4, 5, 6, 7, 8, 9, 10)	1	2
	Flight conditions	Nonfiring Weapons firing	2	

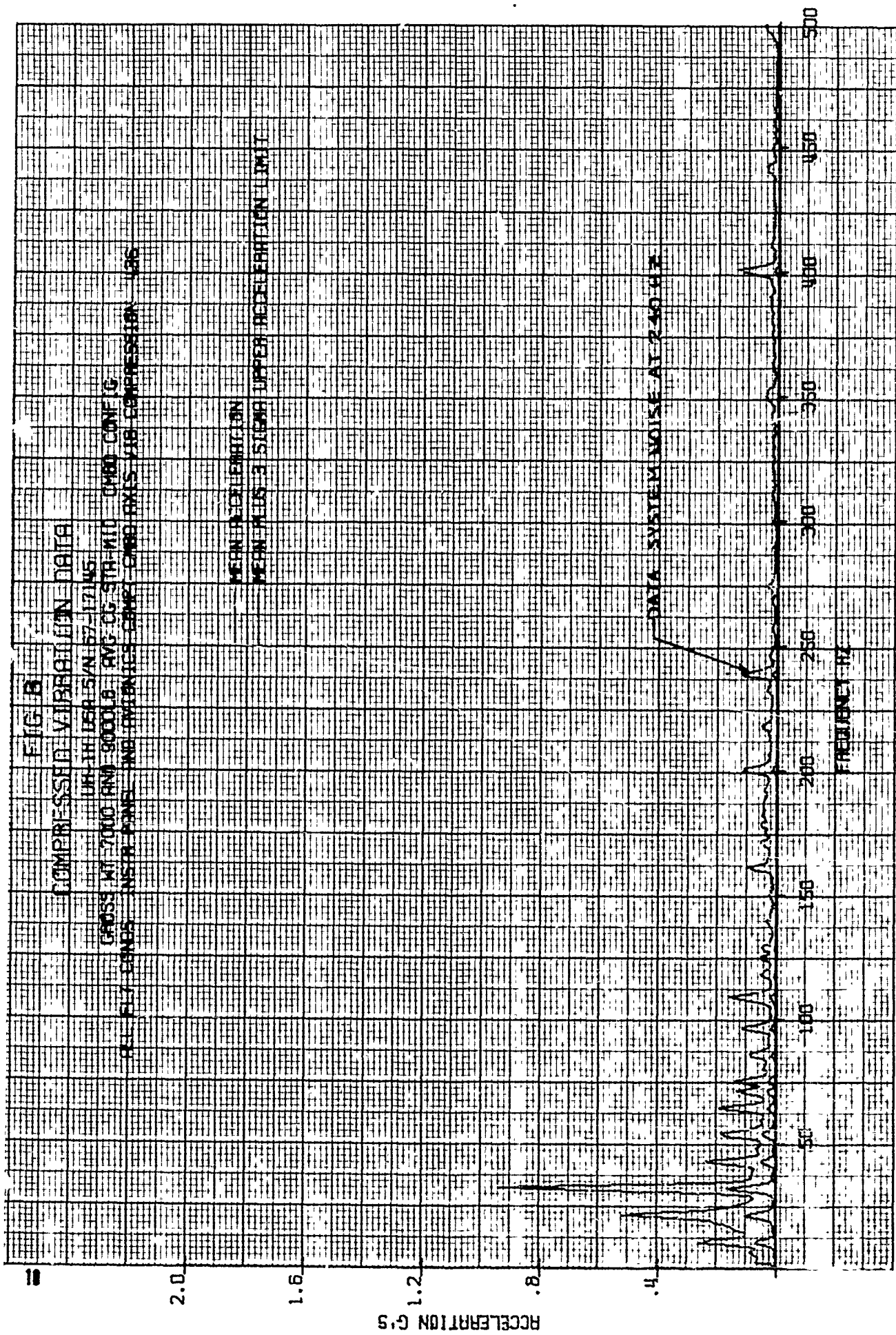
¹All axes combined for all compressions.²Gun mount data presented only for weapons firing.³Flight conditions are described in detail in table 1.

Table 3. UH-1H Vibration Sources.

Main rotor speed: 324 rpm		
Source		Frequency (Hz)
Main rotor	Fundamental	5.4
	2/rev	10.8
	4/rev	21.6
	6/rev	32.4
	8/rev	43.2
	10/rev	54.0
	12/rev	64.8
	14/rev	75.6
Tail rotor	Fundamental	27.6
	2/rev	55.1
	4/rev	110.2
	6/rev	165.3
	8/rev	220.4
	10/rev	275.5
Engine shaft	Fundamental	110
Tail rotor drive shaft		72
Gas producer (100%)		419
Power turbine		351
90-degree gearbox gear mesh		1072
42-degree gearbox gear mesh		1930
Main transmission, second stage		640
Main transmission lower section, drive bevel gear		1857
Main transmission, first stage		1977
Gunfire at 550 rounds/minute	Fundamental	9.2
	1st harmonic	18.3
	2nd harmonic	27.5
	3rd harmonic	36.7
	4th harmonic	45.8
	5th harmonic	55.0
	6th harmonic	64.2
	7th harmonic	73.3
	8th harmonic	82.5
	9th harmonic	91.7
	10th harmonic	100.8

FIG. A
 COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION
 LH-1H DEB 5/N 67-17195
 GROSS WT 2000 AND 3000 LB AVG CG STA-M10 OVER CNF/G
 ALL FLY LINES INSIDE PANEL AND INWARDS COMP CMBD AXES 018 COMPRESSION 125





Instruments and Avionics Vibration

14. Instruments and avionics vibration data were gathered from ten triaxial accelerometer locations at the test conditions shown in table 1. Accelerometer locations are described in detail in table 2, appendix D, and shown in photographs in appendix E. The third-pass data compressions are presented in figures A and B in the body of this report and in figures 40 and 41, appendix G. Second-pass data compressions are presented in figures 4 through 7, appendix G, and first-pass data compressions are presented in figures 80 through 107, appendix G. The data were found to be primarily sinusoidal with a random variation of acceleration amplitude with time at each discrete frequency at steady flight conditions. The random amplitude variation was usually less than 20 to 30 percent of the acceleration amplitude mean value and was apparently due to small changes in variables such as light turbulence or small control inputs. The main rotor was the primary nonfiring vibration source, with the tail rotor, tail rotor drive shaft, and engine also causing significant vibrations. Table 3 lists the primary UH-1H vibration sources and their frequency. A maximum mean plus 3-sigma acceleration value of 0.94g at the main rotor 6/rev frequency of 32.4 Hz was recorded. A peak acceleration value of 2.08g at the main rotor 6/rev frequency was recorded along the longitudinal axis on the lower left portion of the instrument panel (location 2) during a 45-degree bank left turn. Table 4 lists the frequency, flight condition, axis, location, and source of the maximum nonfiring accelerations presented in figure A. A general discussion of helicopter vibration sources is contained in appendix H.

15. The instruments and avionics firing vibration data were broadband with little discrete frequency content. The gunfire-induced vibration levels were lower in amplitude than the nonfiring vibration levels, while the peak amplitudes occurred at higher frequencies. Vibrations at the gunfire fundamental frequency of 9.2 Hz or harmonics of this frequency were not observed. These low-frequency gunfire vibrations may have been concealed by main rotor-induced vibrations which are of similar frequencies. A maximum mean plus 3-sigma gunfire acceleration value of 0.24g at a frequency of 466 Hz was recorded. A peak acceleration value of 0.65g at 209 Hz was recorded along the longitudinal axis in the center of the instrument panel (location 3) with the right door gun firing forward. The majority of the peak accelerations recorded on the forward-mounted instruments and avionics occurred with the door guns firing forward, indicating that the muzzle blast was a significant cause of vibration.

Comparison with the Military Standard

16. Figure C shows a laboratory vibration test curve for equipment installed in helicopters taken from figure 514.1-3 of the military standard, MIL-STD-810B (ref 5, app A). The ordinate is changed from units of vibration amplitude as the curve is presented in MIL-STD-810B to units of vibration acceleration to be compatible with the data presented in this report. The significant mean plus 3-sigma acceleration limits from figure B and figure 40, appendix G, are plotted on this specification curve with previously acquired OH-58A vibration data (ref 2). This

Table 4. Instruments and Avionics Maximum Accelerations for Figure A (Nonfiring).

Frequency (Hz)	Flight Condition ¹	Gross Weight (lb)	Axis ²	Location Number	Amplitude (~ g)	Source
12	LDG B	7000	V	4	0.59	Main rotor 2/rev
22	LDG B	7000	V	5	1.76	Main rotor 4/rev
32	LT 45°	7000	H	2	2.08	Main rotor 6/rev
43	LDG C	7000	V	6	0.45	Main rotor 8/rev
54	LF (V _H)	7000	H	5	0.46	Main rotor 10/rev Tail rotor 2/rev
65	LDG C	7000	H	2	0.68	Main rotor 12/rev
72	LDG B	9000	H	4	0.26	Tail rotor drive shaft
76	LDG C	7000	H	5	0.38	Main rotor 14/rev
86	LDG A	7000	H	5	0.25	Main rotor 16/rev
97	LT 45°	7000	H	2	0.43	Main rotor 18/rev
109	T/O B	9000	V	8	0.46	Main rotor 20 rev Tail rotor 4/rev Engine shaft
125	V _{min} R/D	7000	V	7	0.45	--
151	V _{cruise} R/D	7000	V	7	1.00	--
178	V _{min} R/D	7000	V	7	0.56	--
186	V _{cruise} R/D	7000	V	7	0.45	--
218	V _{min} R/D	7000	V	7	0.47	--
349	V _{min} R/D	9000	V	8	0.33	Power turbine
401	OGE Hover	7000	V	7	0.34	Gas producer

¹Flight condition abbreviations defined in table 1.

²V: vertical.

H: longitudinal.

specification curve does not limit helicopter instrument and avionics vibration levels but gives vibration levels to be used for laboratory qualification of instruments and avionics for helicopter use. A data compression composed of only equipment mounted on isolators was not calculated, since the lower curve of figure C assumes that the vibration isolators will reduce vibrations above a frequency of 33 Hz, which was not the case for the vibration isolators tested. All instruments and avionics mean plus 3-sigma vibration levels are well below the test curve of MIL-STD-810B.

Isolation Mount Characteristics

17. The transmissibility of the isolation mounts on the RT-348/ARC-54 radio and MD-1 vertical gyro was evaluated at the UH-1H driving frequencies. Transmissibility was determined by measuring the input and output accelerations across the isolation mounts and calculating the ratio of output to input acceleration. The input and output accelerations used were those determined from the mean plus 3-sigma compressions of all axes and all nonfiring flight conditions. This ratio is plotted as a data point at each driving frequency in figure D. The results indicate that the isolation mounts significantly amplify UH-1H driving frequencies between 30 Hz and 110 Hz for the RT-348/ARC-54 radio and below 100 Hz for the MD-1 vertical gyro. This amplification is apparently due to isolator resonant frequencies which are near the helicopter driving frequencies. Outside these frequency ranges the isolators were effective in isolating vibration. Several maximum accelerations at particular driving frequencies were recorded on these two isolated items, as shown in figures 7 and 45, appendix G. The amplification of vibrations in this low-frequency range is highly undesirable, since the severest UH-1H instrument and avionics vibrations occur at these low frequencies. Amplification by the vibration isolators is a shortcoming, correction of which is desirable.

Pilot Station Vibrations

18. Pilot station vibrations were measured at the pilot collective grip, cyclic grip, right foot rest, seat structure, seat pad, bite block, and helmet at the conditions shown in table 1. Accelerometer locations are described in detail in table 2, appendix D, and are shown in photographs in appendix E. The second-pass data compressions are presented in figures 8 through 11, appendix G, and the first-pass data compressions are presented in figures 108 through 135. The pilot for which this data were recorded weighed 160 pounds and was 68 inches tall. Forty pounds of ballast was placed on the floor beneath the pilot seat to simulate a 200-pound pilot station loading.

19. The transmissibility of the seat pad was evaluated by calculating the ratio of the seat pad acceleration to the seat structure accelerations at UH-1H driving frequencies. These ratios are plotted in figure E. Seat pad acceleration was measured by attaching an accelerometer to the bottom of a 10-inch by 6-inch by 0.020-inch aluminum plate on which the pilot sat. The accelerations used were those determined from the mean plus 3-sigma compressions of all axes and all nonfiring flight conditions for the seat pad and seat structure. Results indicate that there

FIGURE C-1

LABORATORY VIBRATION TEST CURVES FOR EQUIPMENT INSTALLED IN HELICOPTERS
FROM MIL-STD-810B, FIG 514.1-3

MEAN PLUS 3 SIGMA ACCELERATION, ALL INSTRUMENTS AND
AVIONICS, ALL AXES, ALL CONDITIONS

NOTE: SHADED SYMBOLS DENOTE
WEAPONS FIRING.
OPEN SYMBOLS DENOTE
NON WEAPONS FIRING

SYMBOL
○
□
HELICOPTER
OH-58A
UH-1H

ALL EQUIPMENT WITH MOUNTS
— NORMALLY ISOLATED EQUIPMENT WITHOUT T SOLATORS

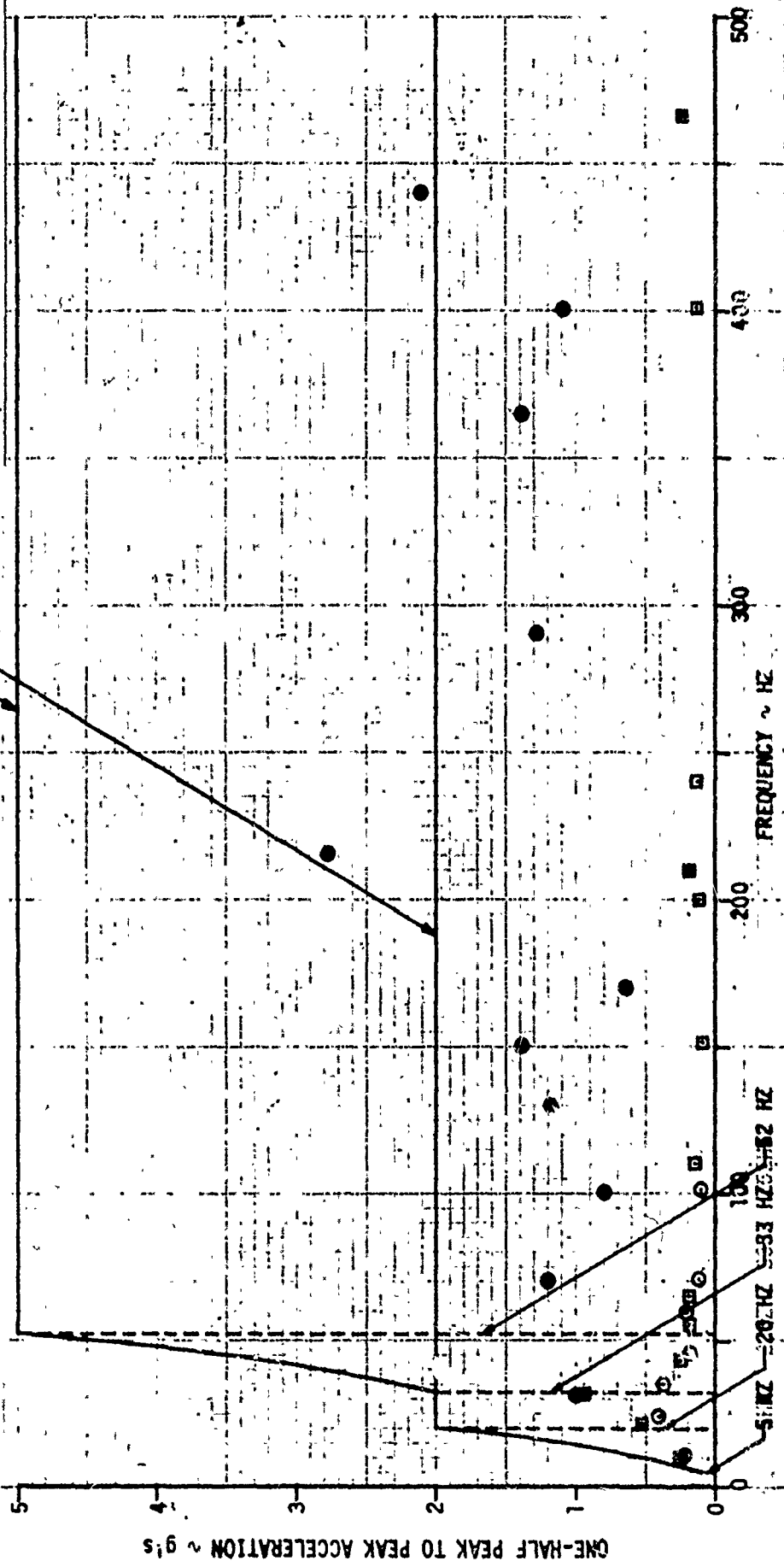
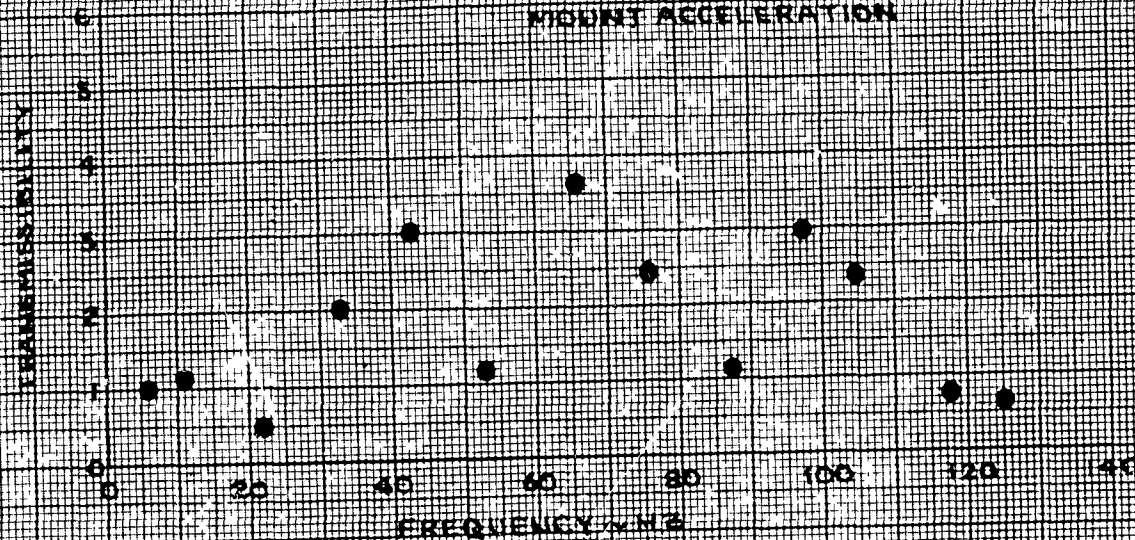


FIGURE D
VIBRATION ISOLATOR TRANSMISSIBILITY
UH-1H USA 3467-17143
ALL AXES, ALL NON-FIRING FLIGHT
CONDITIONS COMBINED

RT-348/ARC-34 RELIEVER-TRANSMITTER

NOTE: TRANSMISSIBILITY IS THE RT-348/ARC-34
ACCELERATION DIVIDED BY THE RT-348/ARC-34
MOUNT ACCELERATION



MD-1 VERTICAL GYRO

NOTE: TRANSMISSIBILITY IS THE MD-1 ACCELERATION
DIVIDED BY THE MD-1 MOUNT ACCELERATION

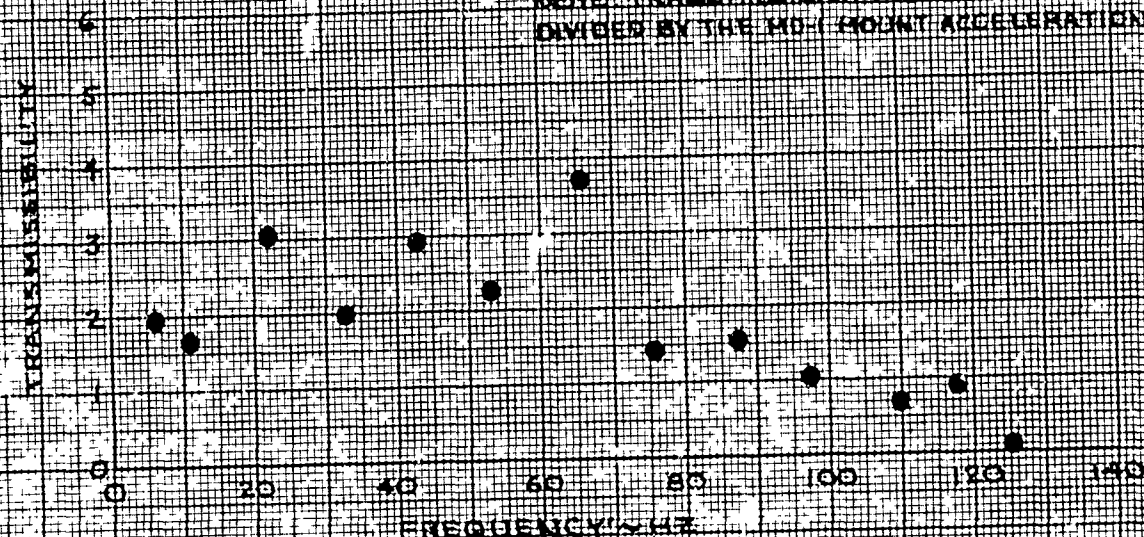
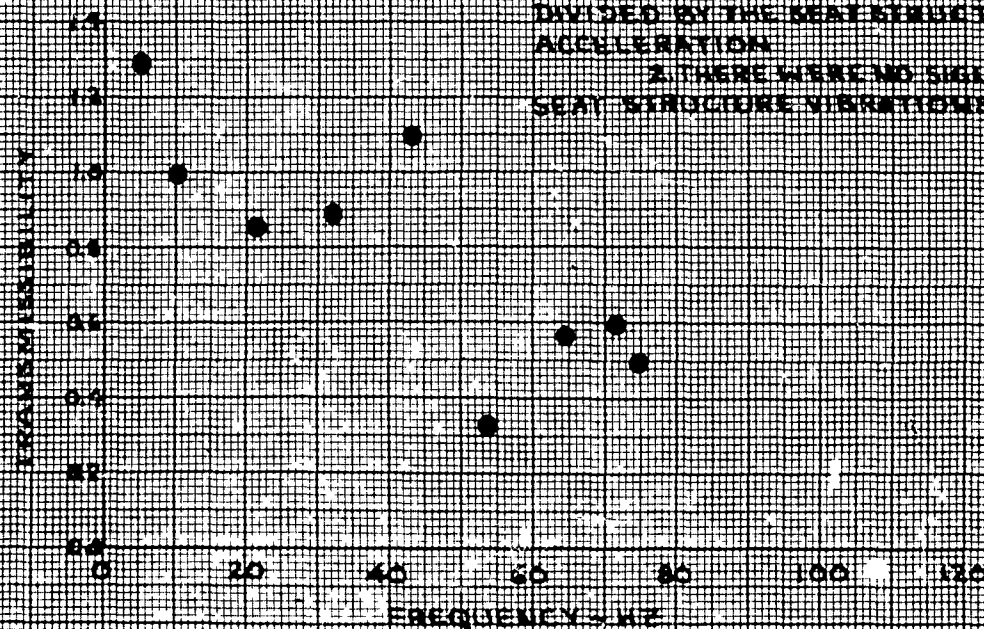


FIGURE E
SEAT PAD AND PILOT TRANSMISSIBILITY
UNITH USAY67-IT145
ALL AXES, ALL NON-FIRING FLIGHT
CONDITIONS COMBINED

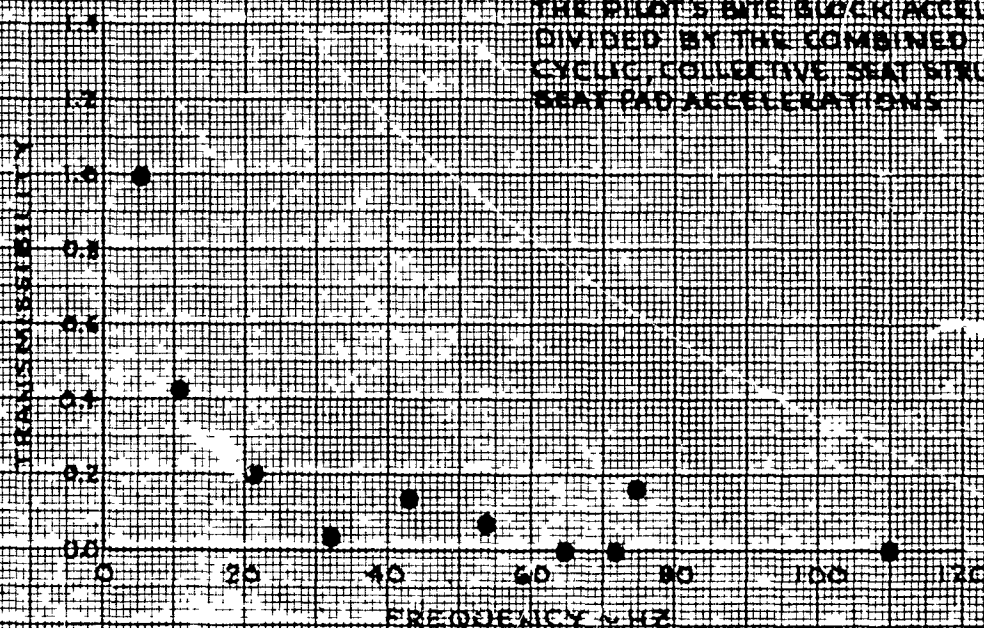
SEAT PAD

NOTE 1: SEAT PAD TRANSMISSIBILITY IS THE SEAT PAD ACCELERATION DIVIDED BY THE SEAT STRUCTURE ACCELERATION
2: THERE WERE NO SIGNIFICANT SEAT STRUCTURE VIBRATIONS ABOVE 100 HZ



PILOT

NOTE 1: PILOT TRANSMISSIBILITY IS THE PILOT'S RATE GUNCK ACCELERATION DIVIDED BY THE COMBINED RIGHT PEDAL CYCLIC, COLLECTIVE, SEAT STRUCTURE AND SEAT PAD ACCELERATIONS



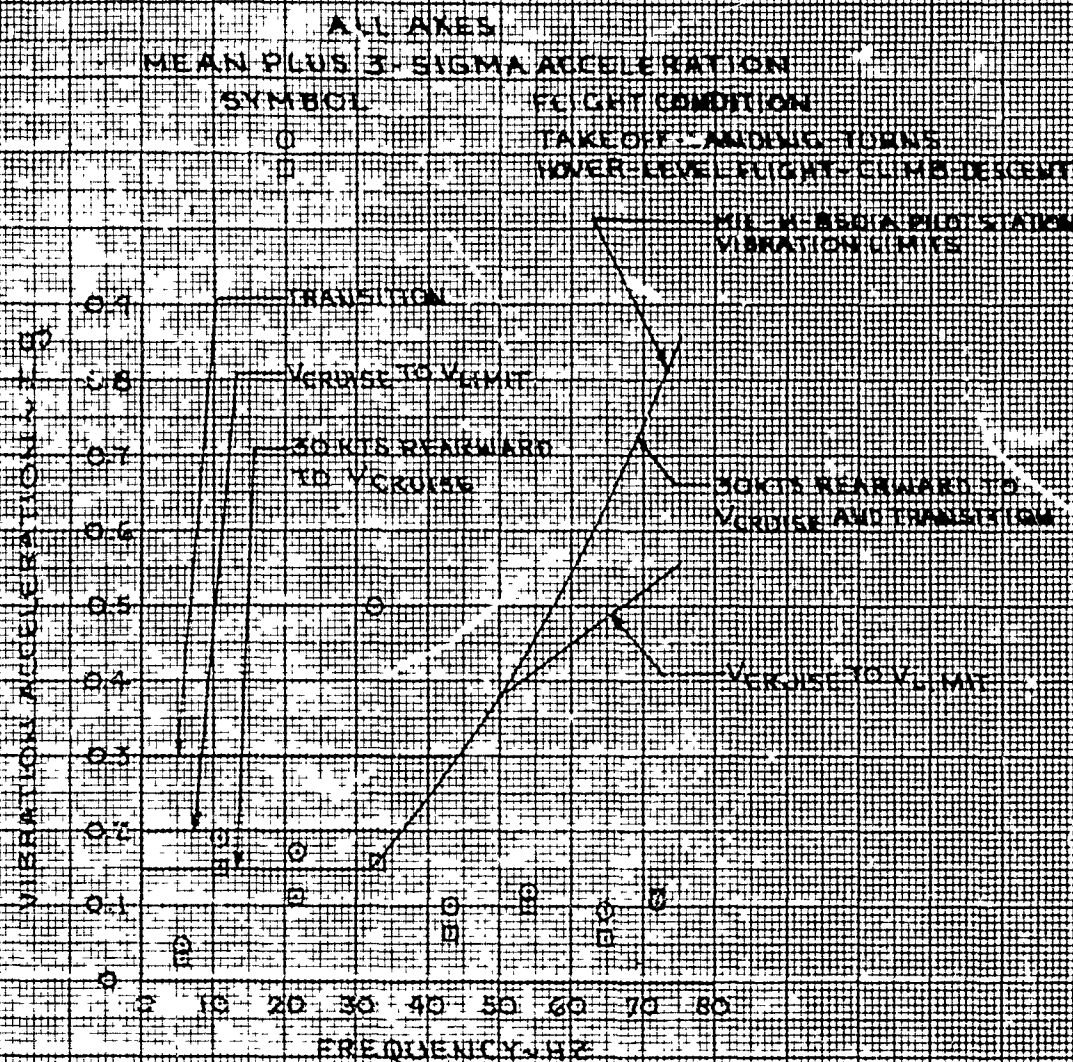
is no attenuation of seat structure vibrations by the seat pad below 45 Hz. Since the primary main rotor-induced vibrations are below 45 Hz, it is likely that a significant reduction in vibrations transmitted to the pilot could be achieved with a seat pad which attenuated low-frequency vibrations.

20. The pilot's head vibrations were measured with an accelerometer attached to a bite block. The bite block was a plastic and aluminum form shaped to fit the pilot's teeth which the pilot held securely in his mouth when vibrations were recorded from this location. The ratio of the bite block acceleration to the combined collective grip, cyclic grip, right foot rest, seat structure, and seat pad accelerations was calculated and is presented as pilot transmissibility in figure F. The results show that the pilot's body attenuates vibrations above 10 Hz.

21. The pilot station vibration limits of paragraph 3.7.1b of MIL-H-8501A (ref 5, app A) are compared to the seat structure and seat pad mean plus 3-sigma accelerations for all axes combined in figure F. The data are divided into two groups: hover, level flight, climb, and descent compose one group; while takeoff, landing, and turns compose the other group. There is no specification limit on vibration levels during maneuvering flight, so these data were combined with the takeoff and landing transition data, since most maneuvers are transient conditions. There is a specification vibration limit for flight from V_{cruise} to V_{limit} airspeeds but no data were grouped for this condition, since the V_{cruise} and V_{limit} airspeeds are identical for the UH-1H helicopter. The results show that the main rotor 2/rev acceleration slightly exceeded the cruise flight limit of 0.15g and the main rotor 6/rev acceleration exceeded the transition flight limit of 0.3g at this frequency. Vibration levels at the pilot station in excess of the limits of MIL-H-8501A are a shortcoming, correction of which is desirable.

22. In addition to this combined test condition data, a bite block mean plus 3-sigma acceleration of 0.32g at 7.3 Hz (fig. 134, app G) was recorded for the ground-idle test condition. This test was conducted in a 15- to 20-knot wind at a main rotor speed of 220 rpm. The wind and low rotor speed excited a helicopter structural mode which produced high-amplitude low-frequency vibrations at the pilot station. This low-frequency vibration was qualitatively judged to be tolerable only for short periods of time. In contrast, the 32.4-Hz (6/rev) combined test condition seat pad vibration of 0.50g was not noticeable to the pilot. This result is indicated in figure D, which shows that vibrations at 32.4 Hz are almost completely attenuated by the pilot's body while those at 7.3 Hz are not attenuated. MIL-H-8501A specifies constant acceleration limits from zero frequency to 32 Hz. The results of this test indicate that specification acceleration levels should decrease with frequency.

FIGURE F
COMPARISON WITH MIL-H-8501A CREW STATION VIBRATION LIMITS
UH-1H USA 3/3GT-114S



Selected Component Vibration Characteristics

23. Vibration data were recorded at 32 locations throughout the helicopter, other than instruments, avionics, and the pilot station. These locations are described in table 2 and appendix D and shown in photographs in appendix E. Data were recorded at the request of the United States Army Air Mobility Research and Development Laboratory (USAAMRDL), Eustis Directorate, and were transmitted to USAAMRDL in the Northrop Corporation data report (ref 7, app A). The selected component second-pass nonfiring data and first-pass firing data are presented in this report in figures 12 through 39 and figures 50 through 79, appendix G, respectively. The selected component first-pass nonfiring data are not presented in this report but are available from USAASTA.

24. The vibration characteristics at these locations will not be discussed in detail but in general show the presence of high-level, high-frequency vibration near rotating equipment, particularly gearboxes. The maximum mean plus 3-sigma vibration acceleration level recorded for all locations was 44g at 1920 Hz at the 42-degree tail rotor gearbox (fig. 26, app G).

Comparison with OH-58A Test Data

25. Vibration data gathered from the OH-58A helicopter (ref 2, app A) are compared with the UH-1H helicopter vibration data in figure C. The nonfiring data are similar for both helicopters. Both helicopters have two-bladed rotors of similar design and the main rotor driving frequencies are nearly alike. The highest vibration levels occurred in both helicopters at the 4/rev and 6/rev frequencies. However, the amplitude of the UH-1H main rotor-induced vibrations was about twice that of the OH-58A main rotor-induced vibrations. The weapons firing vibrations of the UH-1H with the M23 armament subsystem were markedly different from those of the OH-58A with the M27E1 armament subsystem. The UH-1H weapons vibrations were broadband with little discrete frequency content, while the OH-58A weapons firing vibrations were harmonic with a high discrete frequency content. The amplitude of the UH-1H weapons firing vibrations was only about one-tenth that of the OH-58A vibrations. The lack of harmonic frequency content and large reduction in vibration amplitude was not expected, since identical ammunition was fired from each helicopter. The M23 armament subsystem (UH-1H) uses two M60D gas-driven machine guns firing 7.62mm ammunition at about 9 rounds per second from each gun. The M27E1 armament subsystem uses one M134 electrically-driven machine gun firing 7.62mm ammunition at about 33 or 66 rounds per second.

TEMPERATURE DATA

Component Air Temperatures

26. Component part surrounding air temperatures were recorded at 20 locations, as described in table 3, appendix D, and shown in photographs in appendix E.

Temperatures were recorded for static hot soaks in the sun, level flight between 57 and 99 KCAS, and in-ground-effect (IGE) and out-of-ground-effect (OGE) hover. The helicopter was headed toward the sun for all temperature measurements. All vents and the pilot and copilot windows were open for in-flight temperature measurements. Temperatures were recorded with the vents, windows, and doors open and closed for static temperature measurements. Temperature data for all conditions are presented in table 5. Detailed static temperature data are presented in figures 136 through 144, appendix G, for locations with a temperature rise of 10°C or greater. Temperature rise was determined by subtracting the outside air temperature from the component temperature of interest.

27. It was found that solar radiation had a significant effect on static temperatures but only a small effect on in-flight temperatures. In-flight data were obtained over a range of solar radiation values by recording data at different times of day from morning until afternoon. Less than 10 minutes were required for in-flight temperatures to stabilize at steady-state values. The in-flight temperature data presented in table 5 were obtained by averaging the temperature data over the range of solar radiation values tested. Static temperatures required about 2 hours to stabilize. This long stabilization time required that temperatures be recorded around noon, when solar radiation was nearly constant for a 2-hour period. To determine static temperatures for values of solar radiation and ambient air temperature different than those tested, an analytical method was developed which is described in appendix F. Figures 136 through 144, appendix G, are the results of this analytical method and representative solar radiation values (refs 8 and 9, app A).

28. Static temperature data for the cabin and avionics locations are tabulated at a solar radiation value of 350 BTU/hr-ft² and outside air temperature of 45°C in table 5. These results show that the highest temperatures occur in the forward cabin and forward avionics areas under static conditions and decrease in flight. Temperatures in the aft cabin and avionics areas were low under static conditions but increased in flight. The high forward cabin and avionics static temperatures are due to large amounts of transparent area in the forward section of the fuselage, which allow solar radiation to enter. Forward cabin temperatures are lower in flight due to increased air circulation. Aft cabin and avionics temperatures increase in flight due to engine, transmission, hydraulic, and electronic component heat sources. The highest average temperature rise recorded was 81.5°C at the upper engine compartment in an IGE hover.

Wet Bulb Globe Temperature Index

29. The WBGT index (ref 10, app A) was recorded in flight with all doors closed, all vents open, and the pilot and copilot windows open. A sensing unit consisting of a dry bulb thermometer, wet bulb thermometer, and black globe thermometer was located near the pilot in the sun. The sensing unit was obtained from the United States Army Medical Equipment Research and Development Laboratory and is shown in photograph 42, appendix E. Dry bulb and black globe temperatures versus solar radiation and airspeed are presented in figure G.

Table 5. Average Temperature Rise.

UH-1H USA S/N 67-17145

Location Number	Location Name	Average Temperature Rise (~ °C) ¹			
		In-Ground-Effect Hover ²	Out-of-Ground-Effect Hover ²	Level Flight ²	Static ³
1	Forward avionics	10.0	6.5	8.3	26.0
2	Aft avionics	10.5	11.5	9.9	2.9
3	Forward cabin	3.5	3.5	4.5	30.0
4	Aft cabin	6.0	7.0	14.9	10.0
5	Forward transmission compartment	8.5	18.5	24.3	0.8
6	Aft transmission compartment	8.0	11.0	32.1	3.5
7	Upper engine compartment	81.5	31.5	58.6	19.0
8	Lower engine compartment	51.2	26.0	38.5	5.8
9	42-degree gearbox	33.5	18.5	29.1	10.0
10	90-degree gearbox	0.5	0.5	6.6	3.7
11	Oil cooler	15.5	15.5	11.3	7.7
12	Right fuel boost pump	Zero	1.5	1.3	Zero
13	Left fuel boost pump	8.5	17.5	11.7	Zero
14	No. 1 hanger bearing	64.5	37.5	43.0	12.5
15	No. 2 hanger bearing	58.0	28.0	14.0	18.5
16	No. 3 hanger bearing	33.0	71.5	13.8	28.0
17	No. 4 hanger bearing	39.5	28.0	21.2	26.5
18	N ₁ tach generator	59.5	26.5	46.6	8.7
19	N ₂ tach generator	67.5	44.5	47.4	7.4
20	Main rotor tach generator	5.5	21.0	26.1	4.1

¹Average temperature rise calculated by subtracting the outside air temperature from each location temperature.

²57 to 99 KCAS. Average solar radiation of 241 BTU/hr-ft².

³Solar radiation of 350 BTU/hr-ft². Outside air temperature of 45°C.

SYMBOL	SOLAR RADIATION-BTU/HR-FT ²
D	359
O	318
S	296
N	258
A	67



30. The WBGT index is used to describe the effect of the temperature environment on the human body. It is determined by adding 70 percent of the naturally convected wet bulb temperature, 20 percent of the black globe temperature, and 10 percent of the dry bulb temperature. Temperatures are in degrees Fahrenheit. The following criteria for application of the WBGT are proposed in Department of the Army Technical Bulletin TB MED 175 (ref 10, app A):

- a. When the WBGT Index reaches 82°, discretion should be used in planning heavy exercise for unseasoned personnel.
- b. When the WBGT reaches 85°, strenuous exercises, such as marching at standard cadence should be suspended in unseasoned personnel during their first three weeks of training. At this temperature training activities may be continued on a reduced scale after the second week of training.
- c. Outdoor classes in the sun should be avoided when the WBGT exceeds 85°.
- d. When the WBGT reaches 88°, strenuous exercise should be curtailed for all recruits and other trainees with less than 12 weeks training in hot weather. Hardened personnel, after having been acclimatized each season, can carry on limited activity at WBGT of 88° to 90° for periods not exceeding 6 hours a day.

The highest WBGT value recorded in cruise flight was 81°F at an outside air temperature of 86°F, a relative humidity of 26 percent, and a solar radiation value of 250 BTU/hr-ft². Based on the data presented in figure G and a psychrometric chart, the WBGT can be calculated for any combination of outside air temperatures, relative humidity, and solar radiation. For an outside air temperature of 100°F, a relative humidity of 50 percent, and a solar radiation of 250 BTU/hr-ft², the WBGT would be 97°F at the pilot station. This calculation is described in appendix F. A WBGT of 97°F is well in excess of the maximum discussed in the above criteria, and it is likely that a WBGT higher than 97°F would be recorded under certain conditions. Excessively high WBGT index at the pilot station under certain environmental conditions is a shortcoming, correction of which is desirable.

CONCLUSIONS

GENERAL

31. Analysis of the test results obtained during this evaluation resulted in the following conclusions:

a. The UH-1H instrument and avionics vibrations are primarily sinusoidal with a random variation of amplitude with time at each frequency at steady flight conditions (para 14).

b. The primary source of low-frequency vibration is the main rotor, with a maximum mean plus 3-sigma acceleration of 0.94g measured at the main rotor 6/rev frequency of 32.4 Hz (para 14).

c. Gunfire-induced vibrations are broadband with little discrete frequency content (para 15).

d. Gunfire-induced vibrations were less than main rotor induced-vibrations, with a maximum mean plus 3-sigma acceleration of 0.24g at 466 Hz (para 15).

e. All instrument and avionics mean plus 3-sigma vibration levels are well below the laboratory test curve of MIL-STD-810B (para 16).

f. The pilot seat pad did not attenuate vibrations below 45 Hz (para 19).

g. The pilot's body attenuates vibrations above 10 Hz (para 20).

h. Pilot station vibrations at 7.3 Hz are more objectionable than those of equal amplitude at 32.4 Hz (para 22).

i. The maximum mean plus 3-sigma vibration level for all locations tested was 44g at 1920 Hz at the 42-degree gearbox (para 24).

j. Main rotor-induced vibration amplitudes in the OH-58A and UH-1H helicopters reach their highest levels at the 4/rev and 6/rev frequencies in both helicopters (para 25).

k. The amplitude of the UH-1H main rotor-induced vibrations is about twice that of the OH-58A main rotor-induced vibrations (para 25).

l. The highest instrument and avionics temperatures were recorded in the forward cabin and forward avionics areas under static conditions and decreased in forward flight (para 28).

m. The highest average temperature rise was 81.5°C above the outside air temperature at the upper engine compartment in an IGE hover (para 28).

n. There were no deficiencies noted during the testing.

SHORTCOMINGS AFFECTING MISSION ACCOMPLISHMENT

32. Correction of the following shortcomings is desirable for improved operation and mission capabilities:

a. Amplification of vibrations at the main rotor driving frequencies by the vibration isolation mounts on the MD-1 vertical gyro and RT-348/ARC 54 radio (para 17).

b. High pilot station vibrations in excess of the limits of paragraph 3.7.1b of MIL-H-8501A (para 21).

c. Excessively high Wet Bulb Globe Temperature index at the pilot station under certain environmental conditions (para 30).

RECOMMENDATIONS

33. The shortcomings should be corrected.
34. The data in this report and subsequent environmental test reports should be applied to revising appropriate military environmental specifications.
35. Improved vibration isolation for instrument and avionics components should be provided (para 17).
36. Consideration should be given to use of a seat cushion which would attenuate vibrations in the frequency range of the main rotor (para 19).
37. Consideration should be given to specifying the pilot station vibration limits in MIL-H-8501A as a function of frequency below 32 Hz (para 22).
38. Consideration should be given to installing an environmental control system for use in extreme environmental conditions (para 30).

APPENDIX A. REFERENCES

1. Letter, AVSCOM, AMSAV-EF, 31 August 1971, subject: AVSCOM Test Request No. 70-15, Instrument Panel, Avionics Compartment and Crew Station Environmental Study.
2. Final Report, USAASTA, Project No. 70-15-1, *Instrument Panel and Avionics Compartment Environmental Survey, Production OH-58A Helicopter*, September 1972.
3. Technical Manual, TM 55-1520-228-10, *Army Model OH-58A Helicopter*, 13 October 1970.
4. Test Plan, USAASTA, Project No. 70-15, *Helicopter Vibration and Environmental Survey*, July 1971.
5. Military Standard, MIL-STD-810B, *Environmental Test Methods*, 15 June 1967.
6. Military Specification, MIL-H-8501A, *Helicopter Flying and Ground Handling Qualities; General Requirements For*, 7 September 1961, Amended 3 April 1962.
7. Test Data Reduction Report, Northrop Corporation, Electronics Division, NORT 72-279, *Environmental Vibration Survey, UH-1H Helicopter-Iroquois*, August 1972.
8. Publication, Institut Royale Meteorologique de Belgique, *Donnes du Rayonnement Solaire a Leopoldville*, Periode 1953-1962, 1965.
9. Publication, D2-90577-2, R. A. Atlas and B. N. Charles, *Summary of Solar Radiation Characteristics, Tabular Summaries*, December 1964.
10. Department of the Army Technical Bulletin, TB MED 175, *The Etiology, Prevention, Diagnosis and Treatment of Adverse Effects of Heat*, 25 April 1969.

APPENDIX B. GENERAL AIRCRAFT INFORMATION

DIMENSIONS AND DESIGN DATA

Overall Dimensions

Aircraft length (rotor turning)	57 ft, 1.1 in.
Aircraft length (nose to tail skid)	41 ft, 11.1 in.
Width (rotor turning)	48 ft
Width (rotor static)	9 ft, 6.6 in.
Height (to top of rotor mast)	14 ft, 0.7 in.
Height (to top of turning tail rotor)	14 ft, 5.5 in.

Main Rotor

Number of blades	2
Diameter	48 ft
Blade chord (constant)	21 in.
Solidity	0.0464
Blade twist angle	-10.0 deg linear
Hub precone angle	2.75 deg
Airfoil type	NACA 0012

Tail Rotor

Number of blades	2
Diameter	8 ft, 6 in.
Blade chord	8.41 in.
Blade twist angle	Zero deg
Hub precone angle	Zero deg
Airfoil section designation and thickness (constant)	NACA 0015

Control Travel

Cyclic stick (measured at center of grip):

Longitudinal 12.2 in.

Lateral 12.3 in.

Collective stick (measured at center of grip) 10.75 in.

Antitorque pedals (from neutral) 6.8 in.

Gear Ratio

Engine to main rotor 20.370:1

Engine to tail rotor 3.990:1

Operating Limitations

Output shaft speed 6400 to 6600 rpm

Turbine outlet temperature 625°C (continuous)
645°C (30 minutes)

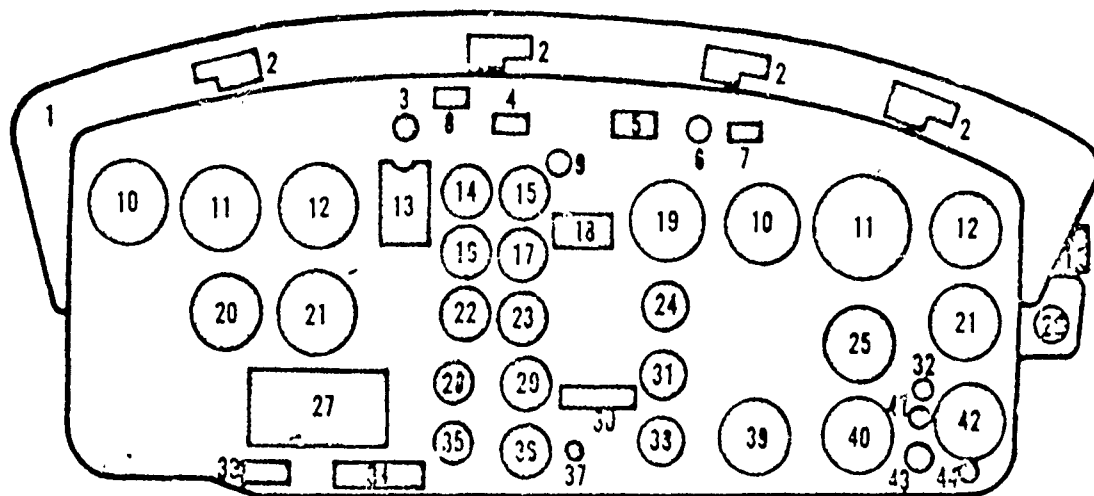
Rotor speed (power ON) 314 to 324 rpm

Rotor speed (power OFF) 294 to 339 rpm

Maximum airspeed (V_{max}), sea level 120 KIAS

Torque 50 psi (continuous)

Instrument Panel Configuration, UH-1H 67-17145



- | | | |
|------------------------------------|--|---------------------------------------|
| 1. Glare Shield | 17. Engine Oil Temperature Indicator | 31. Gas Producer Tachometer Indicator |
| 2. Secondary Lights | 18. Cargo Caution Decal | 32. Marker Beacon Light |
| 3. Engine Air Filter Light | 19. Dual Tachometer | 33. Engine Installation Decal |
| 4. Master Caution | 20. Radio Compass Indicator | 34. Transmitter Selector Decal |
| 5. RPM Warning Light | 21. Vertical Velocity Indicator | 35. Standby Generator Loadmeter |
| 6. Fire Detector Test Switch | 22. Transmission Oil Pressure Indicator | 36. AC Voltmeter |
| 7. Fire Warning Indicator Light | 23. Transmission Oil Temperature Indicator | 37. Compass Slaving Switch |
| 8. Radio Call Designator | 24. Torquemeter Indicator | 38. Exhaust Gas Temperature Indicator |
| 9. Fuel Gage Test Switch | 25. Radio Compass Indicator | 39. Turn and Slip Indicator |
| 10. Airspeed Indicator | 26. Standby Compass | 40. Omni Indicator |
| 11. Attitude Indicator | 27. Operating Limits Decal | 41. Marker Beacon Sensing Switch |
| 12. Altimeter Indicator | 28. Main Generator Loadmeter | 42. Clock |
| 13. Compass Correction Card Holder | 29. DC Voltmeter | 43. Marker Beacon Volume Control |
| 14. Fuel Pressure Indicator | 30. Engine Caution Decal | 44. Cargo Release Armed Light |
| 15. Fuel Quantity Indicator | | |
| 16. Engine Oil Pressure Indicator | | |

AVIONICS EQUIPMENT CONFIGURATION, UH-1H S/N 67-17145

<u>Item</u>	<u>Location</u>
Control intercommunications set C-1611/AIC	Center console (2 each) Aft compartment (2 each)
Radio set AN/ARC-54:	
Receiver-transmitter RT-348/ARC-54	Nose compartment
Control radio set C-3835/ARC-54	Center console
Antenna AT-765/ARC-54	Tail boom above tail rotor
Coupler, antenna CU-943/ARC-54	Tail boom above tail rotor
Antenna assembly 637A-2	Front roof
Radio set AN/ARC-51BX:	
Receiver-transmitter RT-742/ARC-51BX	Nose compartment
Control radio set C-6287/ARC-51BX	Center console
Antenna AT-1108/ARC	Front roof
Radio set AN/ARC-134:	
Receiver-transmitter RT-857/ARC-134	Aft right compartment
Control panel C-7197/ARC-134	Center console
Gyromagnetic compass set AN/ASN-43:	
Induction compass transmitter T-611/AST	Aft tail boom
Electronic control amplifier AM3209/ASN	Nose compartment
Magnetic flux compensator CN-405/ASN	Aft tail boom
Directional gyro CN-988/ASN-43	Aft left compartment
Radio receiving set AN/ARN-82:	
Radio receiver R1388/ARN-82	Nose compartment
DMN 4-4 antenna	Aft tail boom
Control radio set C-6873/ARN-82	Center console

Direction finder set AN/ARN-83:

Radio receiver R-1391/ARN-83
Control direction finder C6899/ARN-83
Antenna AS-1863/ARN-83
Antenna 205-075-325

Nose compartment
Center console
Front roof
Center bottom of aircraft

Transponder set AN/APX-44:

Transponder set control C-2714/APX-44
Antenna AT-884/APX-44

Center console
Bottom of nose section

APPENDIX C. TEST CONFIGURATIONS

HELICOPTER DIAGRAM

FIGURE 1

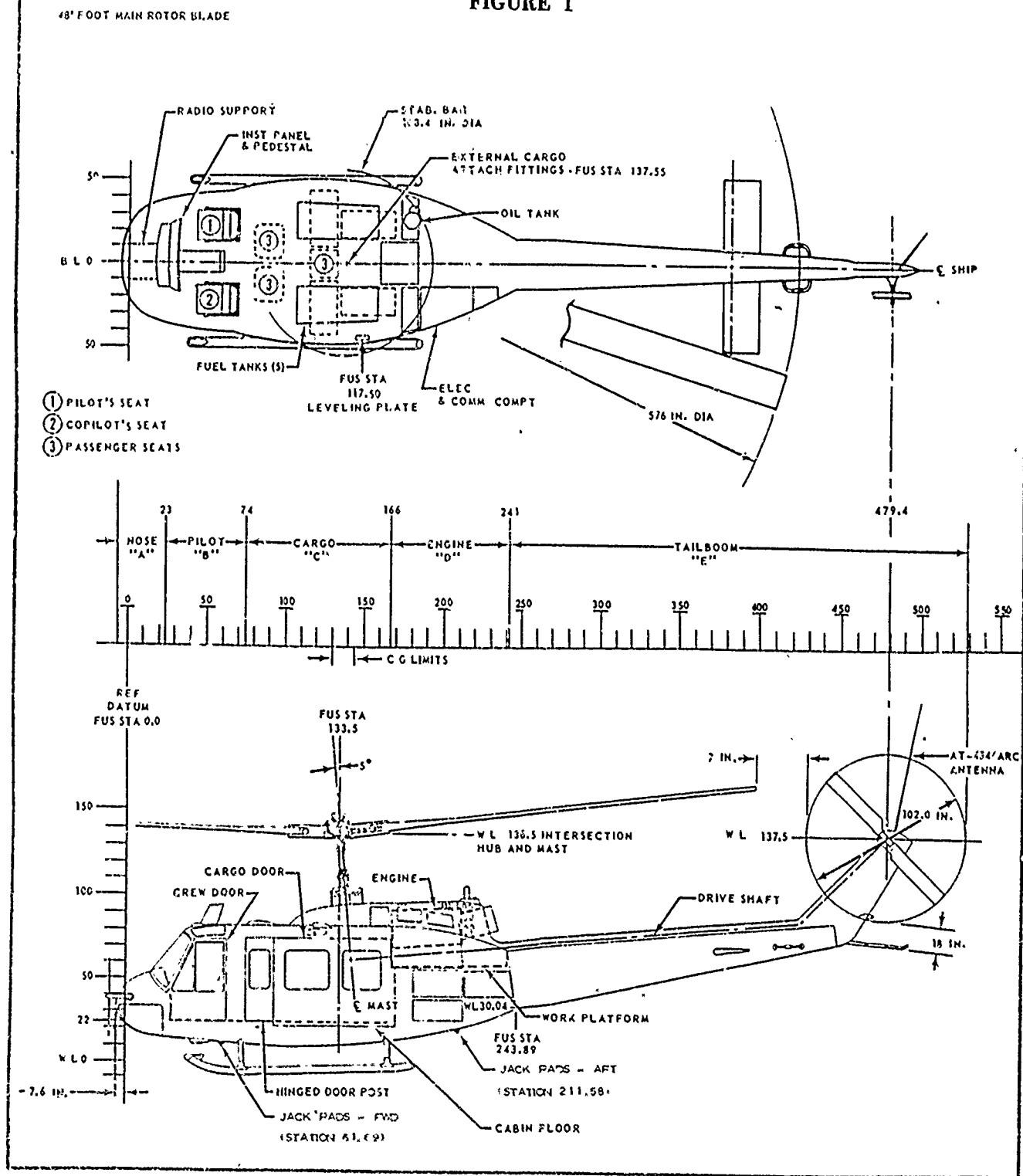


Table 1. Light Weight Test Configuration.¹

Item	Weight (lb)	Longitudinal Fuselage Station (in.)	Lateral Fuselage Station (in.)	Longitudinal Moment (in.-lb)	Lateral Moment (in.-lb)
Basic aircraft	5698	--	--	810,266	-4096
Average fuel	752	--	--	102,500	0.0
Instrumentation	150	100.0	-30	15,000	-3000
Pilot	200	46.7	+22	9,340	+4400
Engineer	200	46.7	-22	9,340	-4400
Test conditions	7000	135.2 (mid)	-1.0, left	946,446	-7096

¹Clean (doors closed).

Table 2. Heavy Weight Test Configuration.¹

Item	Weight (lb)	Longitudinal Fuselage Station (in.)	Lateral Fuselage Station (in.)	Longitudinal Moment (in.-lb)	Lateral Moment (in.-lb)
Basic aircraft	5698	--	--	810,266	-4096
Average fuel	897	--	--	126,000	0.0
Instrumentation	150	100.0	-30	15,000	-3000
Pilot	225	46.7	+22	10,508	+4950
Engineer	225	46.7	-22	10,508	-4950
Ballast	225	90.0	+12	20,250	+2700
Ballast	225	125.0	+35	28,125	+7875
Ballast	225	125.0	+20	28,125	+4500
Ballast	225	125.0	0.0	28,125	0.0
Ballast	225	145.0	+25	32,625	+5625
Ballast	225	145.0	-25	32,625	-5625
Ballast	225	160.0	+25	36,000	+5625
Ballast	230	160.0	-25	36,800	-5750
Test conditions	9000	135.0 (mid)	0.9, right	1,214,957	7854

¹Clean (doors closed).

Table 3. Armed Test Configuration.¹

Item	Weight (lb)	Longitudinal Fuselage Station (in.)	Lateral Fuselage Station (in.)	Longitudinal Moment (in.-lb)	Lateral Moment (in.-lb)
Basic aircraft	5698	--	--	810,266	-4096
Average fuel	926	--	--	130,500	0.0
Instrumentation	150	100.0	-30	15,000	-3000
Pilot	200	46.7	+22	9,340	+4400
Engineer	200	46.7	-22	9,340	-4400
Gunner	200	150.0	+25	30,000	+5000
Gunner	200	150.0	-25	30,000	-5000
M23 armament subsystem	126	150.0	0.0	18,900	0.0
Average ammunition	200	122.0	+15	24,400	+3000
Ballast	200	85.0	+12	17,000	+2400
Test conditions	8100	135.2 (mid)	-0.2, left	1,094,746	-1696

¹M23 armament subsystem (cargo doors open).

APPENDIX D. TEST INSTRUMENTATION

GENERAL

1. Flight test instrumentation was installed, calibrated, and maintained by the Instrumentation and Calibration Divisions of USAASTA and USAAMRDL. This instrumentation was used to record vibration data, temperature data, and flight condition parameters. A list of the instrumentation components is presented in table 1.

VIBRATION INSTRUMENTATION

2. An FM-FM magnetic tape system, was used to record the vibration data. A block diagram of the instrumentation system is presented in figure 1. Data were recorded over a frequency range of 2 to 2000 Hz for all flight conditions. The transducers were miniature triaxial, biaxial, and uniaxial piezoelectric accelerometers which were mounted at 49 locations throughout the aircraft for a total of 140 channels of vibration data. The instrumentation was limited to recording data from 12 accelerometers simultaneously. To record more than 12 channels of data, an eight-position manual switching network was employed and each flight condition was repeated seven times, for a maximum data capacity of 96 channels. To obtain the total of 140 channels of vibration data, the accelerometers were relocated after completion of all test conditions and the test conditions were repeated. The lift link triaxial accelerometer was common to all switch positions to verify repetition of each test condition. The maximum capacity of the instrumentation system is 96 channels without accelerometer relocation and 192 channels with one relocation. Accelerometers were bonded to the component of interest with the accelerometer axis aligned to the component axis. The mounting locations of each accelerometer are shown in the photographs in appendix E. Table 2 lists the accelerometer locations, accelerometer type, and amplitude range.

3. The vibration instrumentation was calibrated to determine the amplitude sensitivity and frequency response of the total data system. A frequency sweep was performed on each accelerometer with an electrodynamic shaker. Each accelerometer was mounted back to back with a calibrated reference accelerometer and the charge sensitivity (picocoulomb/g) and frequency response of the test accelerometer determined by comparison with the reference accelerometer. The airborne data recording system was calibrated by means of a charge source. For each channel, the charge source was set to simulate a given acceleration value by reference to the accelerometer charge sensitivity determined by the shaker calibration, and the airborne data system output was recorded. The ground station was calibrated separately from the airborne system, and the two system scale factors were combined to obtain an overall data system scale factor. It is estimated that the accuracy of the total vibration measurement system, both airborne and ground units, is within ± 10 percent of the true acceleration amplitude.

Table 1. Instrumentation Component Description.

Nomenclature	Manufacturer	Quantity	Model Number
Piezoelectric accelerometer (triaxial)	Endevco	23	2228C
Piezoelectric accelerometer (uniaxial)	Endevco	17	2226C
Piezoelectric accelerometer (uniaxial)	Endevco	6	2242C
Piezoelectric accelerometer (triaxial)	Endevco	2	2223C
Piezoelectric accelerometer (uniaxial)	Endevco	2	2224C
Line driver	MB Electronics	81	9402216
Amplifier	MB Electronics	12	N400
Switching relays	Potter and Brumfield	24	JDT27DD1
FM rack	Electro Mechanical Research	2	--
FM rack voltage code oscillator (VCO)	Electro Mechanical Research	12	307A-02
FM rack mixing amplifier	Electro Mechanical Research	2	311A-02-1
FM rack reference oscillator	Electro Mechanical Research	2	313A-01
Tape recorder	Genisco Technology Corp.	1	10-286
Time code generator	Electro Mechanical Research	1	CL24D-27.6A
Thermocouple switch (24 channels)	Thermo Electric	1	33113
Thermocouple indicator	Newport Laboratories	1	2600
Thermocouple wire (iron-constantan)	Series J	--	--
Thermal radiometer	Teledyne Geotech	1	TCH-188-01

FIGURE 1
AIRBORNE DATA SYSTEM

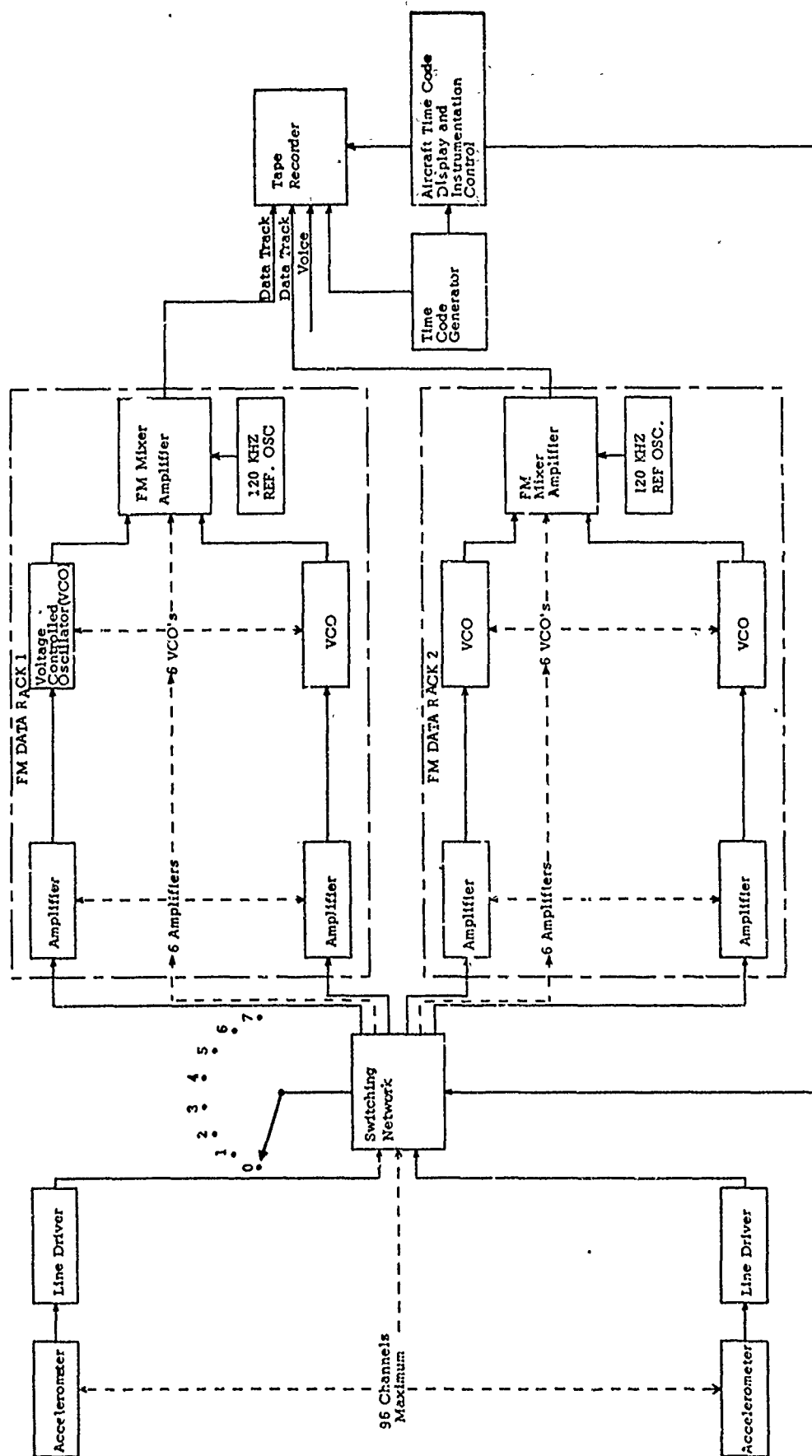


Table 2. Accelerometer Locations.

Location	Location Number	Fuselage Station (in.)	Water Line (in.)	Buttline (in.)	Axis	Full Scale Acceleration Range (\pm g)	Accelerometer Type
Instrument panel	1	31.8	56.3	10.2L	3	5	2228C
	2	34.2	46.9	8.2L	3	5	2228C
	3	33.7	49.0	3.8R	3	5	2228C
	4	31.8	56.3	15.3R	3	5	2228C
	5	34.6	45.4	22.0R	3	5	2228C
Avionics							
HD-1 vertical gyro	6	17.8	42.9	11.5R	3	5	2228C
HD-1 vertical gyro mount	7	17.5	4.9	11.5R	3	5	2226C
Left rear compartment	8	200.0	40.8	26.7L	3	5	2228C
M-348/ARC-54 radio	9	8.0	25.2	3.7L	3	5	2228C
RT-348/ARC-54 radio mount	10	6.5	23.5	3.7L	3	5	2226C
Pilot							
Seat pad plate	11	58.8	35.0	22.8R	3	5	2228C
Seat structure	12	56.7	30.8	22.8R	3	5	2242C
Right pedal foot rest	13	26.9	24.7	29.2R	Vertical, lateral	5	2226C
Collective grip ¹	14	42.5	40.2	11.3R	Vertical	5	2226C
Cyclic grip ²	15	43.6	44.0	22.9R	3	5	2228C
Pilot's helmet (SPH-4)	16	--	--	--	3	5	2228C
Bite block	17	--	--	--	3	5	2228C
Transmission mounts							
Forward left	18	138.8	69.6	12.7L	3	50	2228C
Forward right	19	138.8	69.6	12.7R	3	50	2228C
Aft right	20	156.7	71.7	12.7L	3	50	2228C
Aft left	21	156.7	71.7	12.7R	3	50	2228C
Tail boom attach points							
Upper left	22	246.5	67.0	12.5L	3	5	2228C
Lower right	23	251.5	34.4	12.5R	3	5	2228C
Engine compartment, deck							
Joint	24	185.6	58.2	26.2L	3	5	2228C
Panel	25	203.5	58.2	26.2L	3	5	2228C
Engine compartment, forward							
Firewall, side	26	174.0	70.7	28.3L	3	5	2228C
Firewall, center	27	174.0	70.7	Zero	3	5	2228C
Engine mounts							
Left forward	28	179.4	77.2	8.8L	3	5	2228C
Left aft	29	200.0	75.8	11.8L	3	5	2228C
Tail rotor servo bulkhead	30	219.6	37.7	7.9R	3	5	2228C
Oil cooler	31	227.2	40.8	3.7R	3	5	2228C
Tail rotor shaft 42-degree gearbox	32	441.2	87.7	Zero	3	100	2223C
Tail rotor shaft 90-degree gearbox	33	486.6	138.7	4.6L	3	100	2228C
Hydraulic servo, transmission bay	34	137.1	50.3	6.1L	3	5	2228C
Fuel boost pump, right	35	118.3	11.7	33.7R	3	5	2228C
Gas producer tach generator	36	119.6	80.0	6.2R	3	100	2223C
Main rotor tach generator	37	145.8	63.3	9.2R	3	50	2226C
Power turbine tach generator	38	187.9	86.8	9.6L	3	50	2226C
Tail rotor shaft hanger bearing							
No. 1	39	222.5	68.8	0.8L	Vertical, lateral	100	2224C
No. 2	40	245.8	70.0	0.8L	Vertical, lateral	50	2226C
No. 3	41	308.9	75.2	0.8L	Vertical, lateral	50	2226C
No. 4	42	371.8	80.8	0.8L	Vertical, lateral	50	2226C
Lift link	43	144.0	59.4	1.7L	3	5	2242C
Engine mount, right	44	200.0	75.3	12.5R	3	5	2228C
Left fuel boost pump	45	118.3	11.7	33.7R	3	5	2228C
Engine							
Aft bottom	46	213.6	73.1	Zero	3	100	2228C
Front top	47	185.6	91.2	Zero	3	100	2228C
Mid top	48	202.5	96.2	Zero	3	100	2228C
Gun mount, left side	49	138.3	20.8	52.3R	3	100	2228C

¹Collective full down.²Cyclic centered.

TEMPERATURE INSTRUMENTATION

4. Temperature data were recorded by mounting thermocouples at 20 locations throughout the helicopter. The temperatures were displayed on one temperature indicator which was switched to the desired thermocouple. Table 3 lists the locations of the thermocouples and the temperature measurement equipment is described in table 1. Photographs of the thermocouple locations are presented in appendix E. Solar radiation was recorded on the ground with a calibrated radiometer. Outside air temperature (OAT) was recorded with a laboratory thermometer for static temperature measurements and with the ship's OAT indicator for in-flight temperature measurement.

Table 3. Thermocouple Locations.

Location	Location Number	Fuselage Station (in.)	Water Line (in.)	Buttline (in.)
Forward avionics	1	18.3	45.8	10.0R
Aft avionics	2	200.0	45.8	18.3L
Forward cabin	3	56.7	77.5	Zero
Aft cabin	4	130.0	81.7	Zero
Forward transmission compartment	5	145.0	65.0	Zero
Aft transmission compartment	6	158.3	75.0	Zero
Upper engine compartment	7	190.8	96.7	Zero
Lower engine compartment	8	200.0	59.2	Zero
42-degree gearbox	9	440.8	86.7	Zero
90-degree gearbox	10	487.4	139.1	4.2L
Oil cooler	11	231.6	36.7	4.2R
Right fuel boost pump	12	118.3	10.8	33.3R
Left fuel boost pump	13	118.3	10.8	33.3L
No. 1 hanger bearing	14	222.5	69.2	0.8L
No. 2 hanger bearing	15	245.8	70.0	0.8L
No. 3 hanger bearing	16	310.0	75.0	0.8L
No. 4 hanger bearing	17	372.4	80.8	0.8L
Gas producer tach generator	18	188.3	85.8	10.0L
Power turbine tach generator	19	189.1	80.8	5.8R
Main rotor tach generator	20	163.3	64.2	9.2R

FLIGHT CONDITION PARAMETERS

5. The parameters listed in table 4 were hand-recorded from the ship's standard instruments to determine the flight condition. The readability for each instrument listed in table 4 was determined by dividing the smallest increment marked on the dial by 5.

Table 4. Flight Condition Parameters.

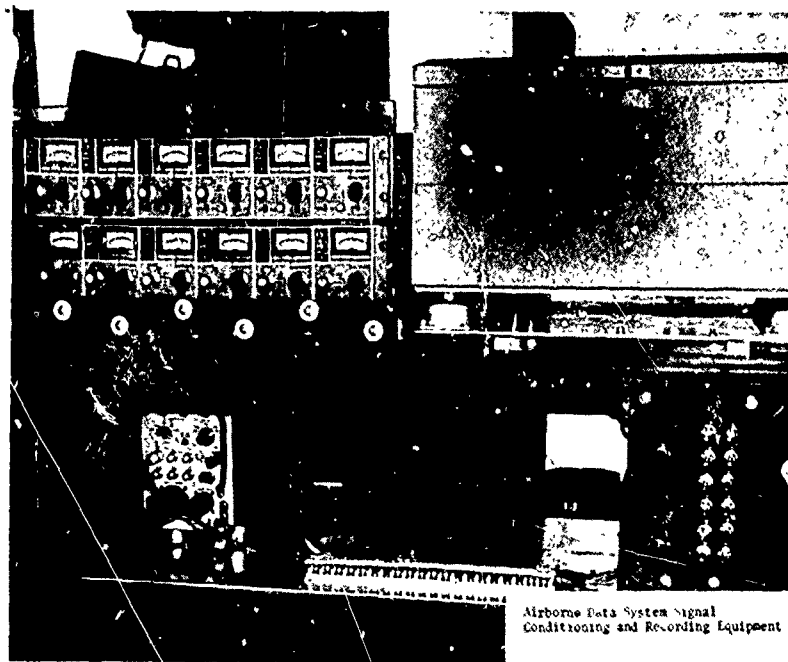
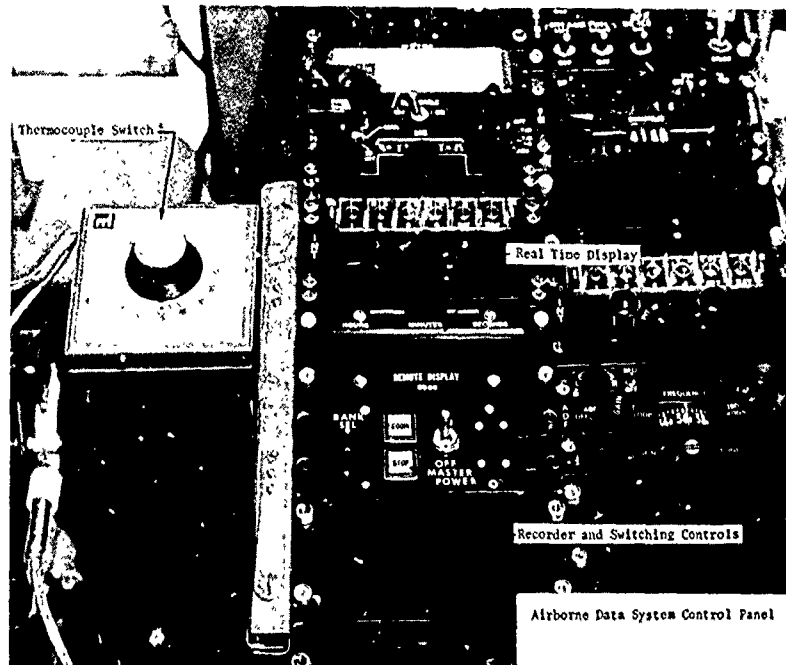
Parameter	Range of Interest	Readability
Airspeed	20 to 120 knots	± 1.0 knot
Altitude	Zero to 10,000 feet	± 4.0 feet
Outside air temperature	Zero to 30°C	$\pm 0.4^\circ\text{C}$
Main rotor speed	294 to 324 rpm	± 2.0 rpm
Gas producer speed	60 to 101.5 percent	± 0.2 percent
Fuel quantity	Zero to 1400 pounds	± 4.0 pounds

APPENDIX E. INSTRUMENTATION PHOTOGRAPHS

Index

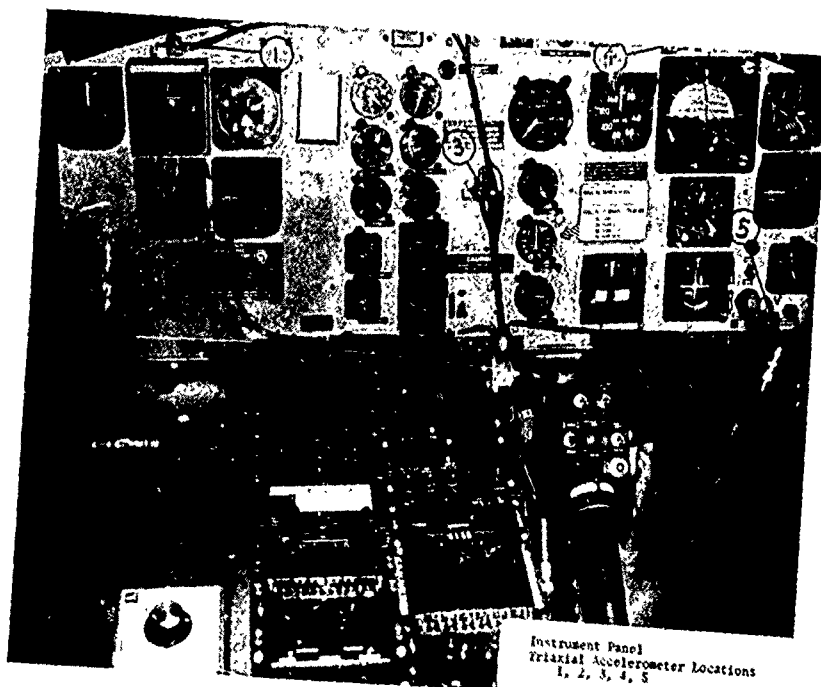
<u>Photograph</u>	<u>Photograph Number</u>
Airborne Data System Control Panel	1
Airborne Data Recording Equipment	2
7.62mm M60D Machine Gun	3
Accelerometer Locations 1, 2, 3, 4, and 5	4
Accelerometer Locations 6 and 7	5
Accelerometer Location 8	6
Accelerometer Locations 9 and 10	7
Accelerometer Location 11	8
Accelerometer Location 12	9
Accelerometer Location 13	10
Accelerometer Location 14	11
Accelerometer Location 15	12
Accelerometer Location 16	13
Accelerometer Location 17	14
Accelerometer Locations 18, 19, 20, and 21	15
Accelerometer Location 22	16
Accelerometer Location 23	17
Accelerometer Locations 24 and 25	18
Accelerometer Location 26	19
Accelerometer Location 27	20
Accelerometer Location 28	21
Accelerometer Location 29	22
Accelerometer Locations 30 and 31	23
Accelerometer Location 32	24
Accelerometer Location 33	25
Accelerometer Location 34	26
Accelerometer Location 35	27
Accelerometer Location 36	28
Accelerometer Location 37	29

Accelerometer Location 38	30
Accelerometer Location 39	31
Accelerometer Location 40	32
Accelerometer Locations 41 and 42	33
Accelerometer Location 43	34
Accelerometer Locations 44 and 46	35
Accelerometer Location 45	36
Accelerometer Locations 47 and 48	37
Accelerometer Location 49	38
Thermocouple Location 1	5
Thermocouple Location 2	6
Thermocouple Location 3	39
Thermocouple Location 4	40
Thermocouple Location 5	34
Thermocouple Location 6	41
Thermocouple Location 7	37
Thermocouple Location 8	35
Thermocouple Location 9	24
Thermocouple Location 10	25
Thermocouple Location 11	23
Thermocouple Location 12	27
Thermocouple Location 13	36
Thermocouple Location 14	31
Thermocouple Location 15	32
Thermocouple Locations 16 and 17	33
Thermocouple Location 18	30
Thermocouple Location 19	28
Thermocouple Location 20	29
Wet Bulb Globe Temperature Sensor	42





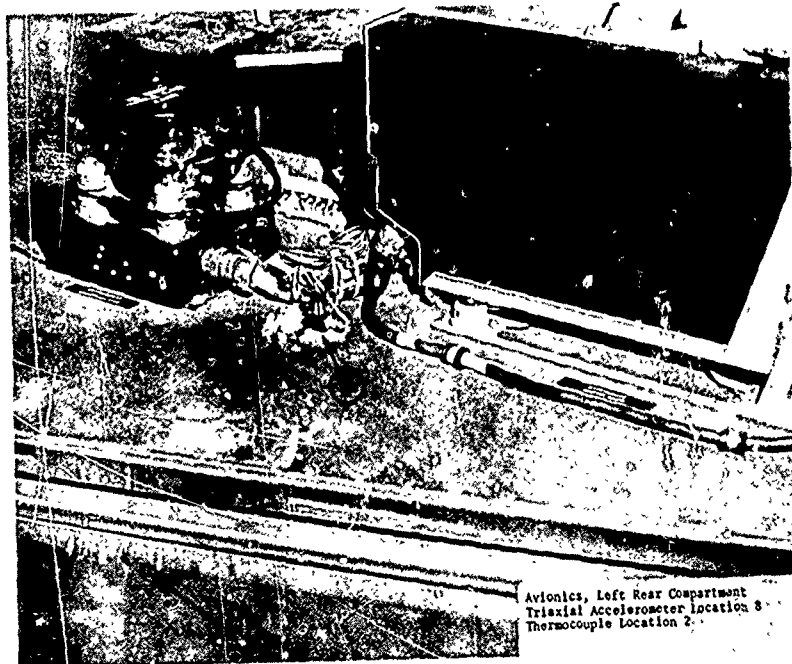
Best Door View
Note Accelerometer Locations
Accelerometer Locations



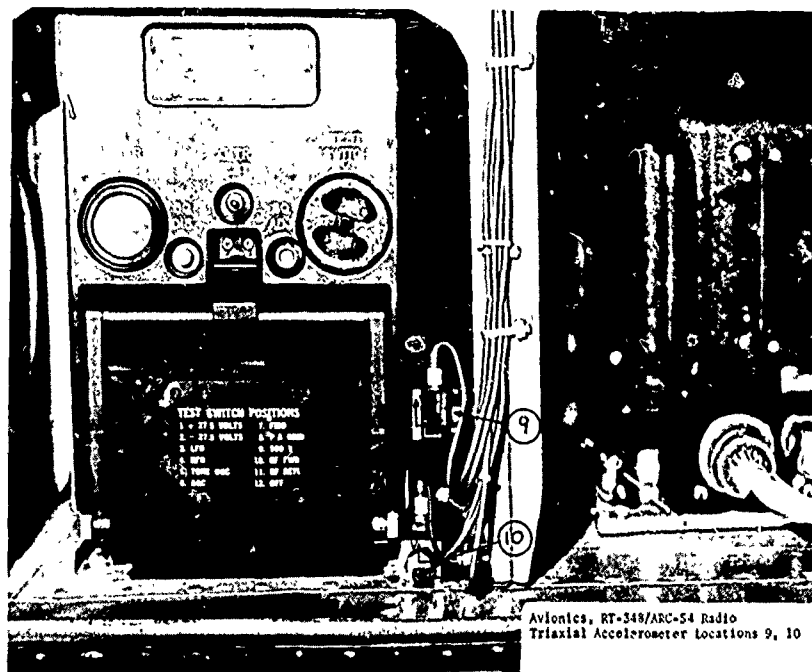
Instrument Panel
Triaxial Accelerometer Locations
1, 2, 3, 4, 5



Avionics, MD-1 Vertical Gyro
Triaxial Accelerometer Locations 6, 7
Thermocouple Location 1



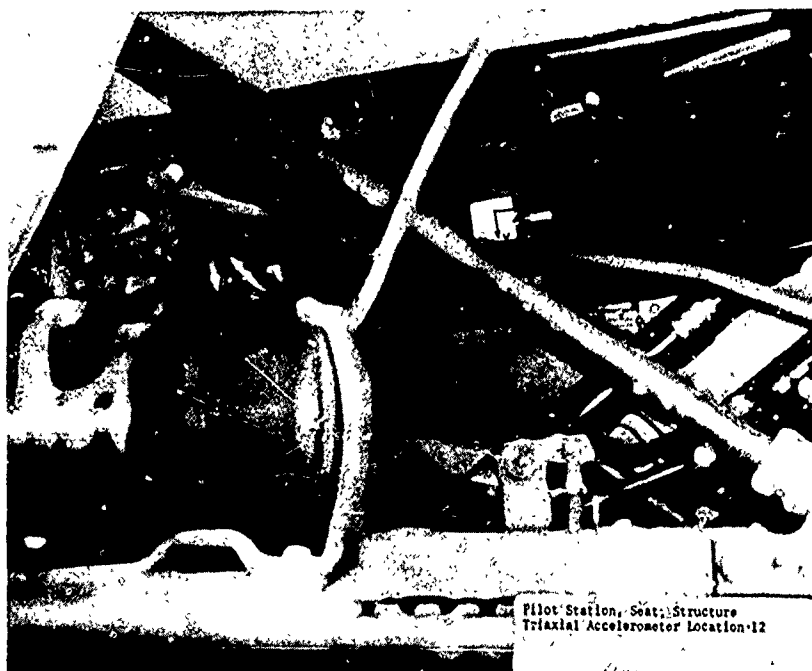
Avionics, Left Rear Compartment
Triaxial Accelerometer Location 8
Thermocouple Location 2



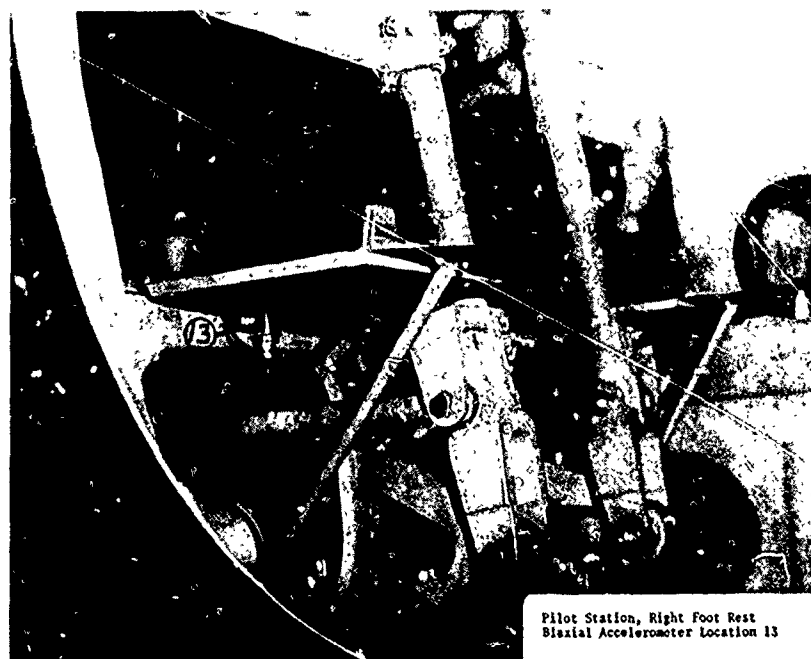
Avionics, RT-348/ARC-54 Radio
Triaxial Accelerometer Locations 9, 10



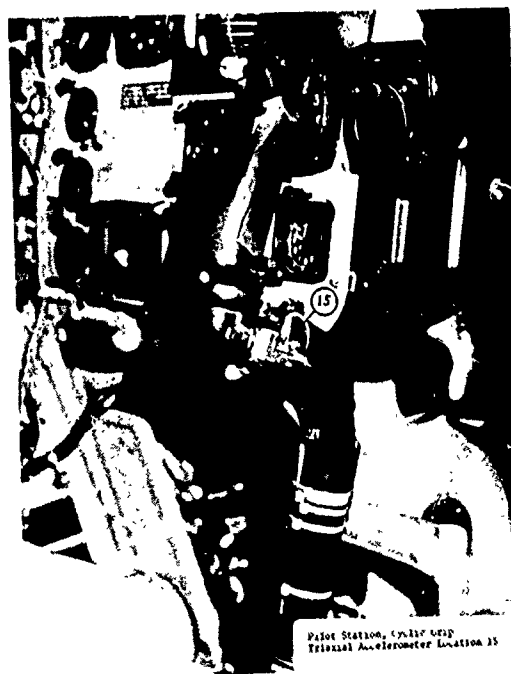
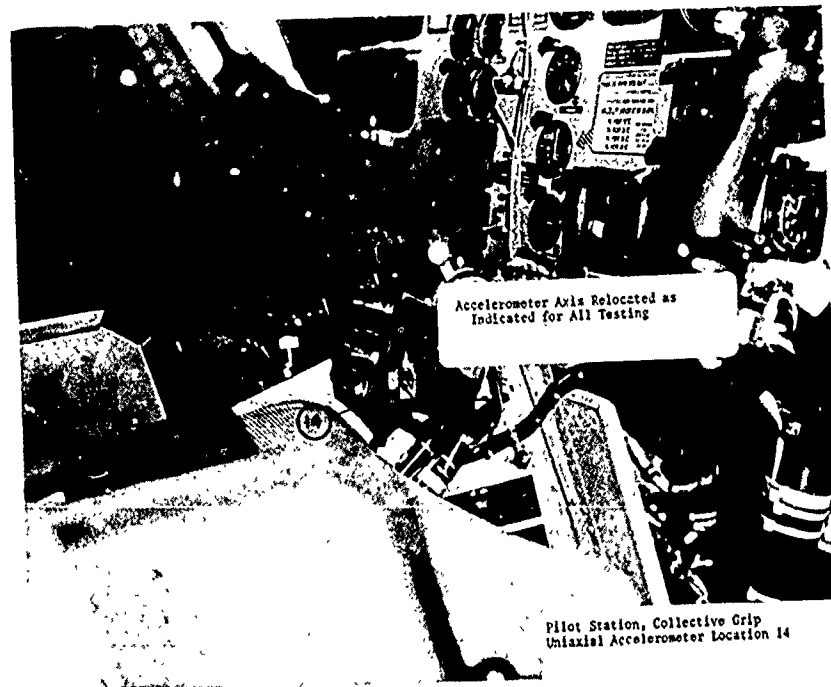
Pilot Station, Seat Pad
Triaxial Accelerometer Location 11

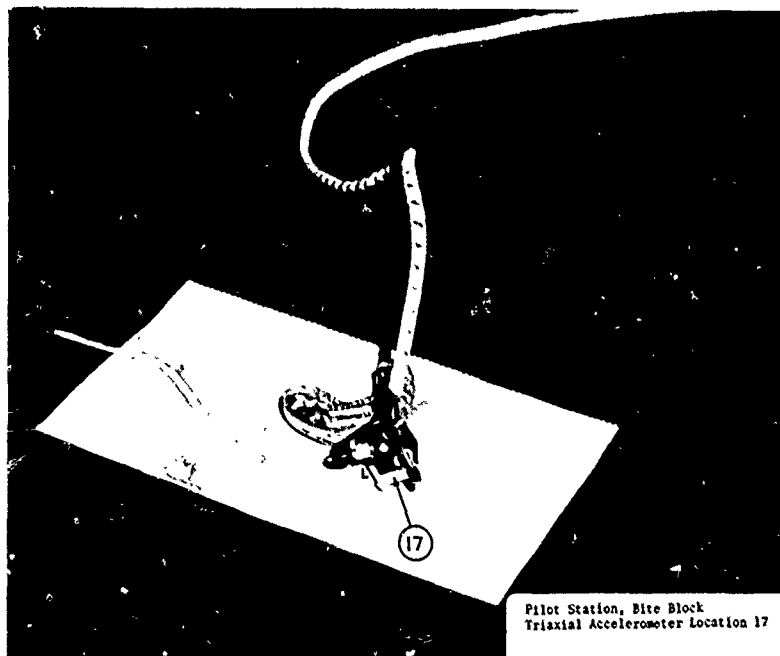
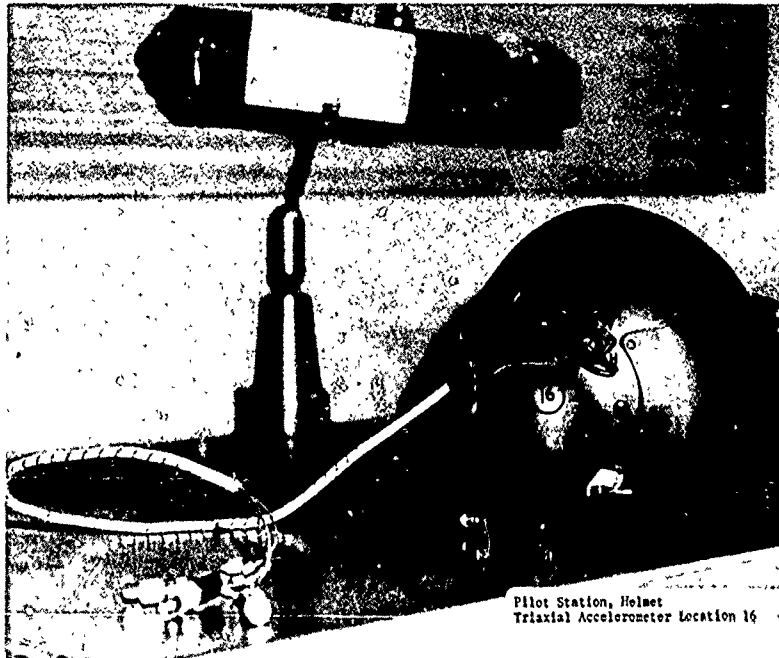


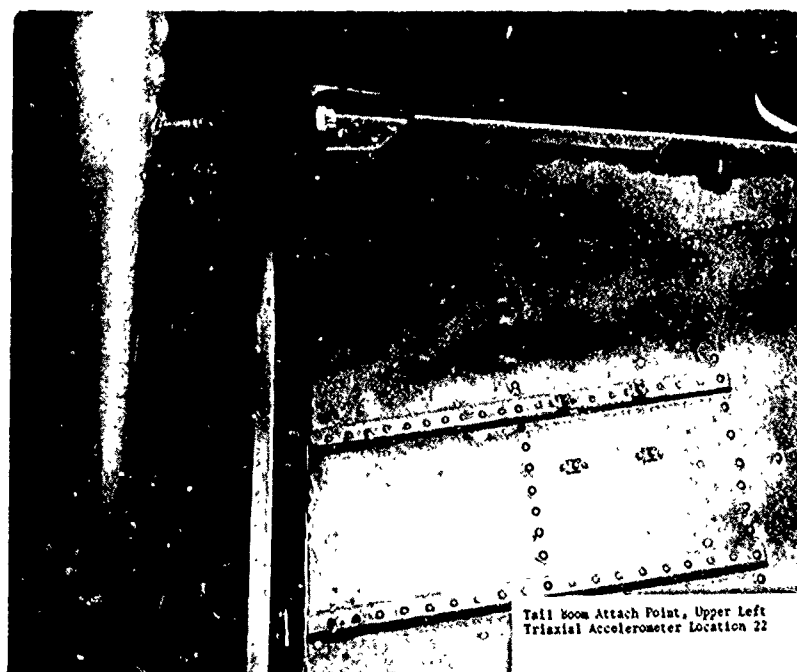
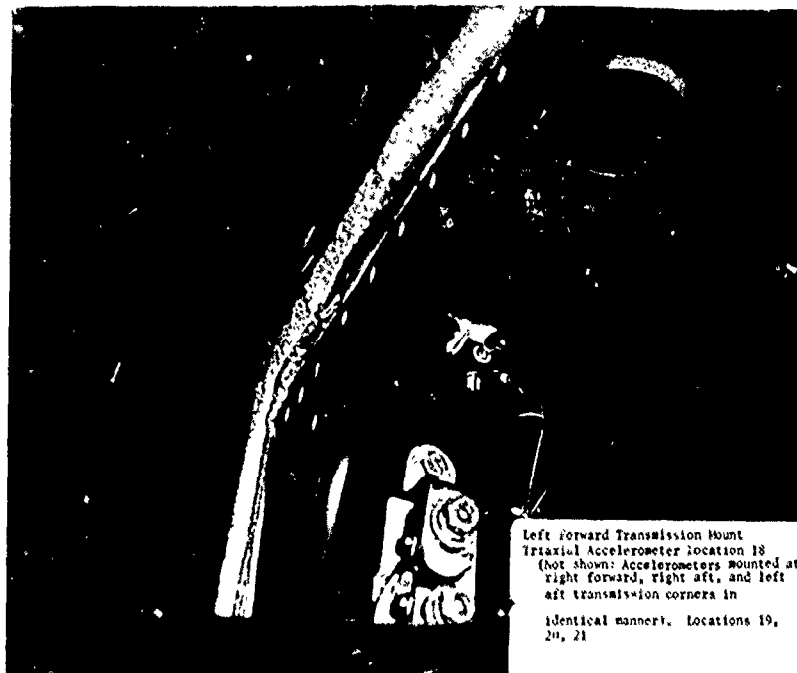
Pilot Station, Seat Structure
Triaxial Accelerometer Location 12

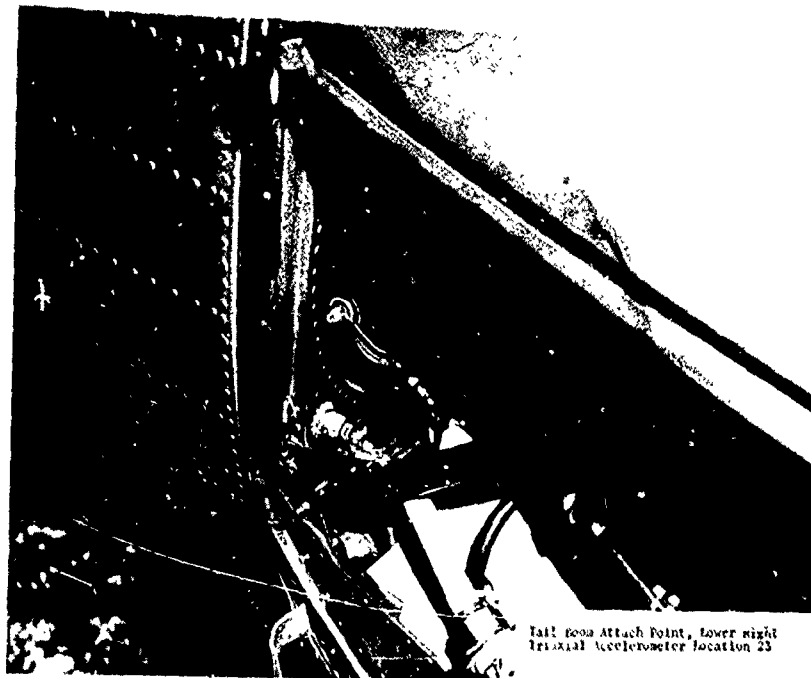


Pilot Station, Right Foot Rest
Biaxial Accelerometer Location 13

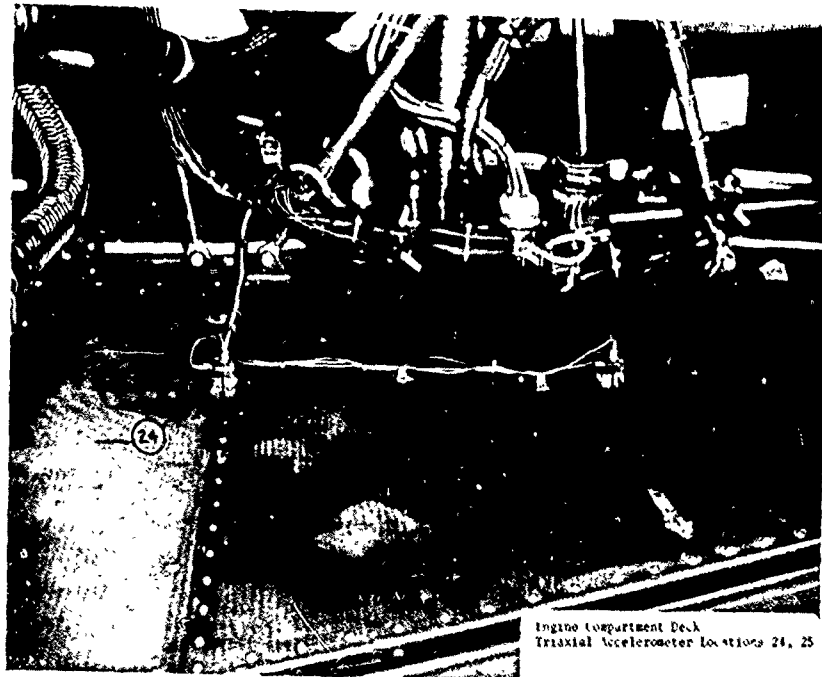




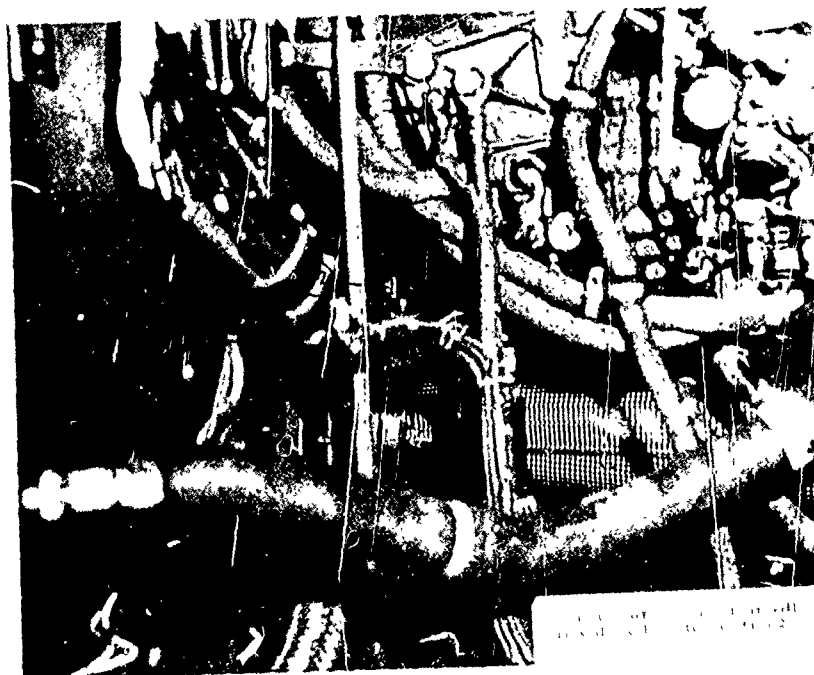
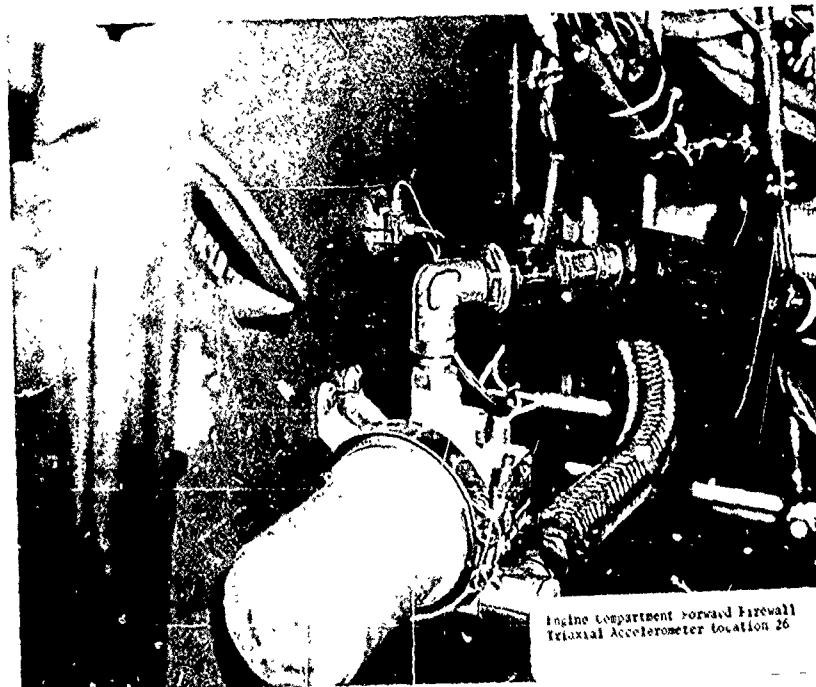


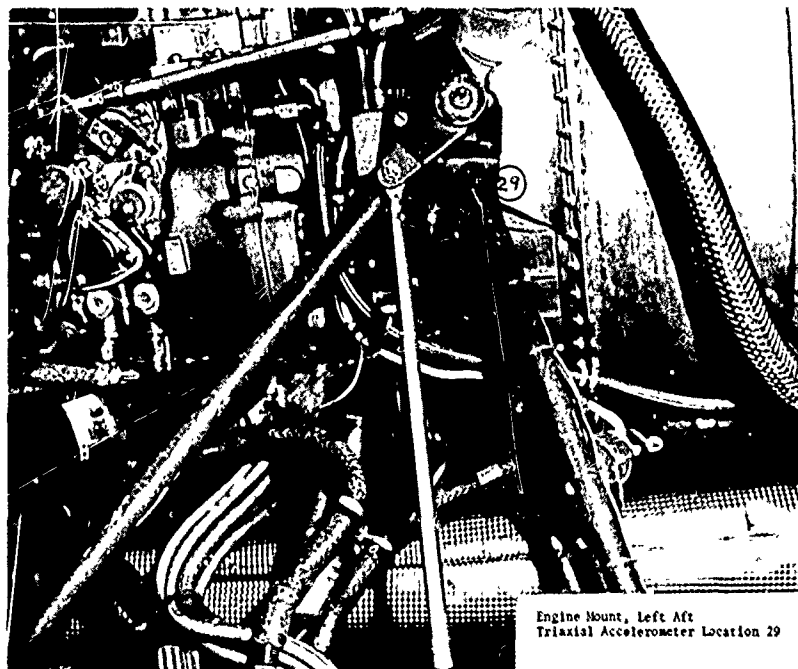
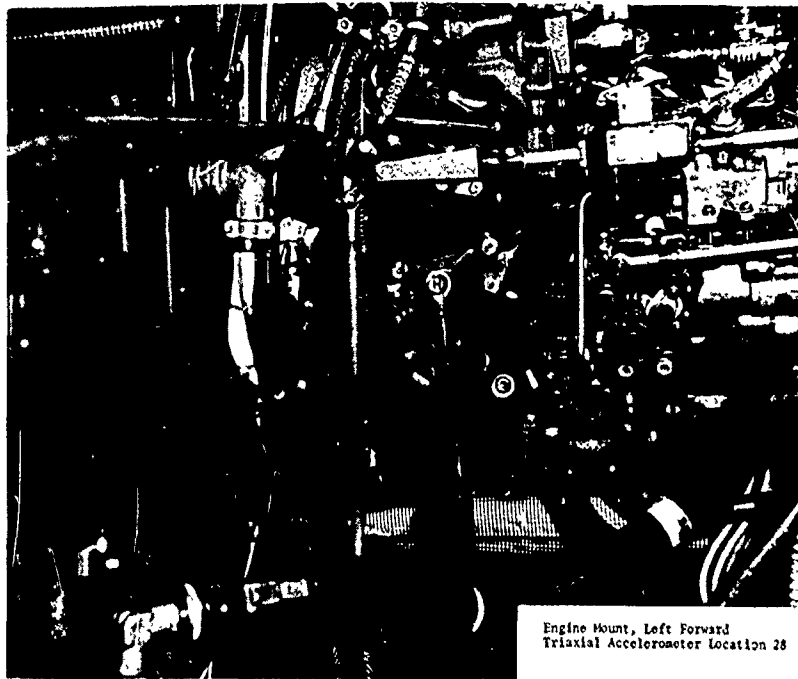


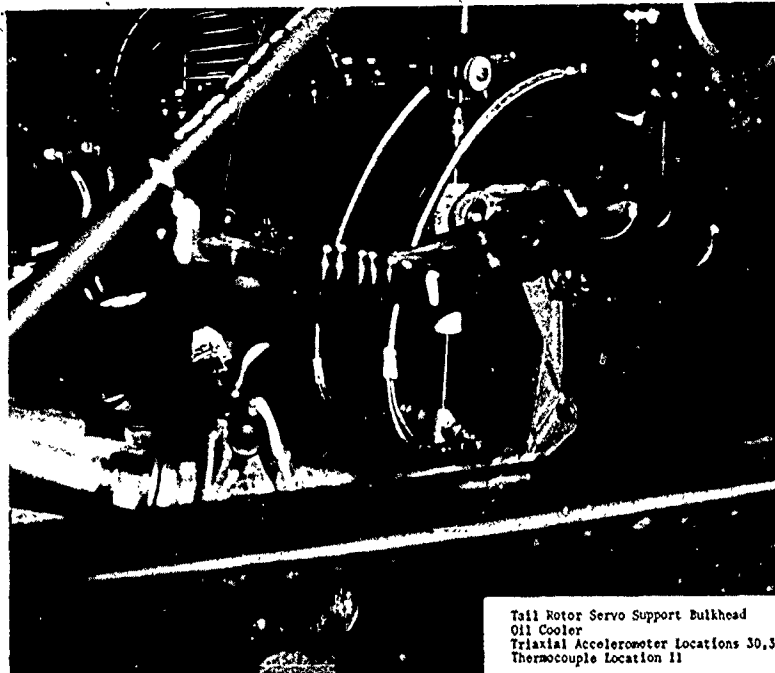
Tail Boom Attach Point, Lower Right
Triaxial Accelerometer location 23



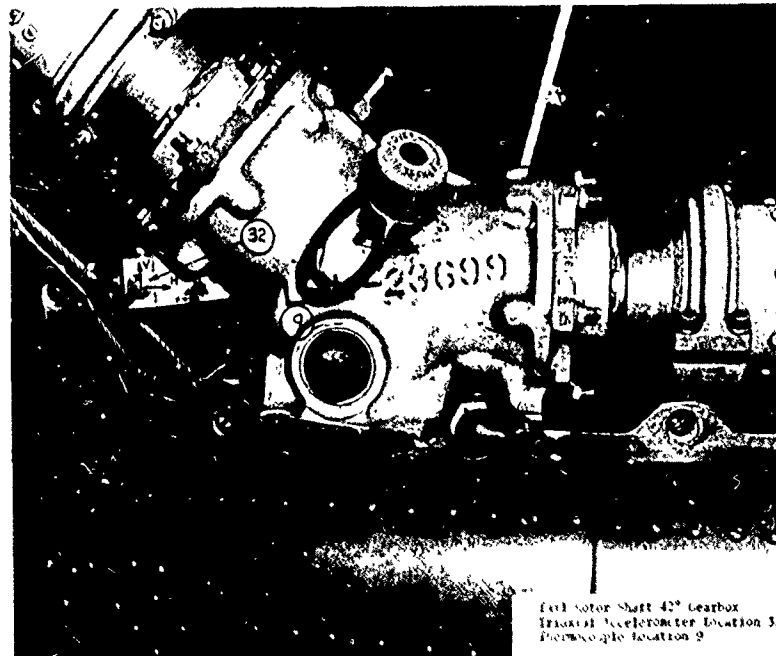
Engine Compartment Deck
Triaxial Accelerometer Locations 24, 25



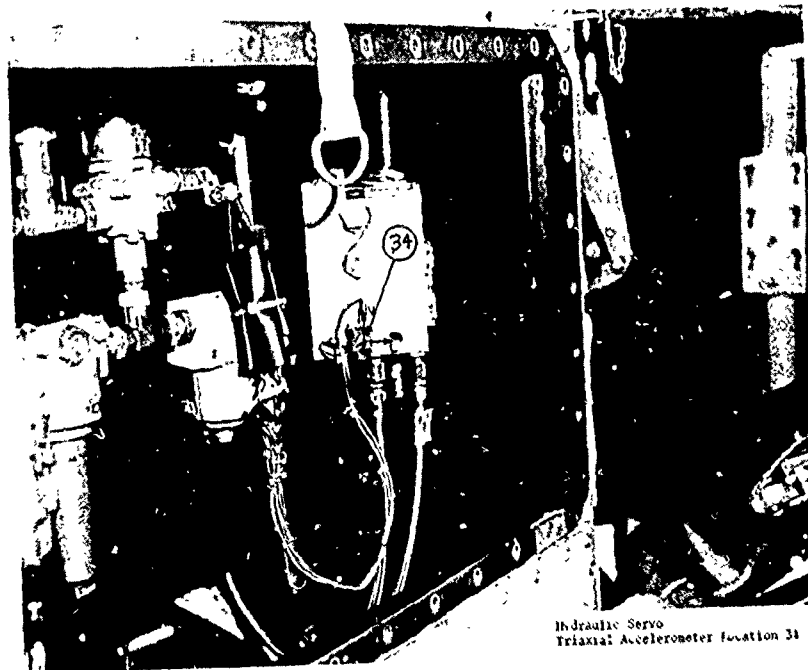
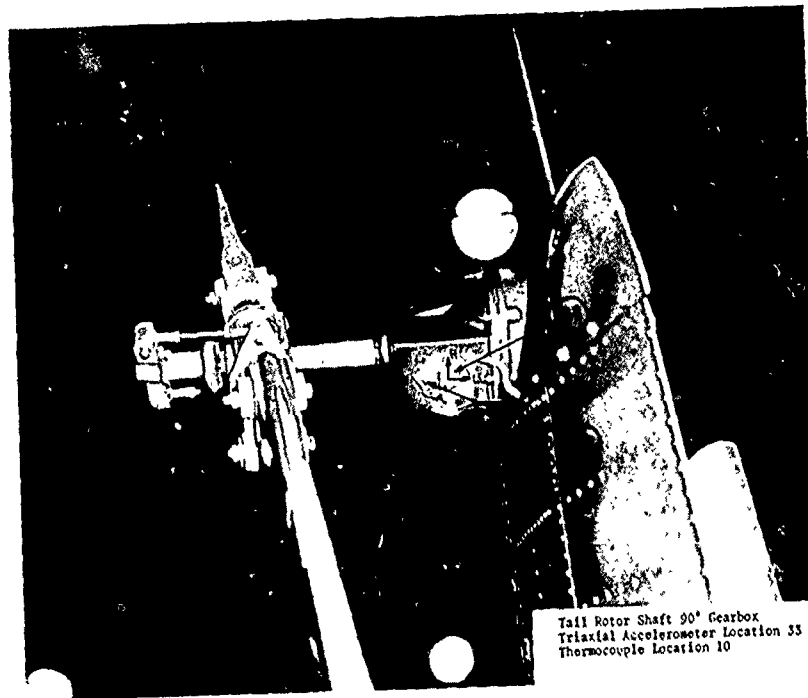


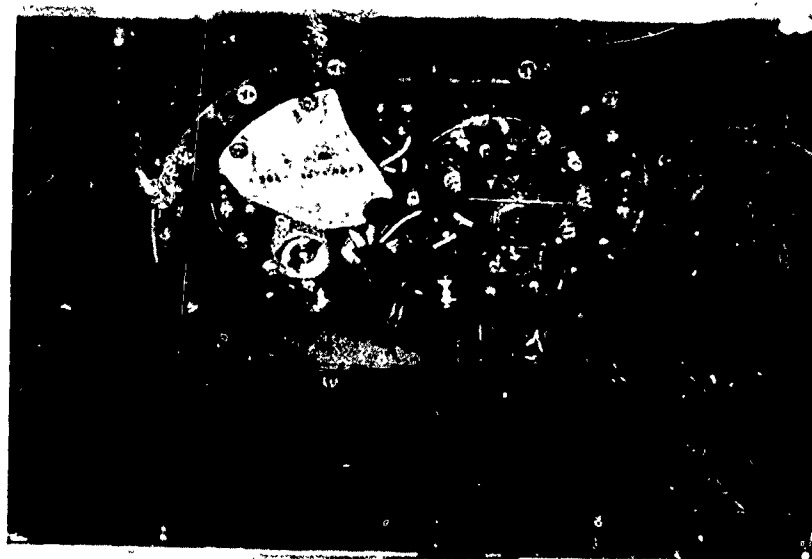


Tail Rotor Servo Support Bulkhead
Oil Cooler
Triaxial Accelerometer Locations 30,31
Thermocouple Location 11

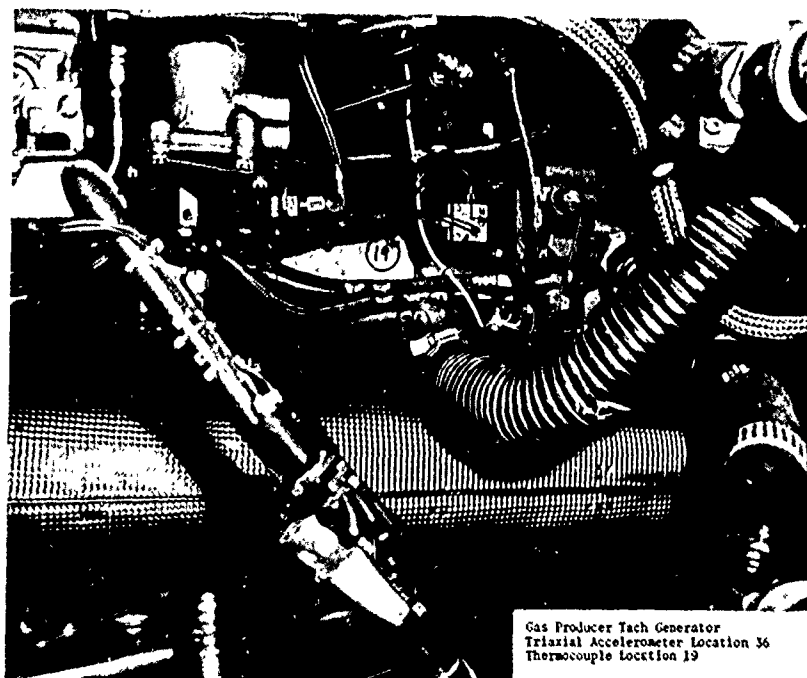


Tail Rotor Shaft 42nd Gearbox
Triaxial Accelerometer Location 32
Thermocouple Location 9

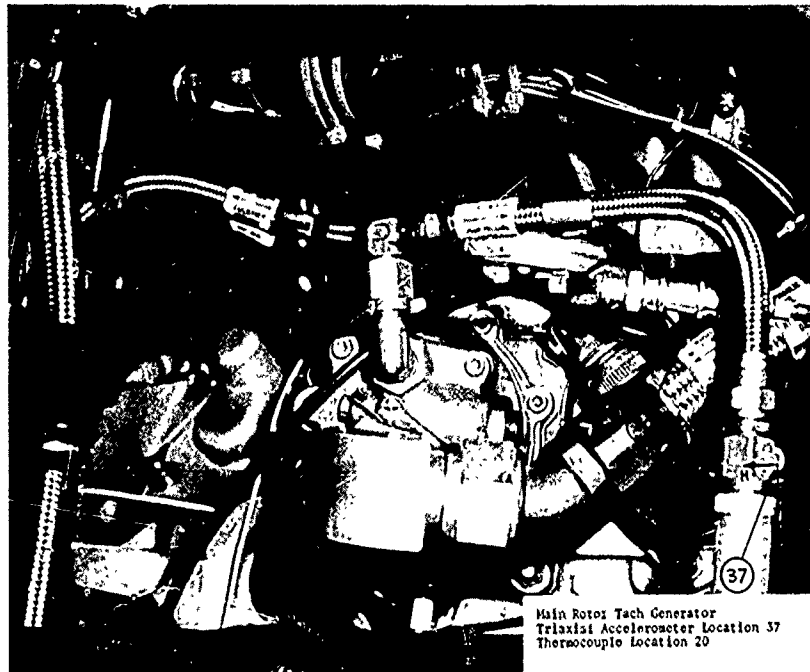




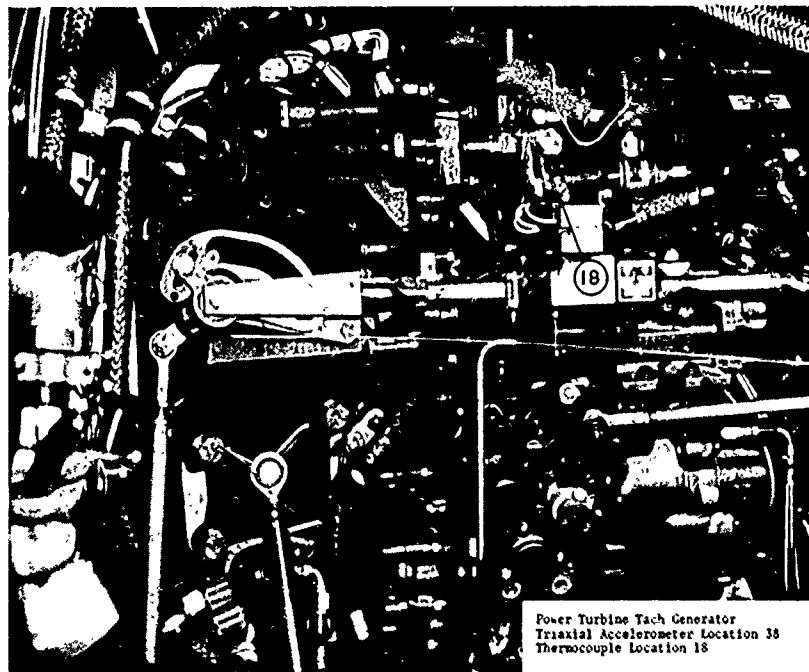
Right Fuel Boost Pump
Triaxial Accelerometer Location 35
Thermocouple Location 12



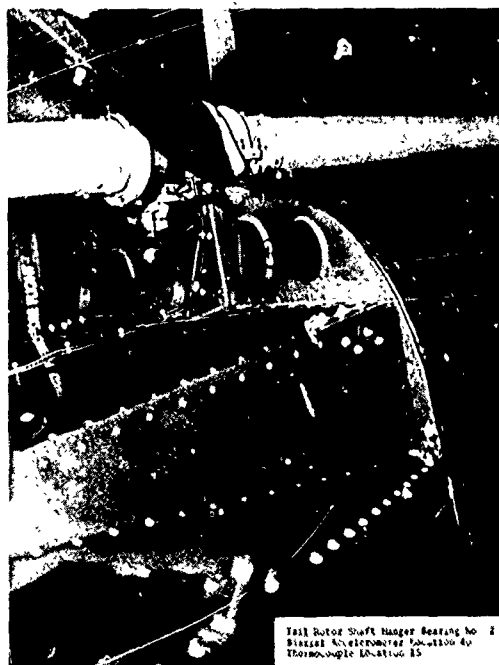
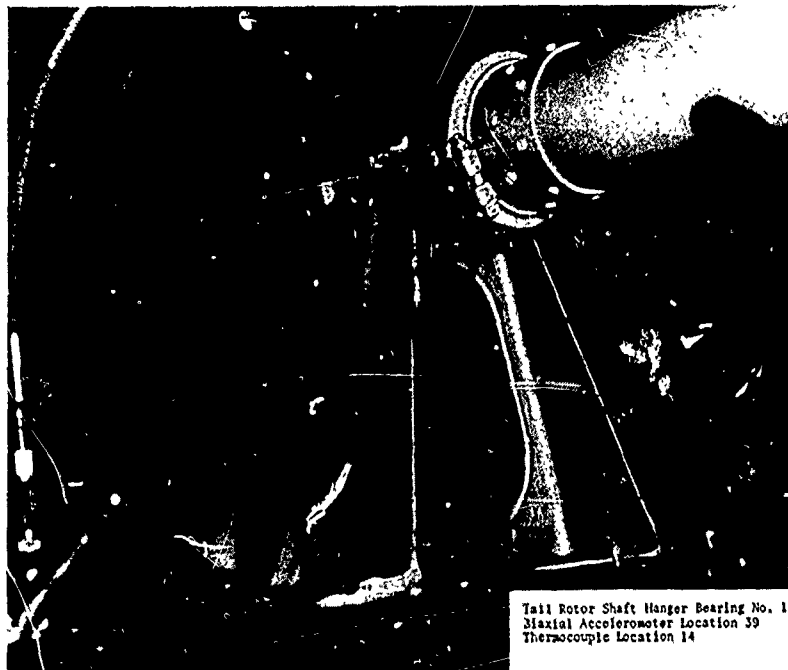
Gas Producer Tach Generator
Triaxial Accelerometer Location 36
Thermocouple Location 19

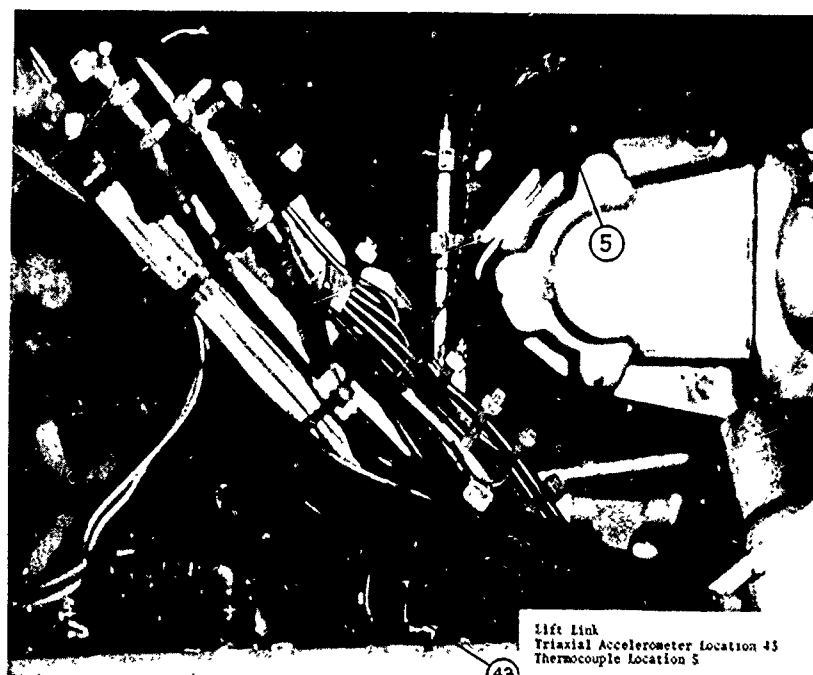
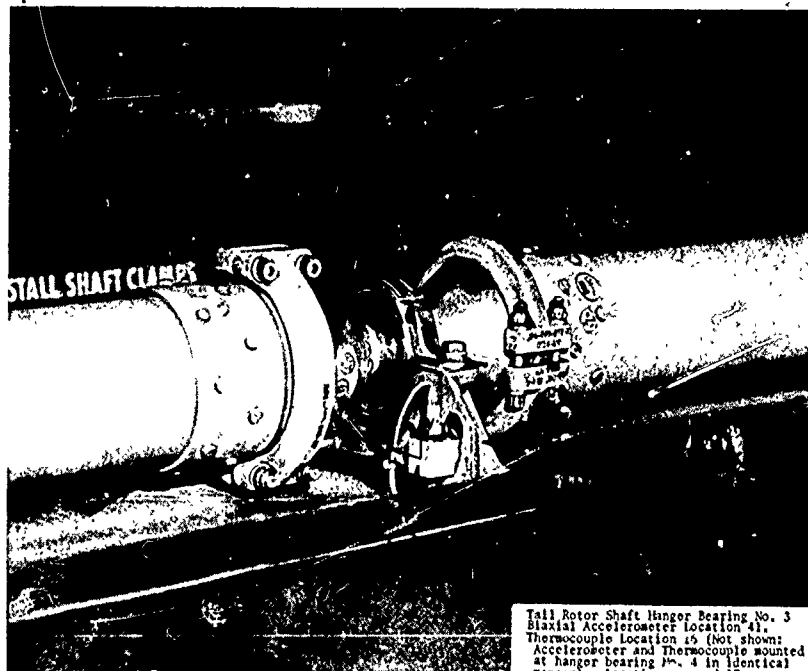


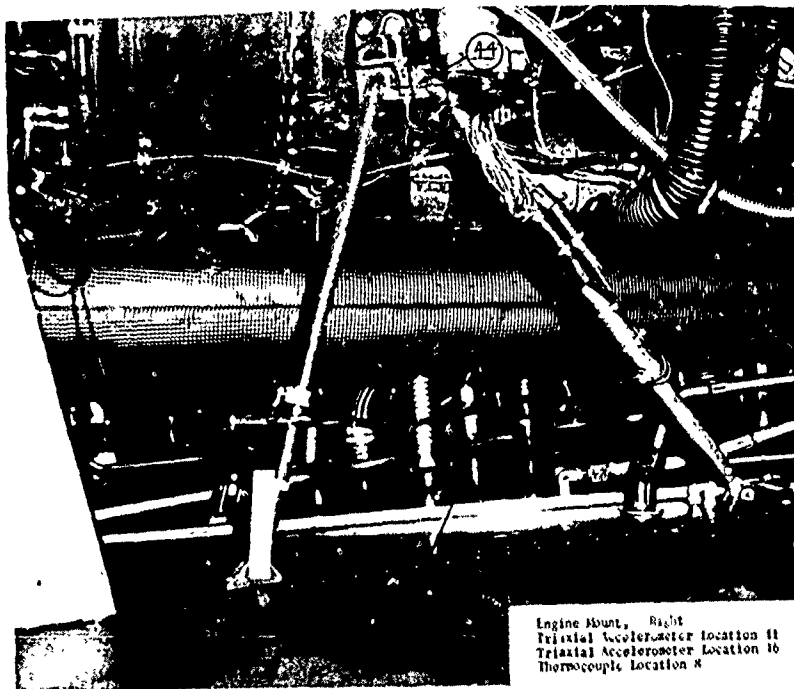
Main Rotor Tach Generator
Triaxial Accelerometer Location 37
Thermocouple Location 20



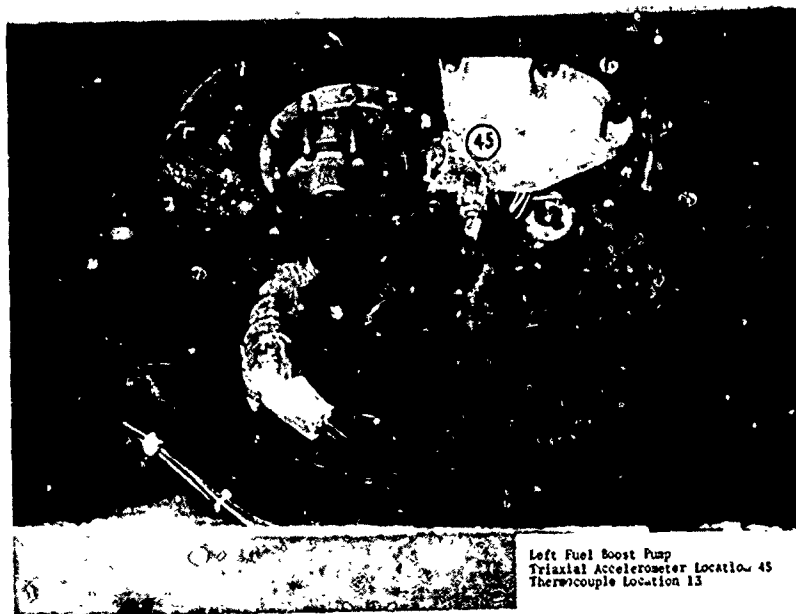
Power Turbine Tach Generator
Triaxial Accelerometer Location 38
Thermocouple Location 18



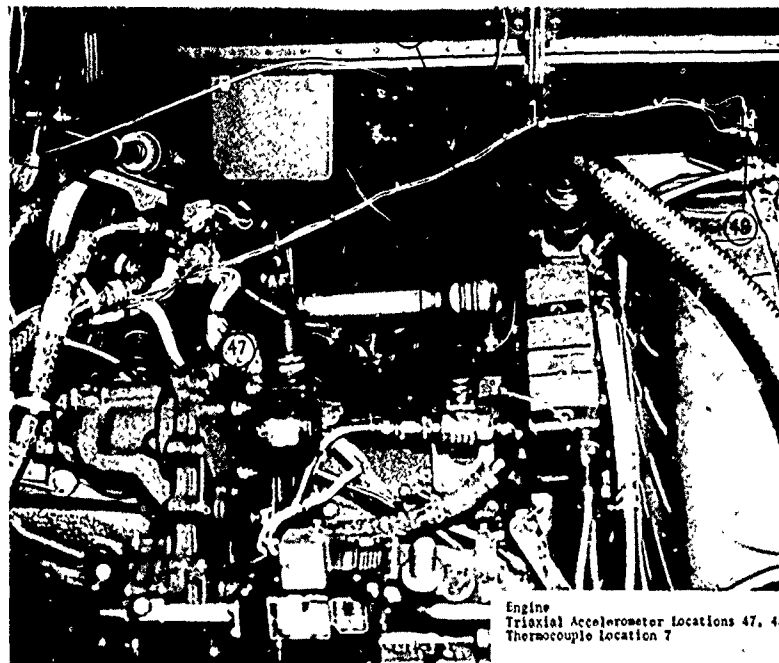




Engine Mount, Right
Triaxial Accelerometer Location 11
Triaxial Accelerometer Location 16
Thermocouple Location 8



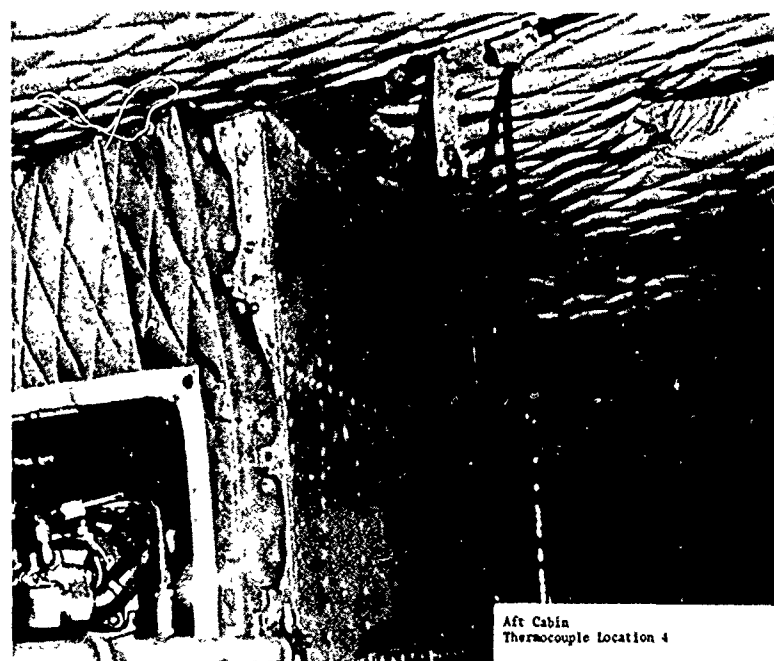
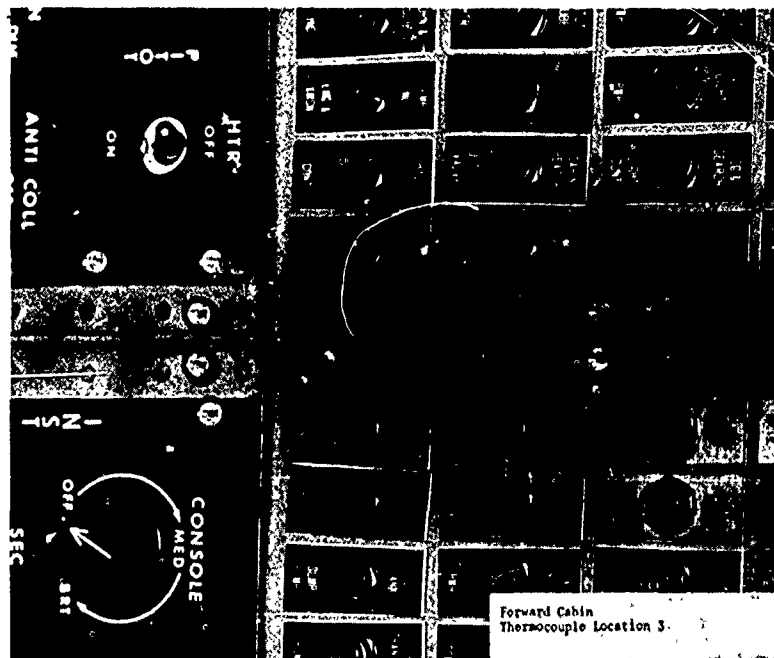
Left Fuel Boost Pump
Triaxial Accelerometer Location 45
Thermocouple Location 13

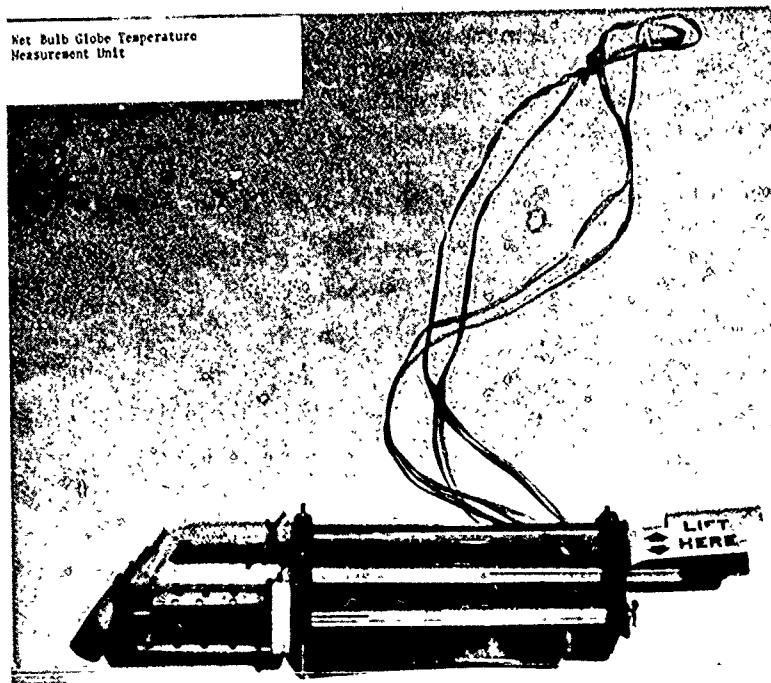
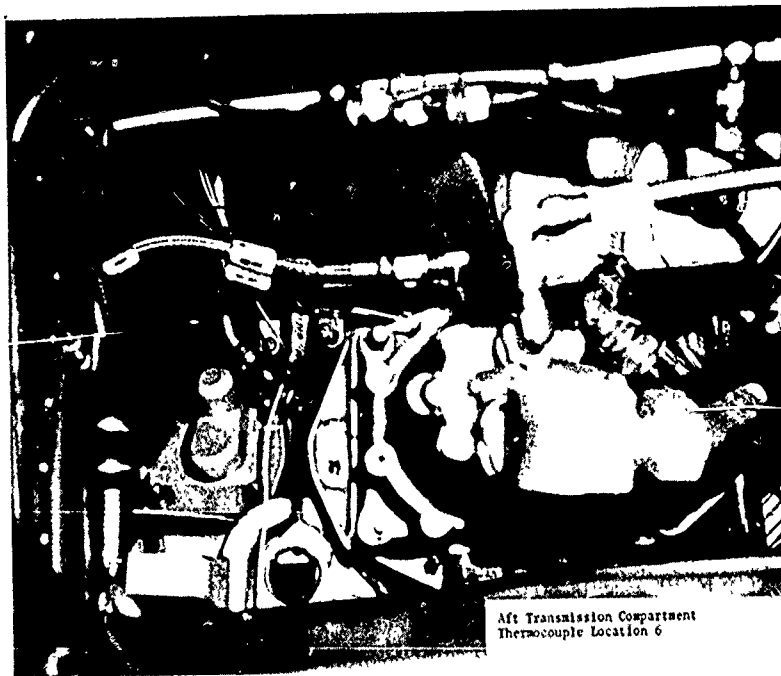


Engine
Triaxial Accelerometer Locations 47, 48
Thermocouple Location 7



Mass Mount
Triaxial Accelerometer Location 49





APPENDIX F. DATA REDUCTION METHODS

VIBRATION DATA

1. Because of the discrete frequency content of the data, a narrow-band spectral analysis was performed. A Spectral Dynamics 301 real-time spectral analyzer was utilized to perform the spectral analysis. This spectral analysis converted the data from the time domain (acceleration as a function of time) to the frequency domain (acceleration as a function of frequency). The output of the spectral analysis was a digital plot of acceleration versus frequency composed of acceleration values at 500 discrete frequencies uniformly spaced over the selected frequency range of the spectrum analyzer. The data were analyzed over two frequency ranges: zero to 500 Hz for instruments, avionics, and the pilot station, and zero to 2000 Hz for all other locations with resolution bandwidths of 1 Hz and 4 Hz, respectively. The zero-to-500-Hz analysis range was utilized for all instruments, avionics, and pilot station data, since there were no data of interest above 500 Hz, and the frequency resolution was better on the 500-Hz range than on the 2000-Hz range. The zero-to-2000-Hz analysis range was used for all other locations, since there were significant data above 500 Hz and the maximum instrumentation frequency response was 2000 Hz. Because of the random variation in amplitude, the data were averaged over a period of time to determine the mean acceleration amplitude for each test condition. This data averaging was accomplished with a Spectral Dynamics 302B ensemble averager. Data were averaged over an 8-second time interval for steady-state nonweapons-firing flight conditions, a 2-second interval for maneuvering flight, and a 2-second interval for weapons firing. The 2-second maneuvering flight analysis time interval was selected to cover the most severe vibrations encountered during the maneuver.

2. The following equations were used to calculate the acceleration mean and standard deviation values:

a. Mean (\bar{X}):

$$\bar{X} = \frac{\sum_{j=1}^N X_j}{N}$$

b. Standard deviation (S):

$$S = \sqrt{\frac{\sum_{j=1}^N (X_j - \bar{X})^2}{N}}$$

c. Mean plus standard deviation (Y):

$$Y = \bar{X} + S$$

Where: X_j = acceleration at a specific frequency

N = number of records compressed

3. Figures 1 and 2 are block diagrams of the spectral analysis and data compression procedures.

TEMPERATURE DATA

4. The electrical analogue shown in figure 3 was developed to predict the temperature of the cabin and avionics under static conditions at values of ambient air temperature and external radiation different than those tested. The results of this analysis are presented in figures 136 through 144, appendix G.

FIGURE 1
PROJECT 70-15 VIBRATION DATA
SPECTRAL ANALYSIS PROCEDURE

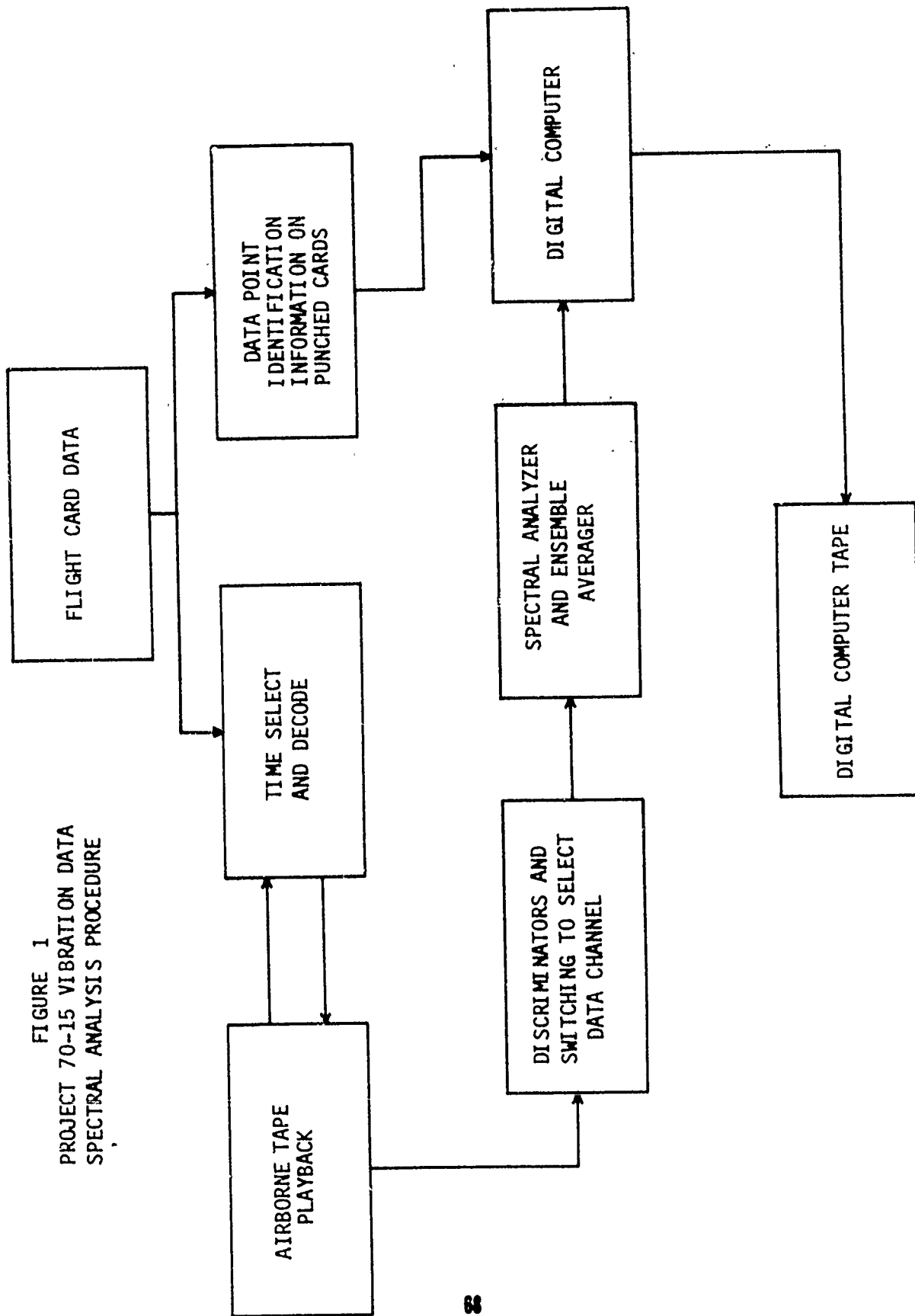
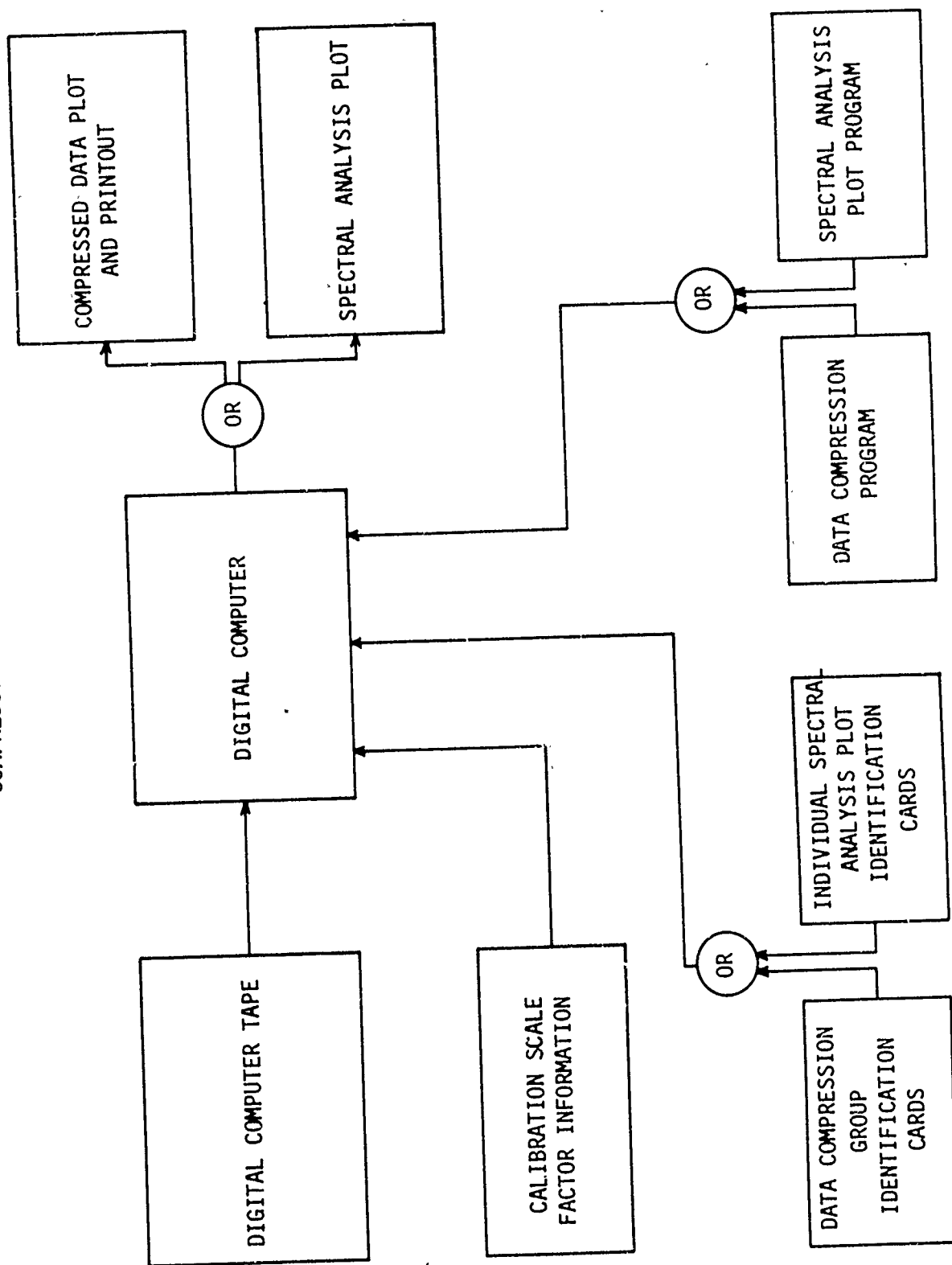


FIGURE 2
PROJECT 70-15 VIBRATION DATA
COMPRESSION PROCEDURE



<u>ELECTRICAL QUANTITY</u>	<u>HEAT TRANSFER QUANTITY</u>	<u>UNIT (°K)</u>
$V \sim$ Voltage	$T_a \sim$ Ambient air temperature	°K
$V_c \sim$ Voltage across capacitor	$T_c \sim$ Transient temperature inside helicopter	°K
	$T_{ss} \sim$ Steady-state temperature inside helicopter	°K
	$T_o \sim$ Initial temperature inside helicopter	°K
$R_1 \sim$ Resistance	$K_c \sim$ Conduction coefficient	Hr · °K/BTU
$R_1 \sim$ Resistance	$K_r \sim$ Radiation heat transfer coefficient	Hr · °K/BTU
$C \sim$ Capacitor	$C \sim$ Heat capacity	BTU/°C
$I \sim$ Current	$E_{ex} \sim$ Total external radiation	BTU/hr
	$E_a \sim$ Atmospheric radiation (total external radiation minus solar radiation)	BTU/hr
	$F_s \sim$ Solar radiation	BTU/hr
$t \sim$ Time	$t \sim$ Time	Hr

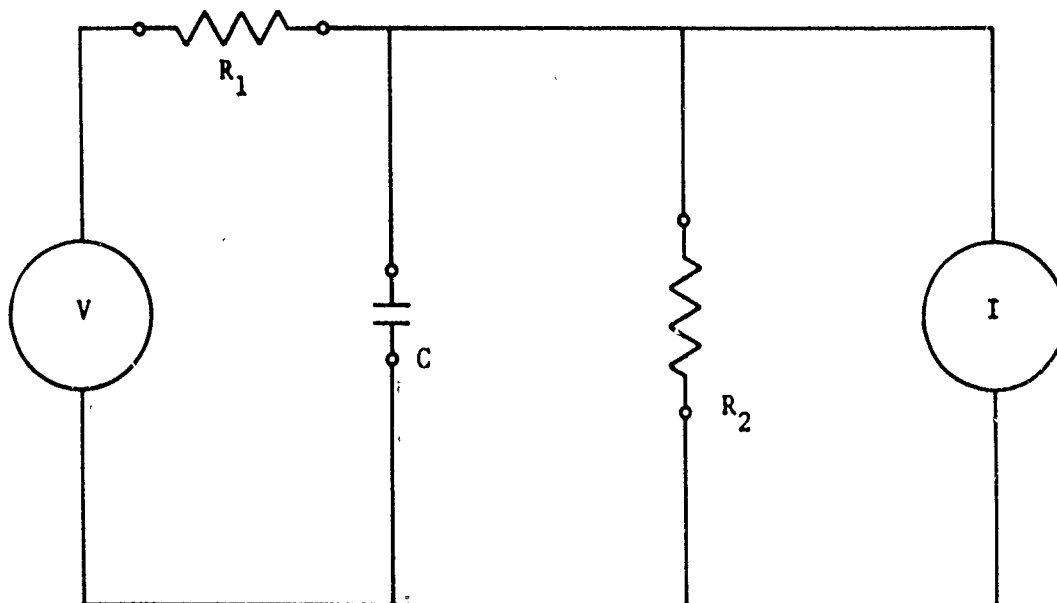


Figure 3. Heat Transfer Electrical Analog.

5. Using the circuit shown in figure 3, the equation describing the transient response of the helicopter to an ambient air temperature and source of external radiation can be written as:

$$T_c = e^{-t/K_{eq}C} \left[T_o - \frac{T_a K_r + E_{ex} K_c K_r}{K_c + K_r} \right] + \frac{T_a K_r + E_{ex} K_c K_r}{K_c + K_r} \quad (1)$$

Where: $K_{eq} = \frac{K_c K_r}{K_c + K_r}$

When t (time) $\rightarrow \infty$ the steady-state helicopter temperature T_{ss} is given by:

Where: $T_{ss} = \frac{T_a K_r + E_{ex} K_c K_r}{K_c + K_r} \quad (2)$

$$E_{ex} = E_s + \sigma T_a^4$$

$$\sigma = 1.8 \times 10^{-8} \text{ BTU/ft}^2\text{-hour} \cdot ^\circ\text{K}^4$$

6. Equation 2 was used to find K_c and K_r by allowing the helicopter to reach its steady-state temperature at two different constant ambient air temperatures (T_{a1} and T_{a2}) and at two different external radiation values (E_{ex1} and E_{ex2}). This resulted in two equations with two unknowns, K_c and K_r , which were solved for K_c and K_r , equations 3 and 4.

$$K_c = \frac{T_{a2} T_{ss1} - T_{a1} T_{ss2}}{E_{ex1} T_{ss2} - E_{ex2} T_{ss1}} \quad (3)$$

$$K_r = \frac{T_{ss1} K_c}{T_{a1} + E_{ex1} K_c - T_{ss1}} \quad (4)$$

7. A different K_C and K_T were calculated for each temperature sensor location. Each location was considered to comprise an area of 1 square foot which enabled the measured external radiation value in units of BTU/ft²-hr to be converted to BTU/hr. These values of K_C and K_T were then inserted into equation 2 in order to calculate the steady-state temperature at each temperature sensor location for different values of solar radiation and ambient air temperature than those tested (figs. 136 through 144, app G).

WET BULB GLOBE TEMPERATURE CALCULATION

8. The WBGT index is calculated from the following equation:

$$WBGT = 0.7WB + 0.2GT + 0.1DB$$

Where: WB = Naturally convected wet bulb temperature - °F

DB = Dry bulb temperature - °F

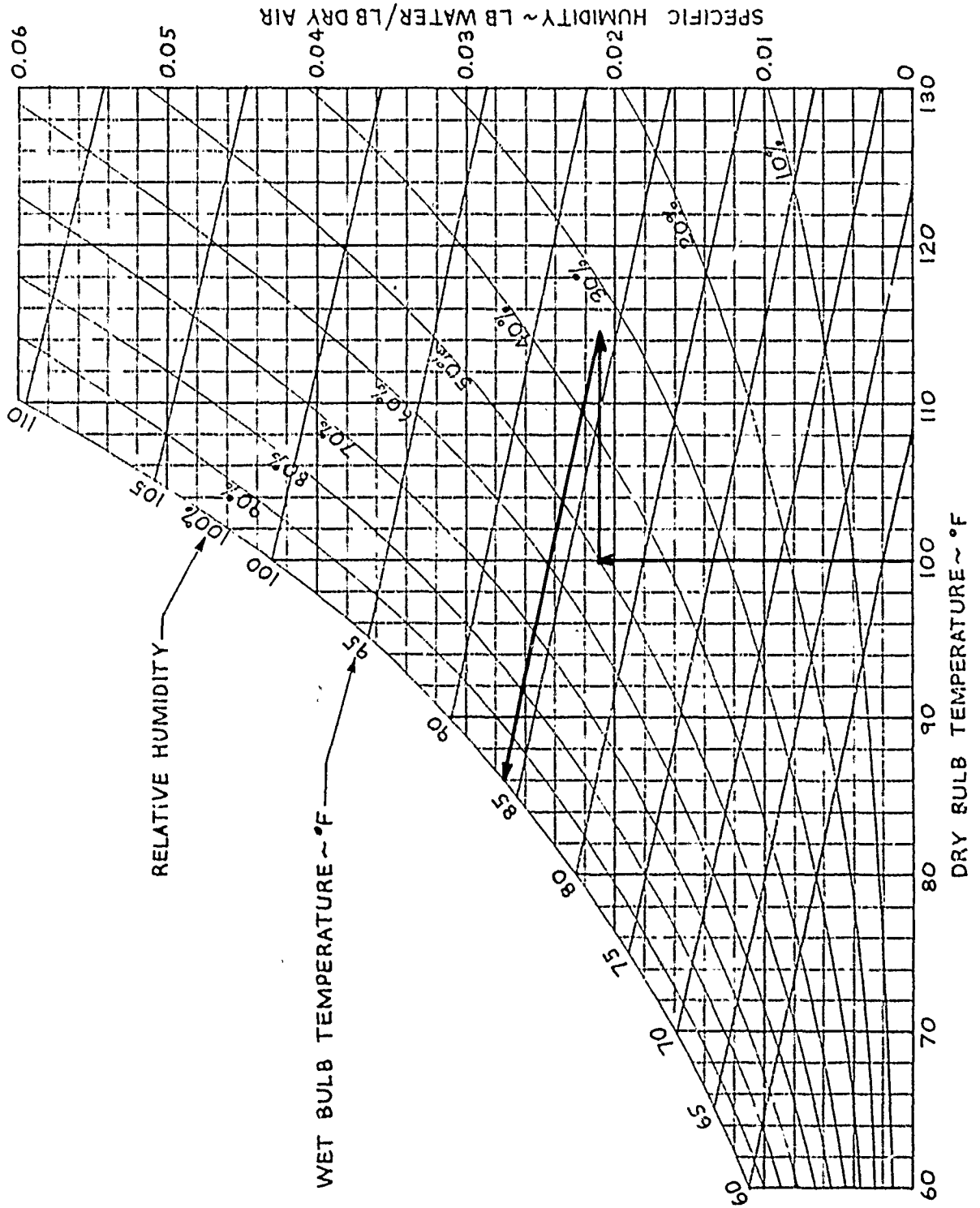
GT = Globe temperature - °F

For an outside air temperature of 100°F, a solar radiation value of 250 BTU/hr-ft² and an airspeed of 80 KCAS, a cabin temperature of 114.4°F and a globe temperature of 124.8°F can be determined from figure G. At a relative humidity of 50 percent at 100°F, a psychrometric chart can be used to determine a wet bulb temperature of 86.5°F for a cabin dry bulb temperature of 114.4°F. Using these temperature values, the WBGT can be calculated.

$$WBGT = (0.7)(86.5) + (0.2)(124.8) + (0.1)(114.4) = 97.0^\circ\text{F}$$

PSYCHROMETRIC CHART

BAROMETRIC PRESSURE 29.92 IN. Hg



APPENDIX G. TEST DATA

Index

<u>Figure (Compression Number)</u>	<u>Figure Number</u>
Data Compression Arrays	1 through 3
Instrument Vibrations, all Flight Conditions (402)	4 and 5
Avionics Vibrations, all Flight Conditions (403)	6 and 7
Pilot Vibration Input, all Flight Conditions (404)	8 and 9
Pilot Vibration, all Flight Conditions (405)	10 and 11
Transmission Mount Vibration, all Flight Conditions (406)	12 and 13
Tail Boom Vibrations, all Flight Conditions (407)	14 and 15
Engine Deck Vibrations, all Flight Conditions (408)	16 and 17
Engine Firewall Vibrations, all Flight Conditions (409)	18 and 19
Engine Mounts Vibrations, all Flight Conditions (410)	20 and 21
Tail Rotor Servo Vibrations, all Flight Conditions (411)	22 and 23
Oil Cooler Vibrations, all Flight Conditions (412)	24 and 25
42-Degree and 90-Degree Gearbox Vibrations, all Flight Conditions (413)	26 and 27
Hydraulic Servo Vibrations, all Flight Conditions (414)	28 and 29
Fuel Boost Pumps Vibrations, all Flight Conditions (415)	30 and 31
Tach Generator Vibrations, all Flight Conditions (416)	32 and 33
Hanger Bearing Vibrations, all Flight Conditions (417)	34 and 35
Lift Link Vibrations, all Flight Conditions (418)	36 and 37
Engine Vibrations, all Flight Conditions (419)	38 and 39
Instrument and Avionics Vibrations, Firing (437)	40 and 41
Instrument Vibrations, Firing (376)	42 and 43
Avionics Vibrations, Firing (377)	44 and 45
Pilot Vibration Input, Firing (378)	46 and 47
Pilot Vibration, Firing (379)	48 and 49
Transmission Mounts Vibration, Firing (380)	50 and 51
Tail Boom Vibrations, Firing (381)	52 and 53
Engine Deck Vibrations, Firing (382)	54 and 55
Engine Firewall Vibrations, Firing (383)	56 and 57

Engine Mounts Vibrations, Firing (384)	58 and 59
Tail Rotor Servo Vibrations, Firing (385)	60 and 61
Oil Cooler Vibrations, Firing (386)	62 and 63
42-Degree and 90-Inch Gearbox Vibrations, Firing (387)	64 and 65
Hydraulic Servo Vibrations, Firing (388)	66 and 67
Fuel Boost Pumps Vibrations, Firing (389)	68 and 69
Tach Generators Vibrations, Firing (390)	70 and 71
Hanger Bearings Vibrations, Firing (391)	72 and 73
Engine Vibrations, Firing (392)	74 and 75
Gun Mount Vibrations, Firing (393)	76 and 77
Lift Link Vibrations, Firing (401)	78 and 79
Instrument Vibrations, Hover (249)	80 and 81
Instrument Vibrations, Level Flight (250)	82 and 83
Instrument Vibrations, Climb (251)	84 and 85
Instrument Vibrations, Descent (252)	86 and 87
Instrument Vibrations, Takeoff and Landing (253)	88 and 89
Instrument Vibrations, Maneuvering (254)	90 and 91
Instrument Vibrations, Ground Run (255)	92 and 93
Avionics Vibrations, Hover (256)	94 and 95
Avionics Vibrations, Level Flight (257)	96 and 97
Avionics Vibrations, Climb (258)	98 and 99
Avionics Vibrations, Descent (259)	100 and 101
Avionics Vibrations, Takeoff and Landing (260)	102 and 103
Avionics Vibrations, Maneuvering (261)	104 and 105
Avionics Vibrations, Ground Run (262)	106 and 107
Pilot Vibration Input, Hover (263)	108 and 109
Pilot Vibration Input, Level Flight (264)	110 and 111
Pilot Vibration Input, Climb (265)	112 and 113
Pilot Vibration Input, Descent (266)	114 and 115
Pilot Vibration Input, Takeoff and Landing (267)	116 and 117
Pilot Vibration Input, Maneuvering (268)	118 and 119
Pilot Vibration Input, Ground Run (269)	120 and 121
Pilot Vibrations, Hover (270)	122 and 123
Pilot Vibrations, Level Flight (271)	124 and 125
Pilot Vibrations, Climb (272)	126 and 127
Pilot Vibrations, Descent (273)	128 and 129

Pilot Vibrations, Takeoff and Landing (274)	130 and 131
Pilot Vibrations, Maneuvering (275)	132 and 133
Pilot Vibrations, Ground Run (276)	134 and 135
Forward Avionics Static Temperature	136
Forward Cabin Static Temperature	137
Aft Cabin Static Temperature	138
Engine Compartment Static Temperature	139
42-Degree Gearbox Static Temperature	140
No. 1 Hanger Bearing Static Temperature	141
No. 2 Hanger Bearing Static Temperature	142
No. 3 Hanger Bearing Static Temperature	143
No. 4 Hanger Bearing Static Temperature	144

FIGURE 1

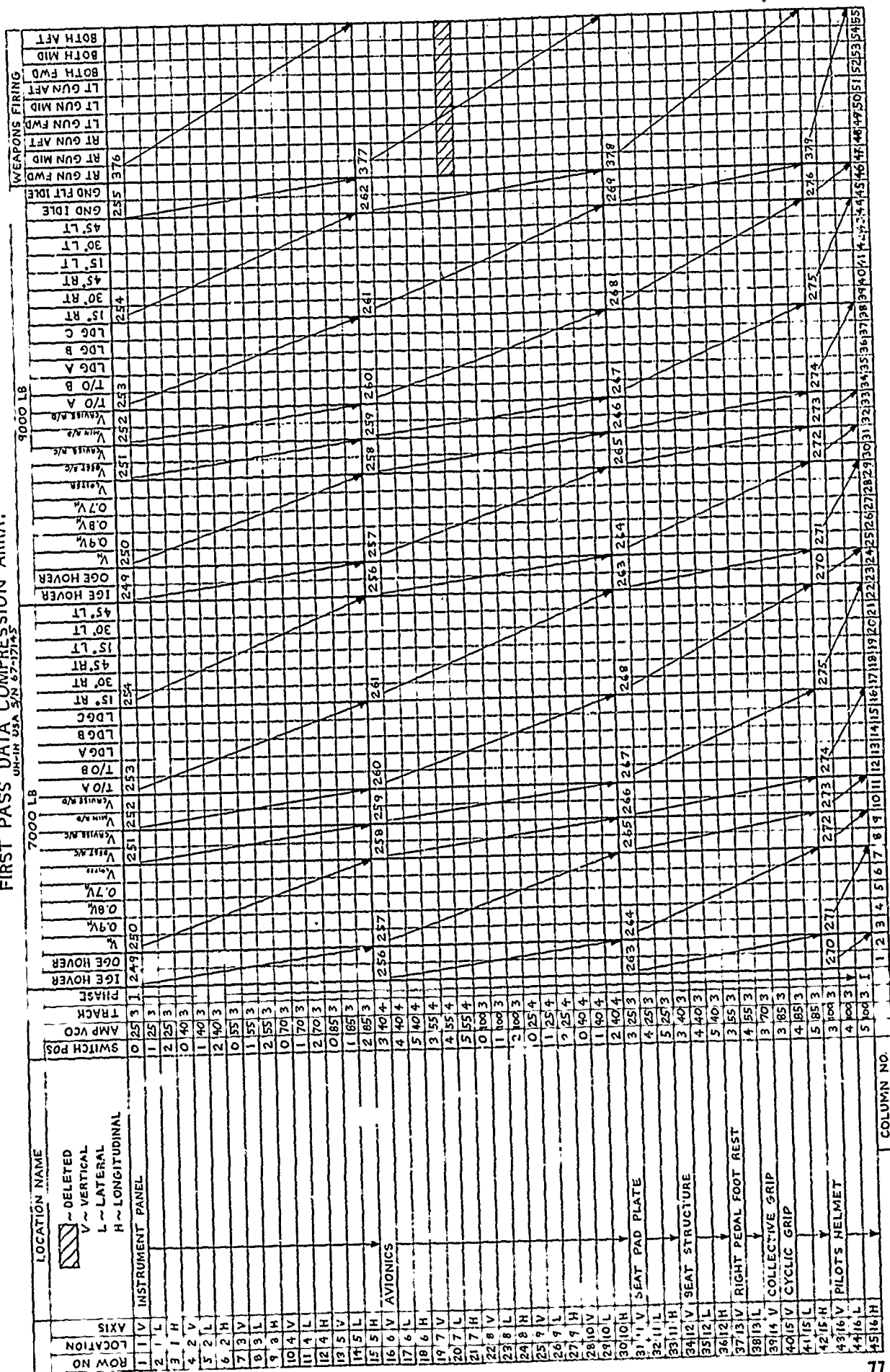


FIGURE 1
FIRST PASS DATA COMPRESSION ARRAY

PAGE 2 OF 4

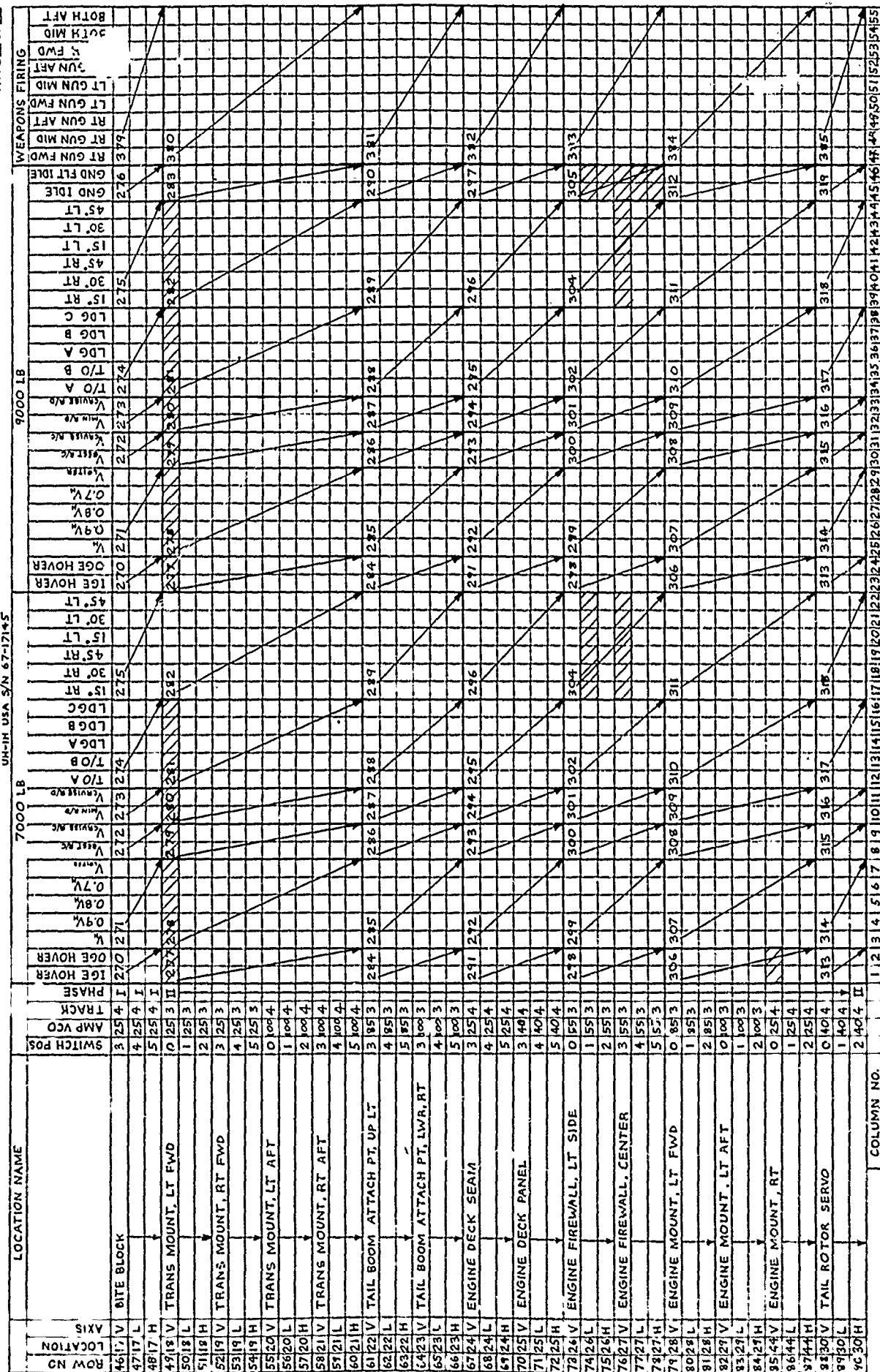


FIGURE 1
FIRST PASS DATA COMPRESSION ARRAY

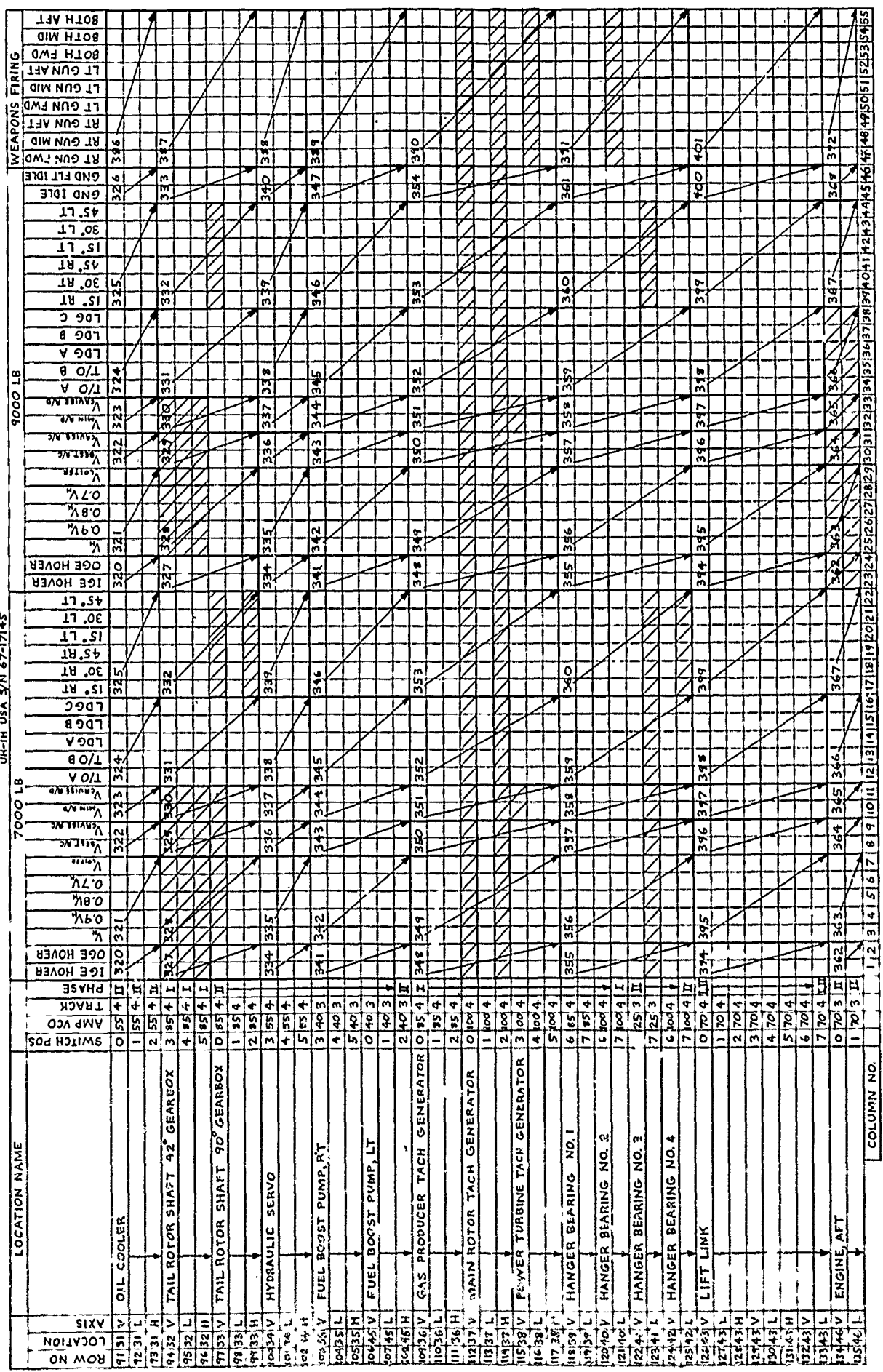


FIGURE 1
FIRST PASS DATA COMPRESSION ARRAY

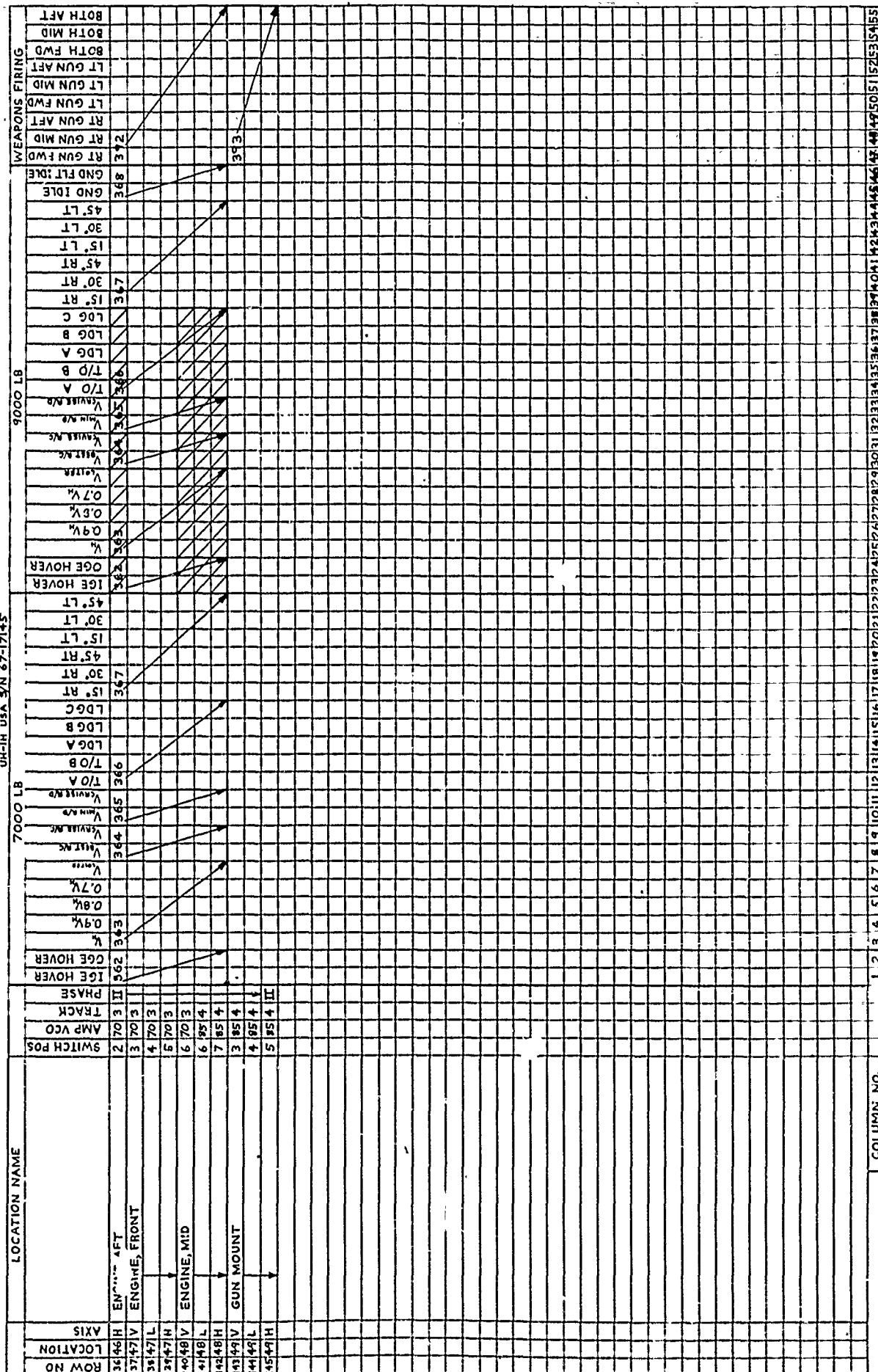


FIGURE 2

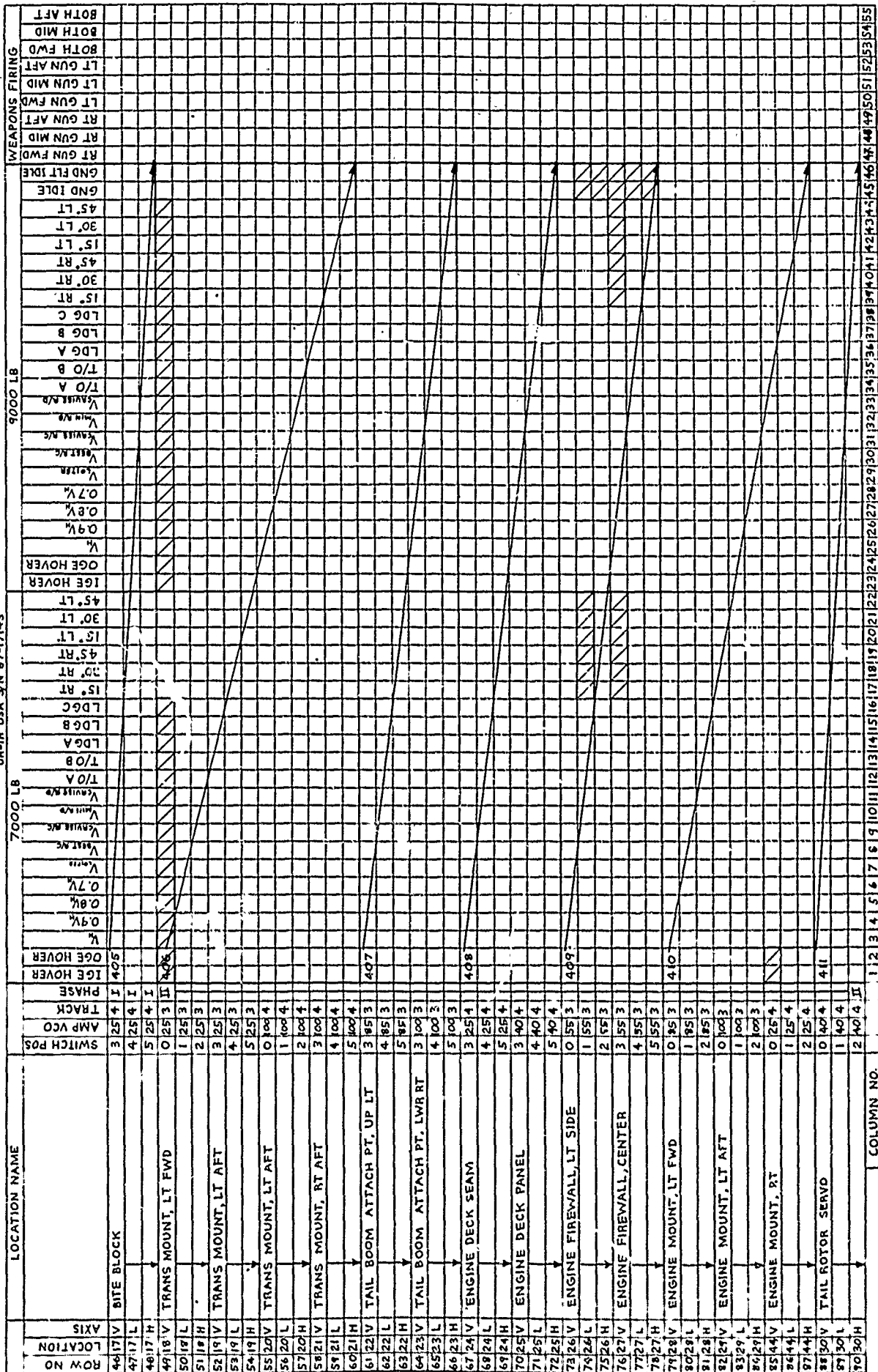


FIGURE 2
SECOND PASS DATA COMPRESSION ARRAY
UH-1H USA S/N 67-17145

[illegible]

FIGURE 2
SECOND PASS DATA COMPRESSION ARRAY

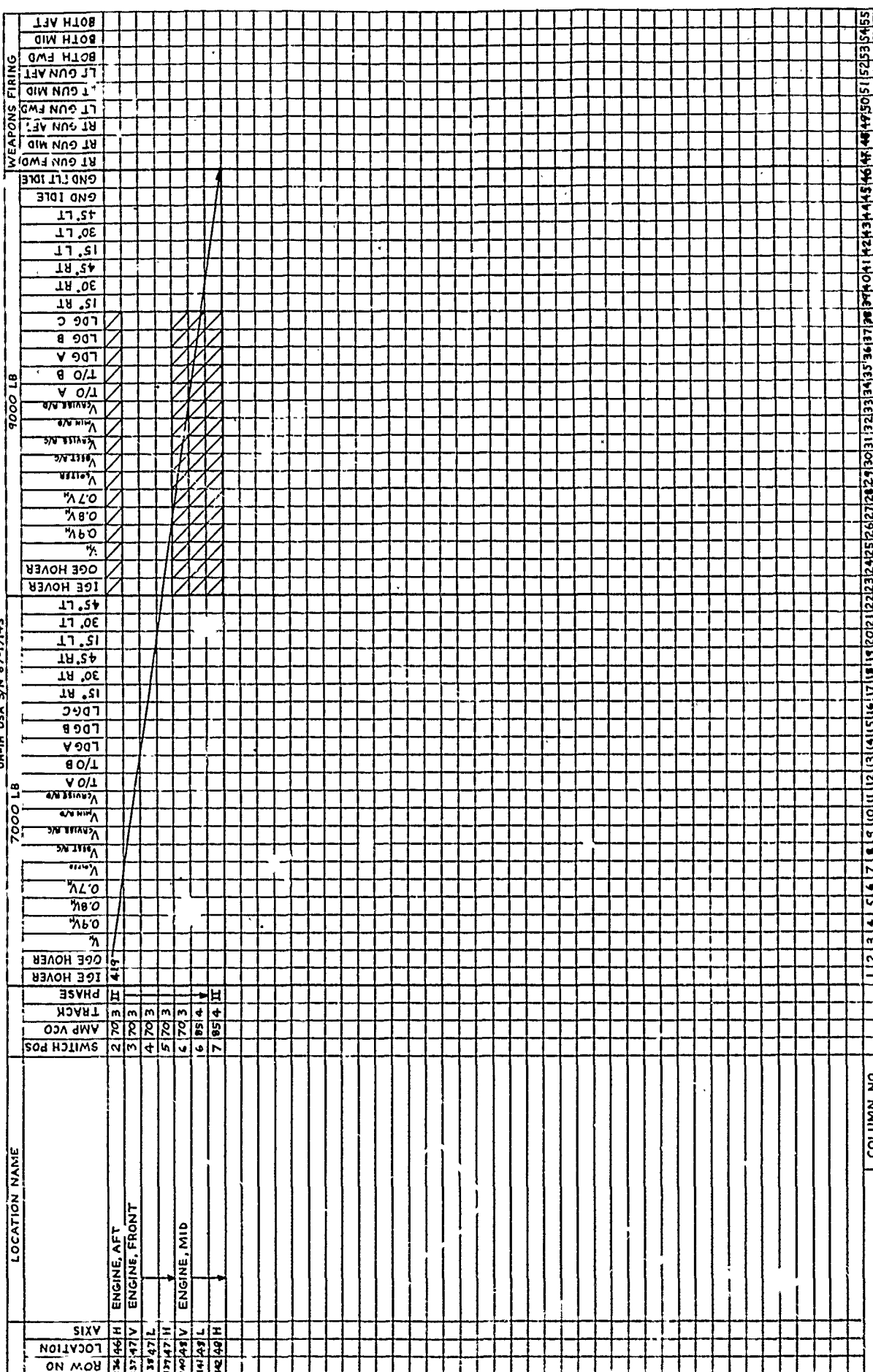
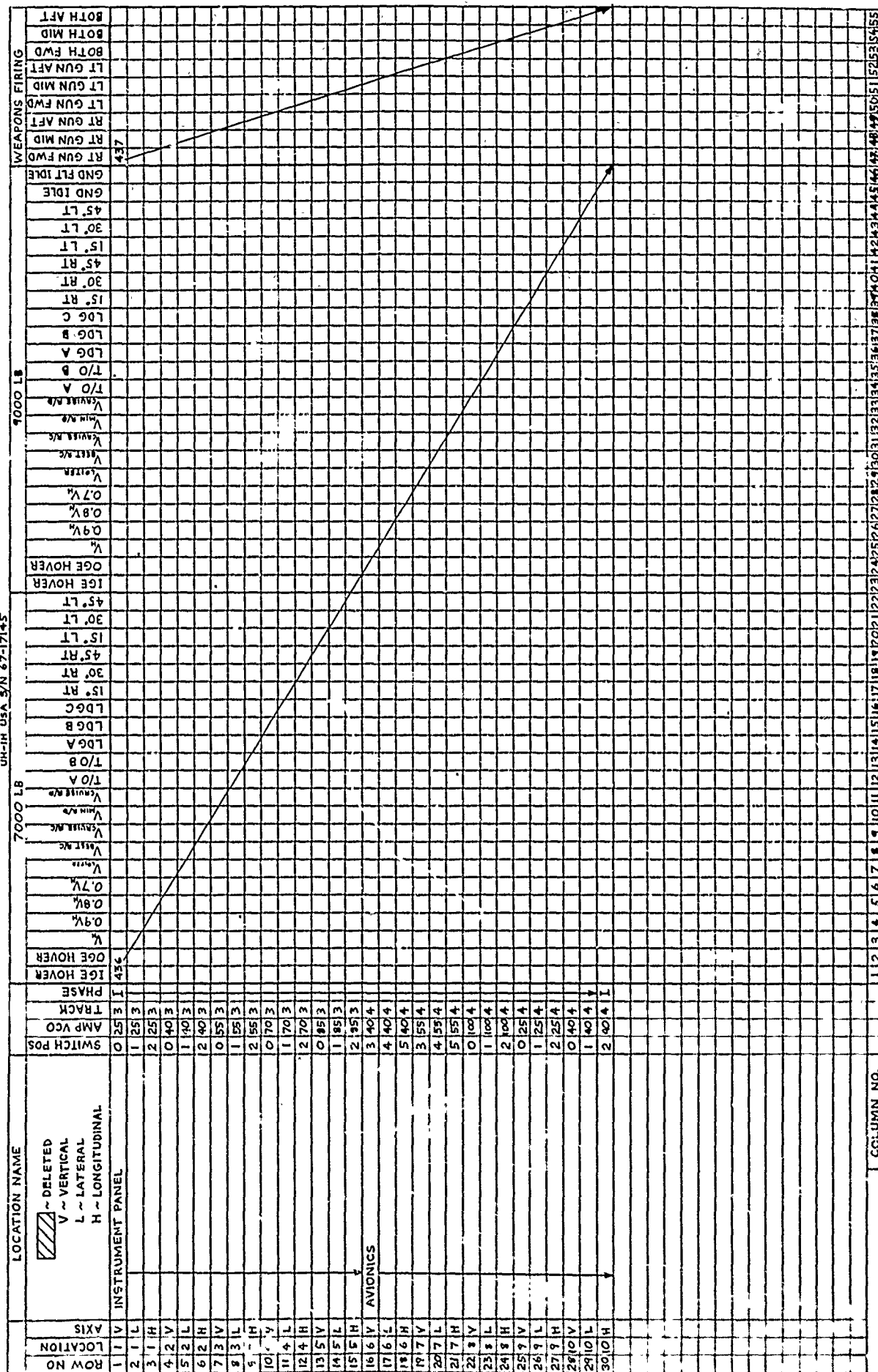
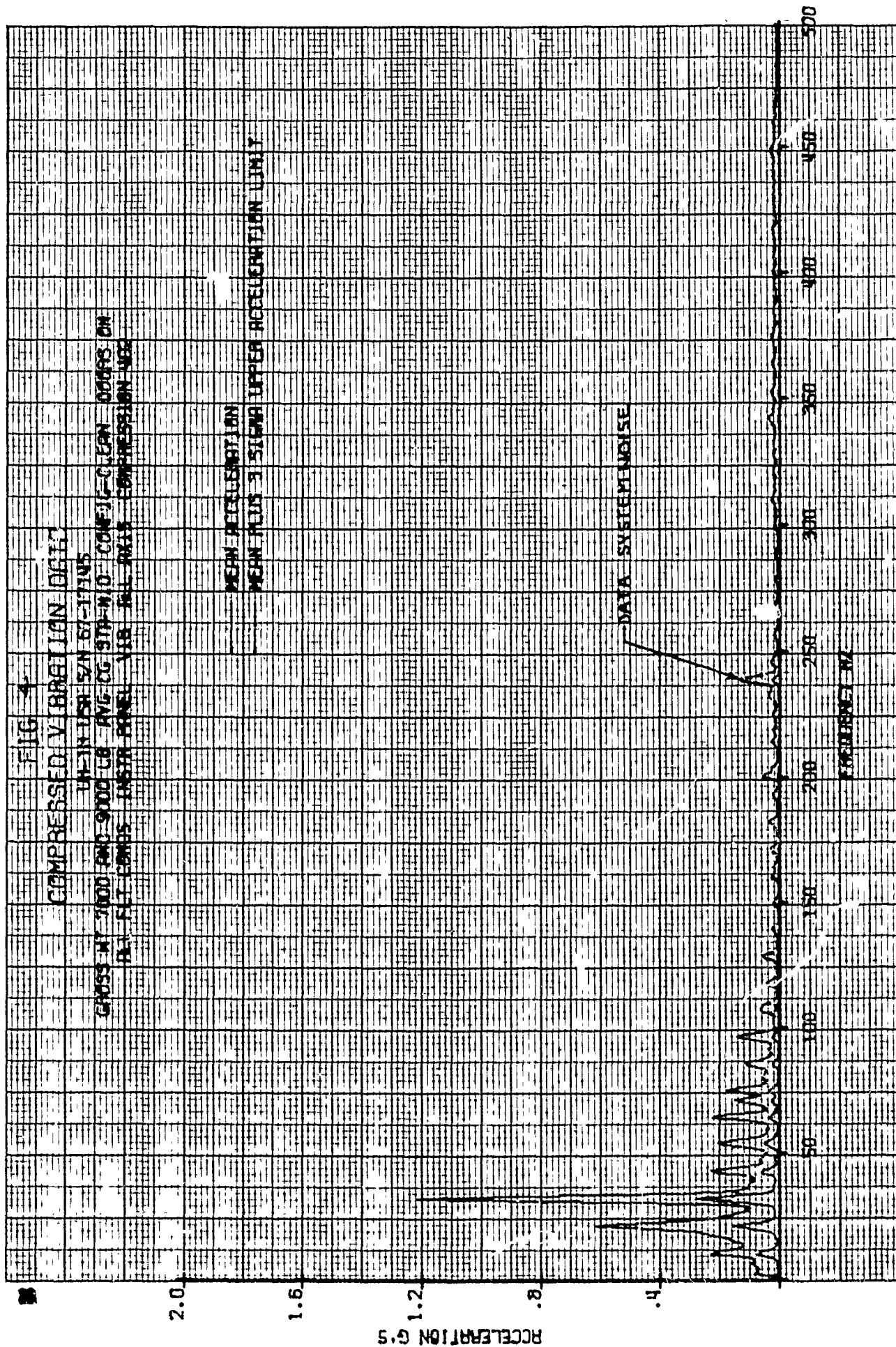
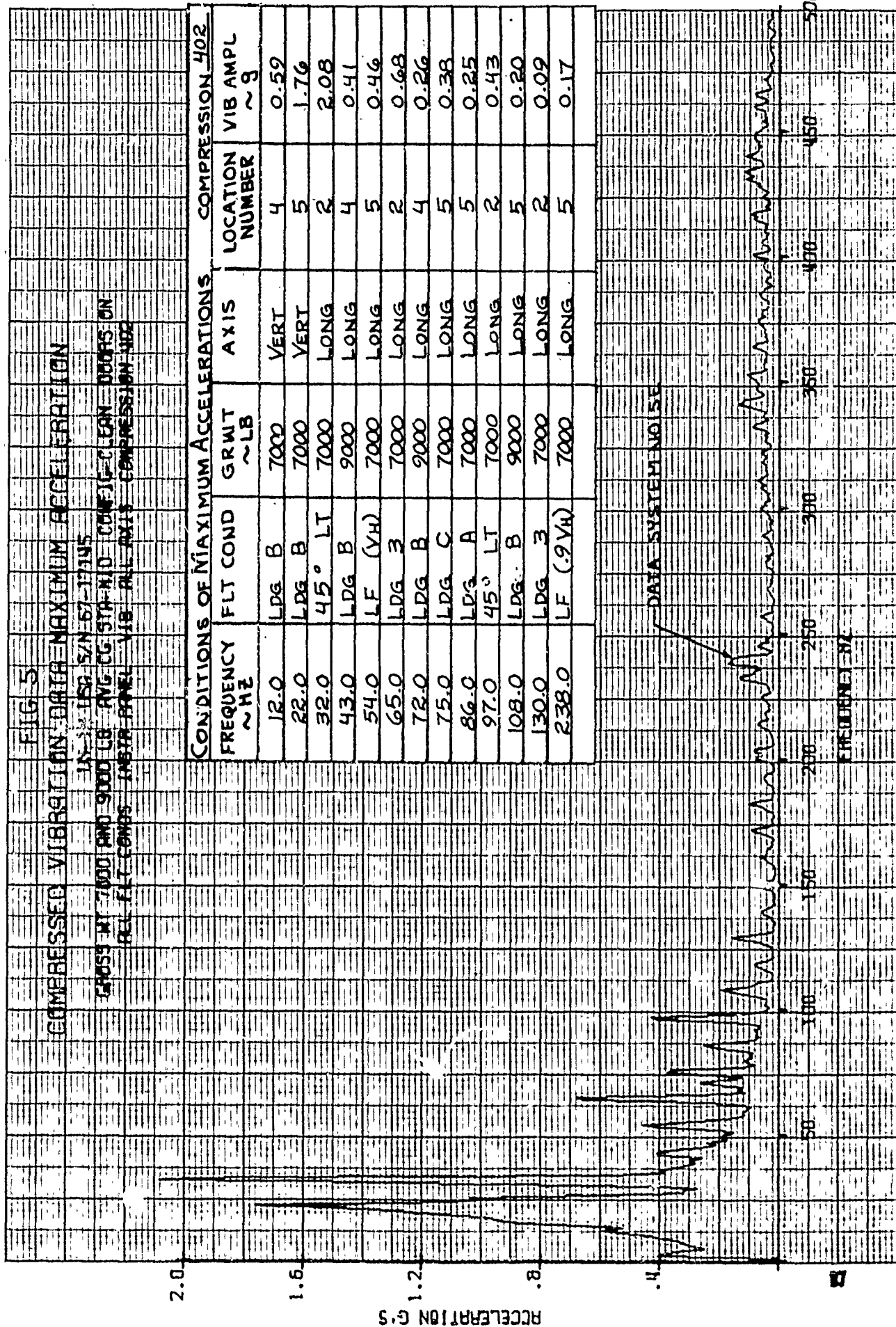


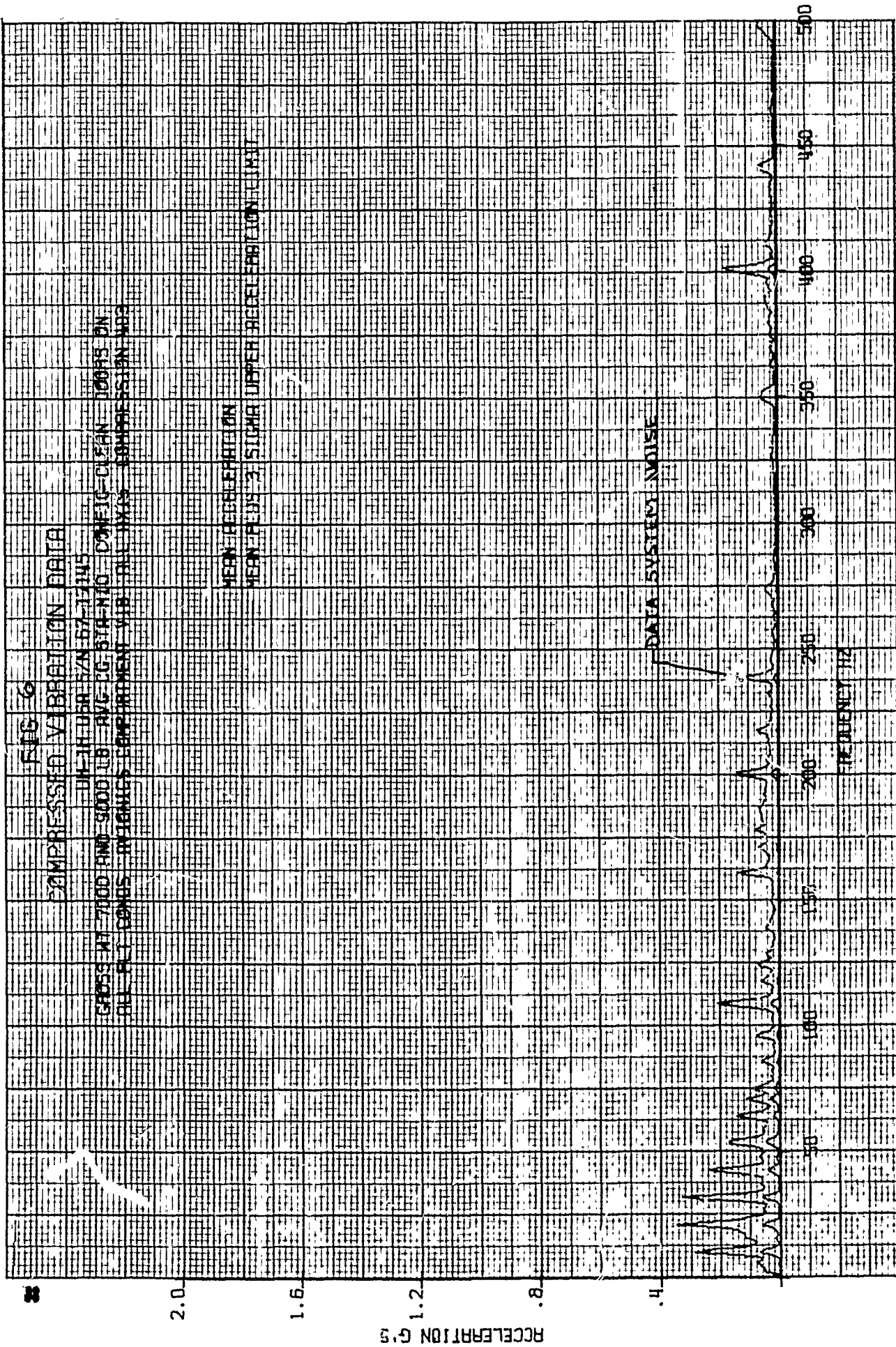
FIGURE 3
THIRD PASS DATA COMPRESSION ARRAY

PAGE 1 OF 1









COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION									
GROSS WT 7000 LBS. AVG 10 STR-MID COME-CL SAN 100015 ON									
ALL FLT CONDS. INSTANT COMPRESS. VIB. ALL AXIS COMPRESS. IN 1003									
TUE 11/15/54 57N 67W 174US									
CONDITIONS OF MAXIMUM ACCELERATIONS									
FREQUENCY ~HZ	FLT COND	GR WT ~LB	AXIS	LOCATION NUMBER	COMPRESSION 403				
6.0	GND IDLE	9000	VERT	9	0.27				
10.0	45° RT	9000	LAT	6	0.46				
18.0	LDG B	7000	VERT	10	0.86				
22.0	LDG B	7000	VERT	10	0.78				
32.0	LDG B	9000	LONG	8	1.39				
43.0	LDG C	7000	VERT	6	0.45				
54.0	LDG B	9000	VERT	6	0.28				
64.0	45° RT	9000	LAT	6	0.30				
75.0	LDG B	9000	LAT	6	0.19				
96.0	LDG B	9000	LONG	8	0.27				
109.0	T/O B	9000	VERT	8	0.46				
125.0	VMIN R/D	7000	VERT	7	0.45				
161.0	VCruise R/D	7000	VERT	7	1.00				
178.0	VMIN R/D	7000	VERT	7	0.56				
186.0	VCruise R/D	7000	VERT	7	0.45				
214.0	VMIN R/D	7000	VERT	7	0.47				
340.0	VMIN R/D	9000	VERT	8	0.33				
401.0	OGE	7000	VERT	7	0.34				

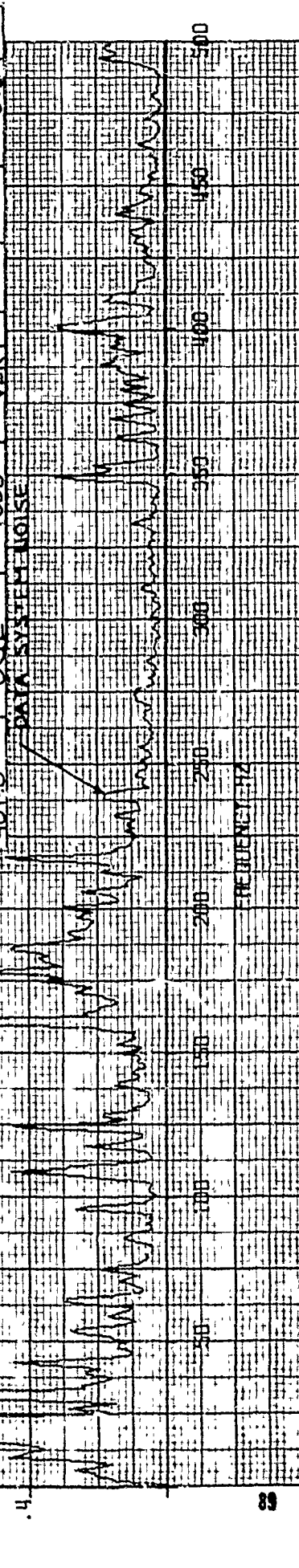


FIG. 8

COMPRESSED VIBRATION DATA

UL-111 USF SN 57-17115
 CROSS AT 1000 HNO 5000L0 AVG CG STR-MID COMFIC-CLEAN DOORS ON
 HELI FLY ZONES DEPART FRE 0075 VIB IN HELI HNS COMPRESSION WEN

WERN RECELERATION

WERN REUS 3 STEER UPPER RETELLERATION LIMIT

DATA SYSTEM NOISE

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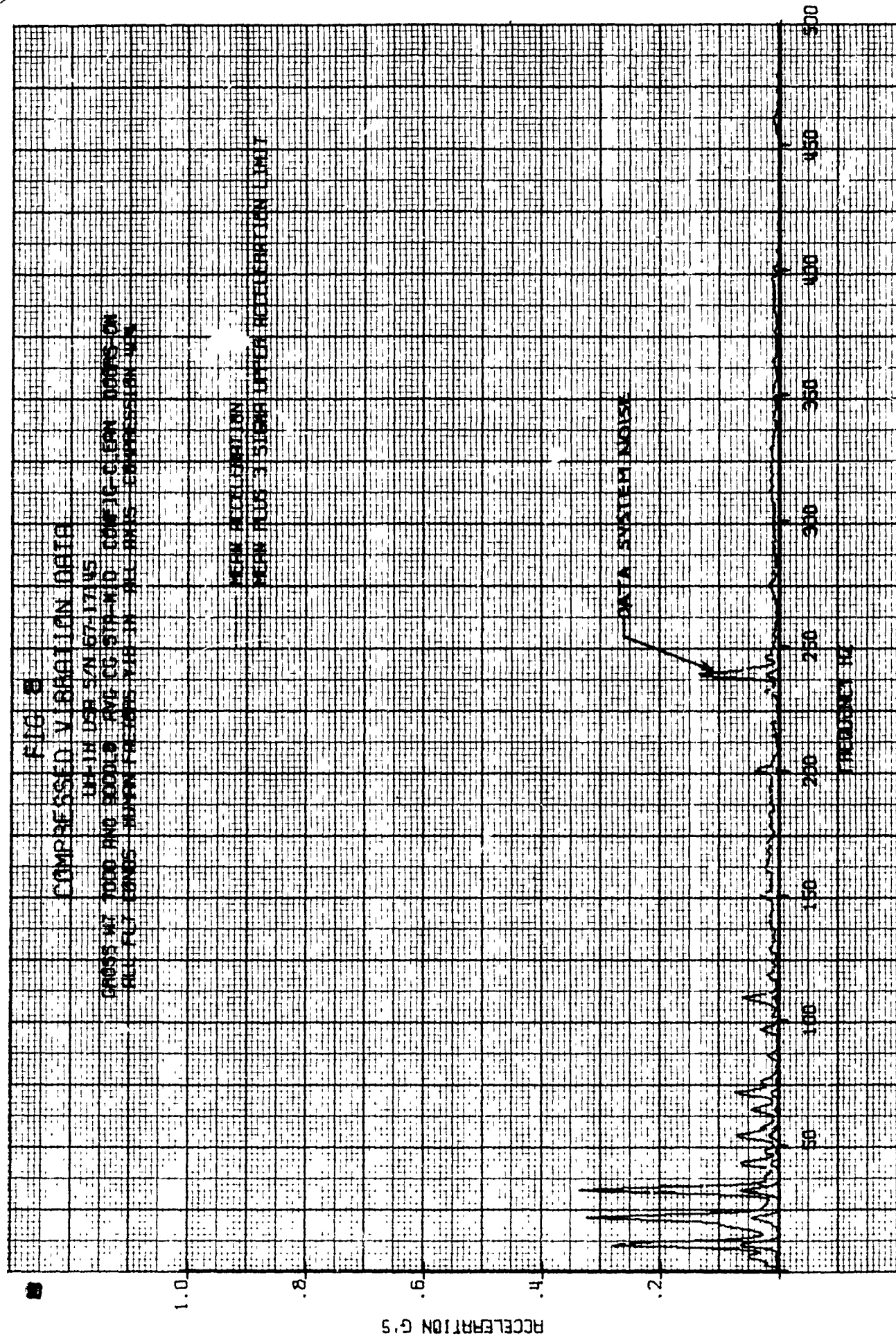


FIG 9

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UNIT: USA S/N 52-17145
 CROSS AT 1000 AND 2000 Hz AVG LG 3/4 INQ CONFIG-CLEAN 10015 ON
 ALL FLT BANDS HUMAN FREQUENCIES IN ALL BKS COMPRESSION VIB

1.0

ACCELERATION G'S

.8

.6

.4

.2

50

100

150

200

250

300

350

400

450

500

FREQUENCY Hz

DATA SYSTEM NOISE

CONDITIONS OF MAXIMUM ACCELERATIONS

FREQUENCY ~ Hz	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	COMPRESSION VIB AMPL ~ g
6.0	GND IDLE	9000	VERT	15	.18
10.0	45° RT	9000	VERT	14	.69
18.0	IGE	9000	VERT	14	.44
21.0	45° LT	9000	VERT	14	.82
32.0	LDG C	7000	VERT	15	.57
43.0	LDG C	7000	LONG	11	.13
53.0	45° RT	9000	VERT	12	.14
168.0	LF (VH)	7000	VERT	14	.12
200.0	GND FLT IDLE	9000	VERT	14	.15
241.0	LF (.7VH)	7000	VERT	14	.21

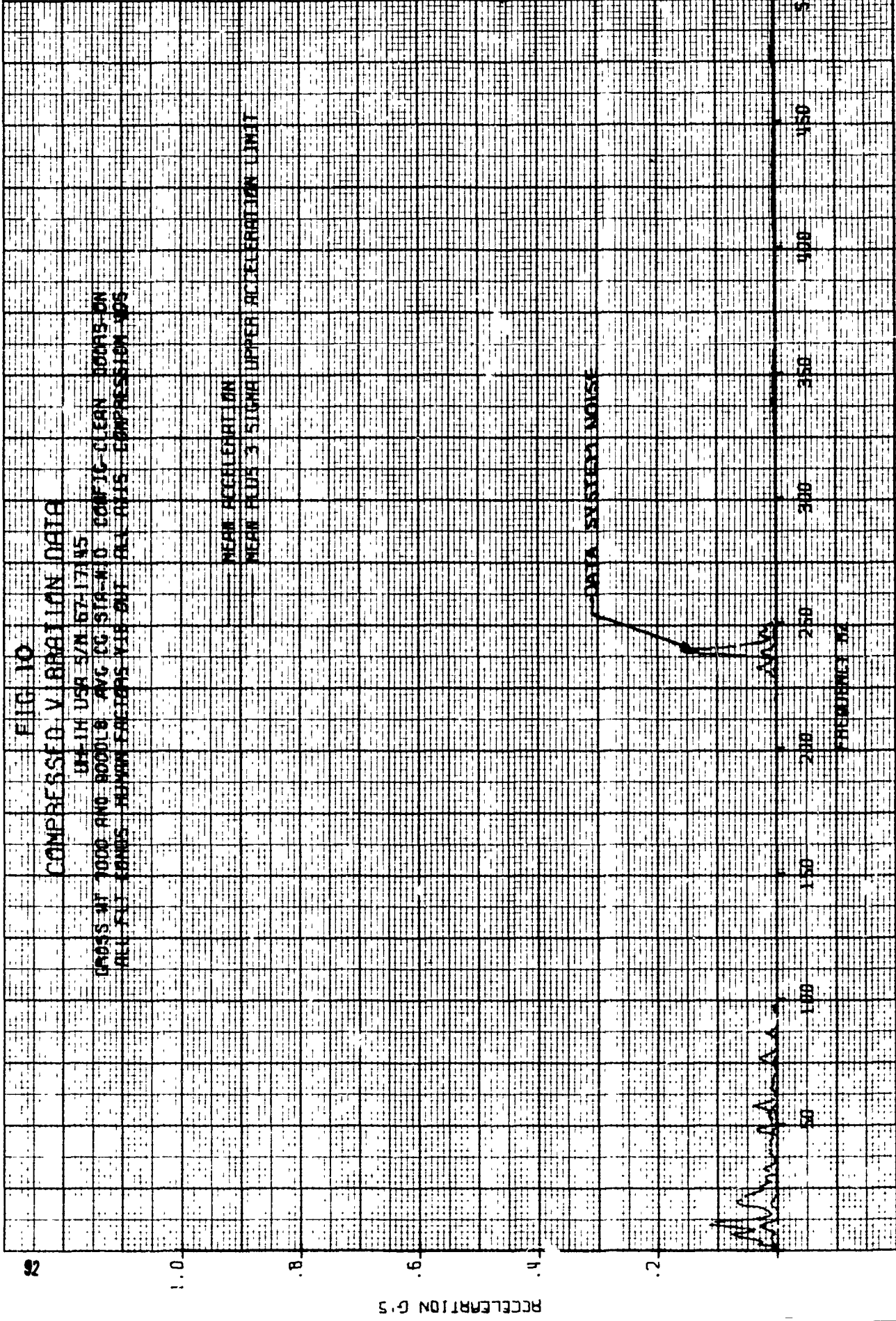


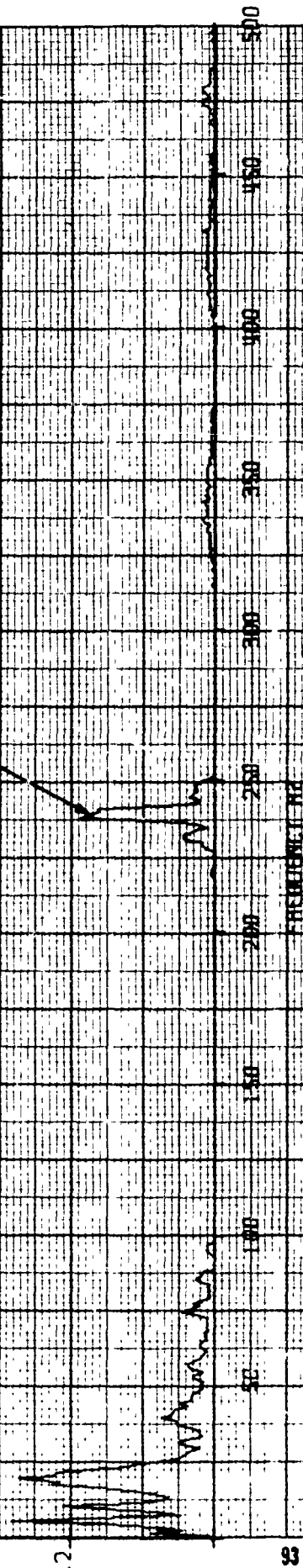
FIG 11

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UH-1H USA S/N 67-17145
 CROSS-UT 7000 RPM 9000 LB CWT LG STR-W/O CONFIO-CLEAN DOORS-ON
 ALL FLT-REMS HUMAN FACTORS VIB-OUT DEL AXIS COMPRESSION-VIBS

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 405	
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g
6.0	GND IDLE	9000	VERT	16	.28
11.0	30° LT	7000	VERT	17	.21
20.0	LDG B	7000	LAT	17	.27
32.0	45° RT	7000	VERT	16	.05
40.0	LDG B	7000	LAT	17	.073
54.0	LDG B	7000	LONG	16	.03
75.0	45° RT	7000	LONG	16	.045

DATA SYSTEM NOISE

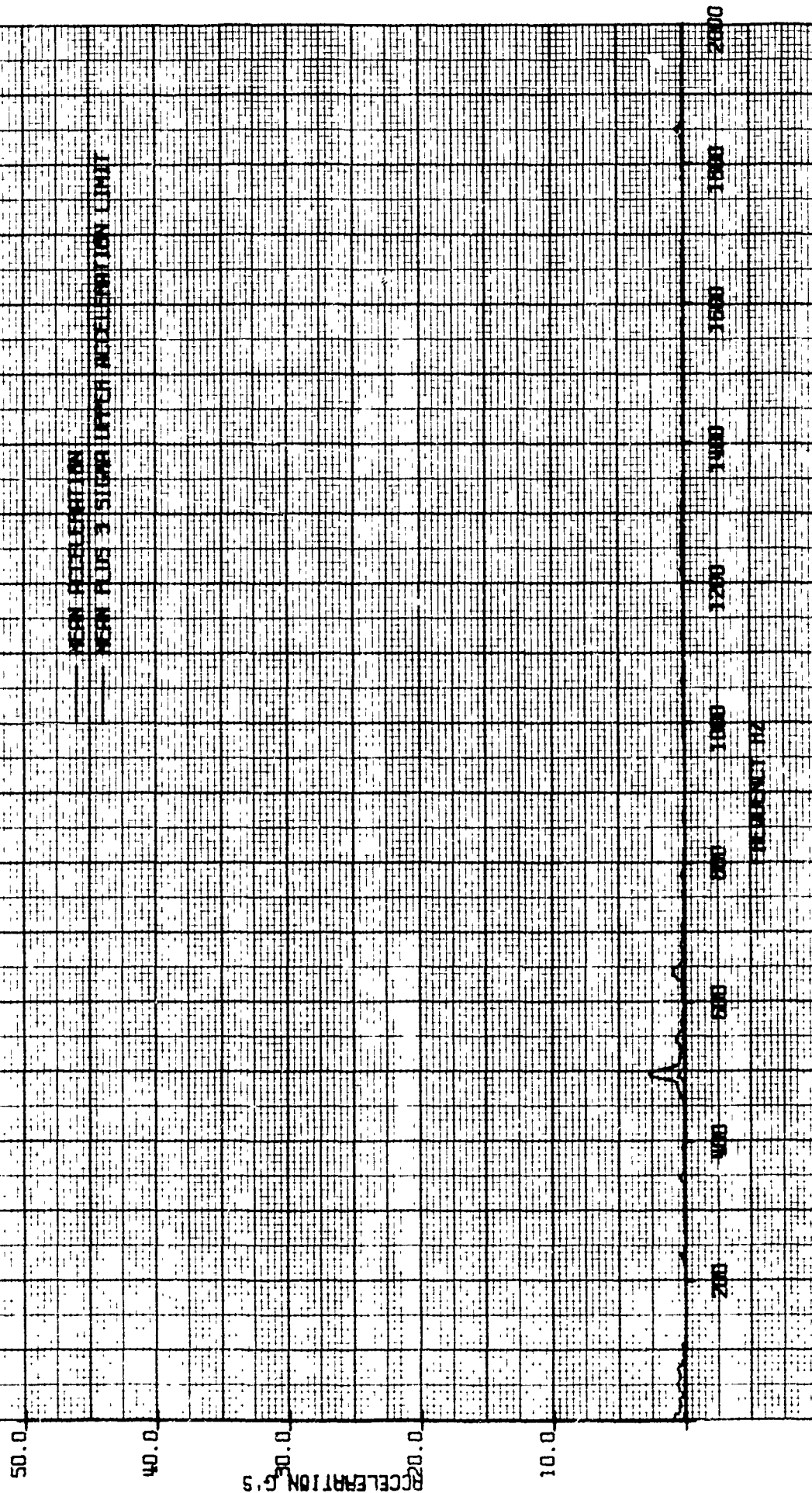


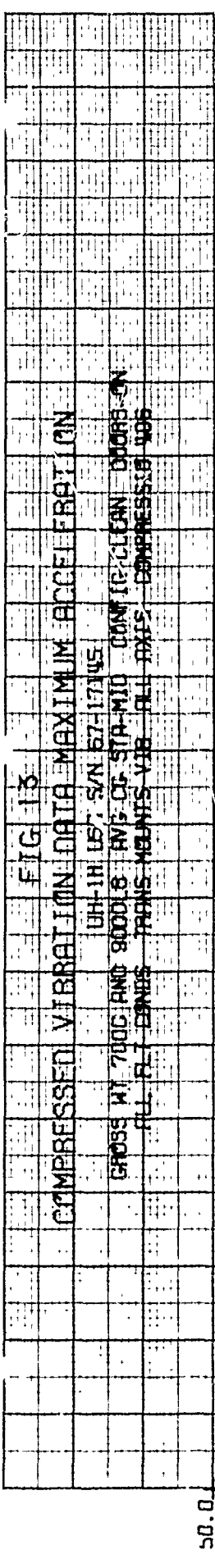
0004-5415/95 \$04.00

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 406	
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g	
108.0	IGE	7000	VERT	19	1.53	
348.0	LDG B	7000	VERT	21	2.06	
492.0	IGE	7000	VERT	21	4.58	
640.0	QGE	9000	VERT	20	1.75	
780.0	IGE	7000	VERT	19	1.92	
1062.0	IGE	7000	VERT	19	0.42	
1648.0	LDG B	7000	VERT	21	3.76	

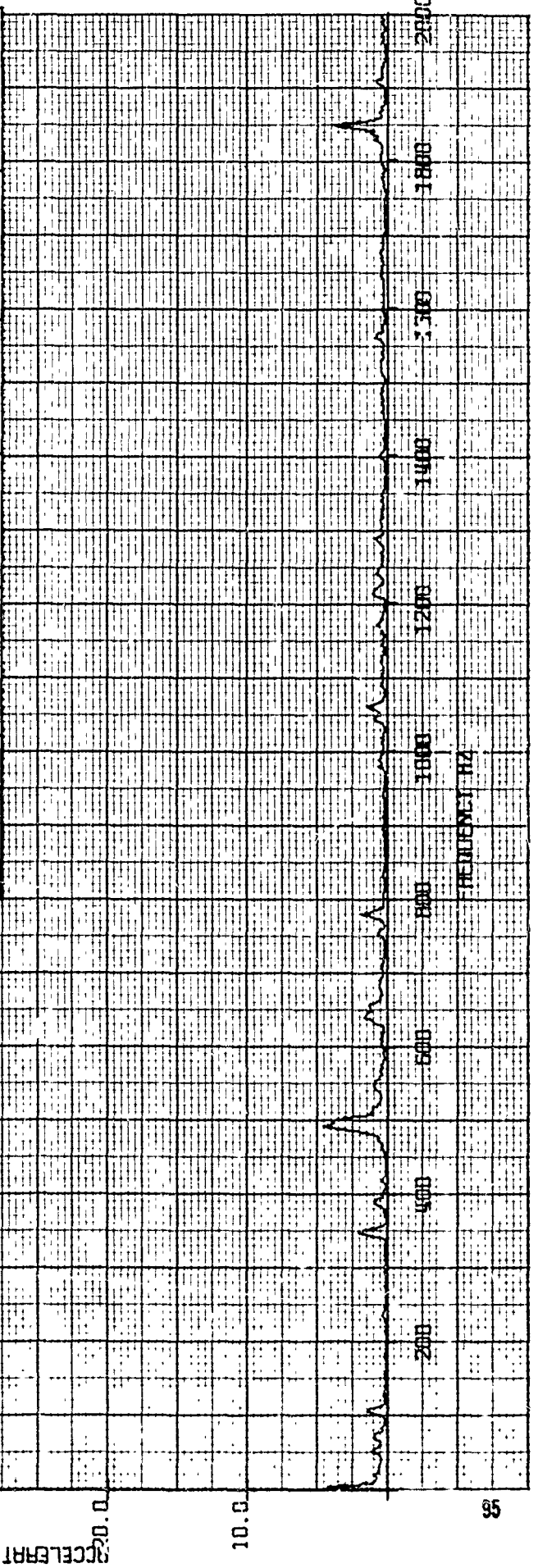


FIG 14

COMPRESSED VIBRATION DATA

GROSS WT 7000 AND 9000 LB. AVG OF STR-MID CONFIG-CLEAN DOORS-ON
 ALL PLT CONDS. TAIL BOOM ATTACH PTS VIB. ALL AXIS COMPRESSION-407

5.0

4.0

ACCELERATION G'S

3.0

2.0

1.0

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

2000

4000

6000

8000

10000

12000

14000

16000

18000

20000

FREQUENCY HZ

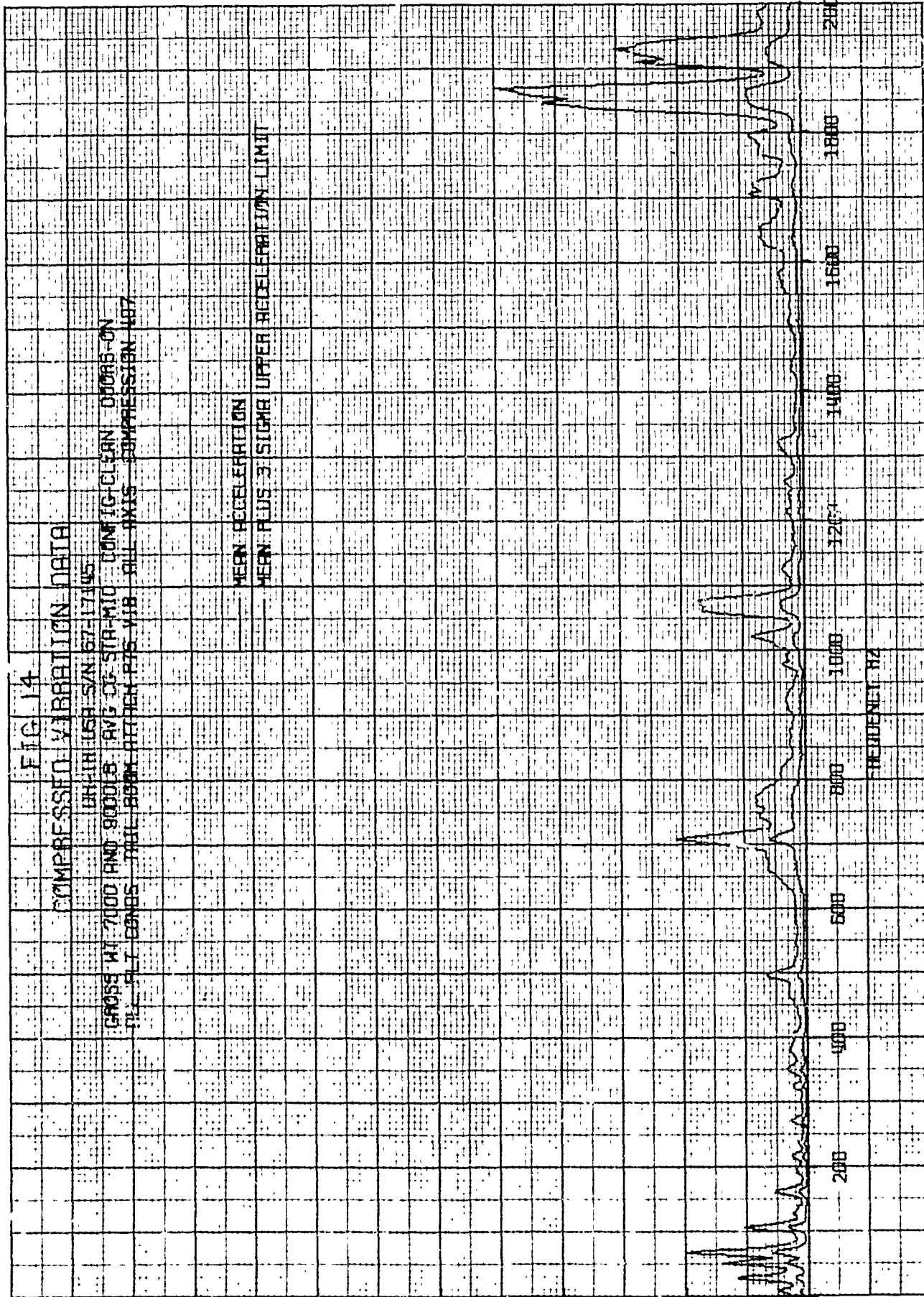


FIG 15

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UH-1H USA S/N 67-17145
 GROSS WT 7000 AND 9000 LB AVG CG STR-MID CONFIG-CLEAN DMORE-ON
 ALL FLT CONDS. THE 1800M ATTACHED RT5 VIB ALL AXIS COMPRESSION 1897

CONDITIONS OF MAXIMUM ACCELERATIONS				COMPRESSION 407	
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g
32.0	45° LT	9000	VERT	23	0.84
52.0	OG E	9000	VERT	23	0.85
68.0	LF (VL)	7000	VERT	23	0.93
700.0	GND IDLE	9000	LONG	23	2.00
1056.0	T/O A	7000	VERT	22	1.93
1080.0	LF (.8VH)	7000	LAT	22	1.34
1704.0	LF (.7VH)	9000	VERT	22	1.11
1848.0	LDG B	7000	VERT	22	4.16
1868.0	VERUSE R/D	9000	VERT	22	5.73
1904.0	45° RT	7000	VERT	23	2.15
1916.0	LDG B	7000	VERT	23	2.40
1928.0	45° LT	7000	VERT	23	2.40

ACCELERATION G'S

2.0

3.0

4.0

5.0

2.0

1.0

2.0

1.0

250

500

800

1000

1200

1400

1600

1800

2000

2200

FREQUENCY HZ

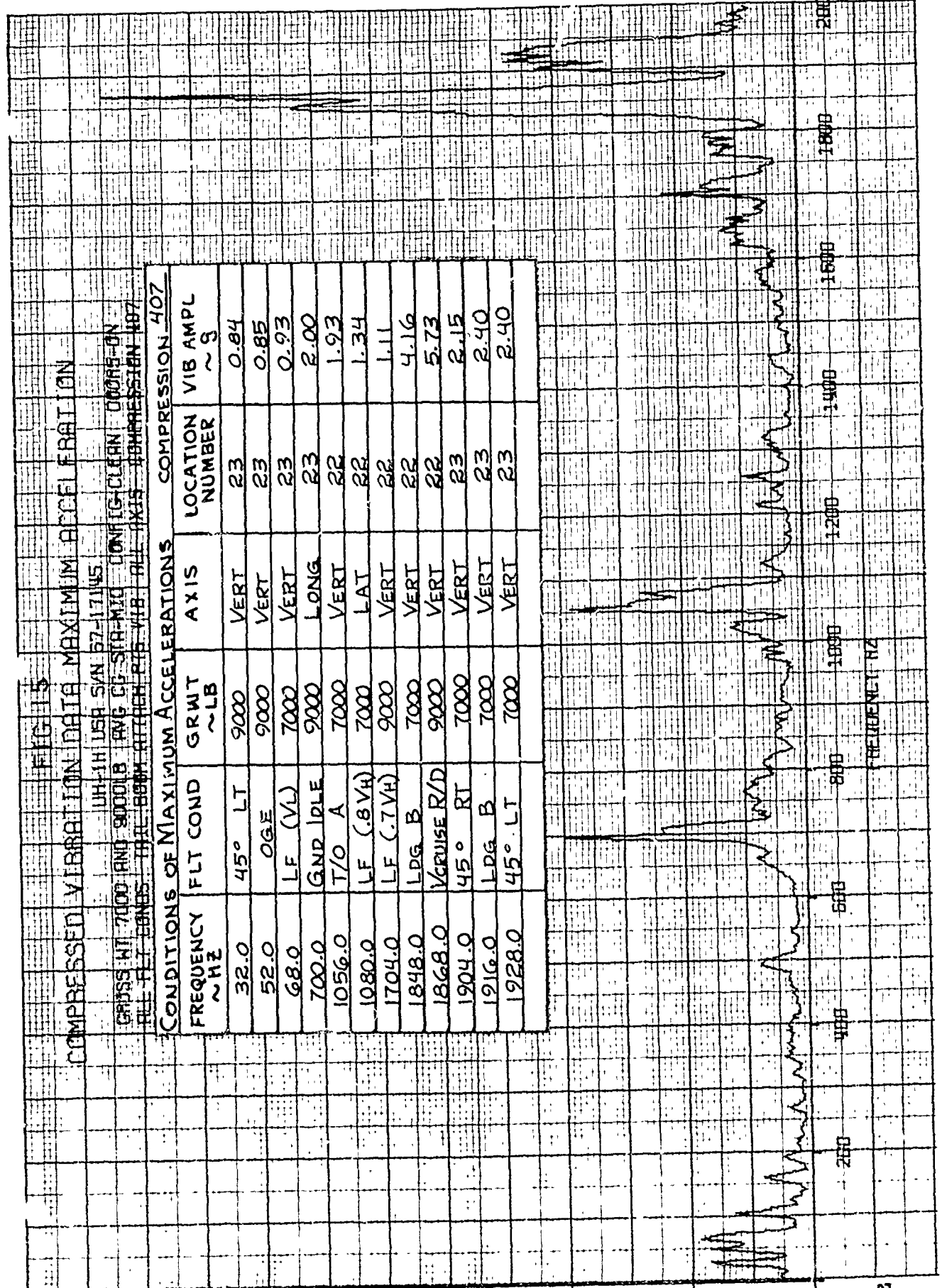


FIG 16

COMPRESSED VIBRATION DATA

UN-JH USB S/N 67-17195
 GROSS WT 7000 LBS DOUBLE AVG CG STA-MID. C&F IG-CLEAN OBSERV-ON
 ALL FLT COMOS ENG DOCK YTD ALL AXES COMPRESSION 400

MEAN DECELERATION
 MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ACCELERATION G'S

FREQUENCY Hz

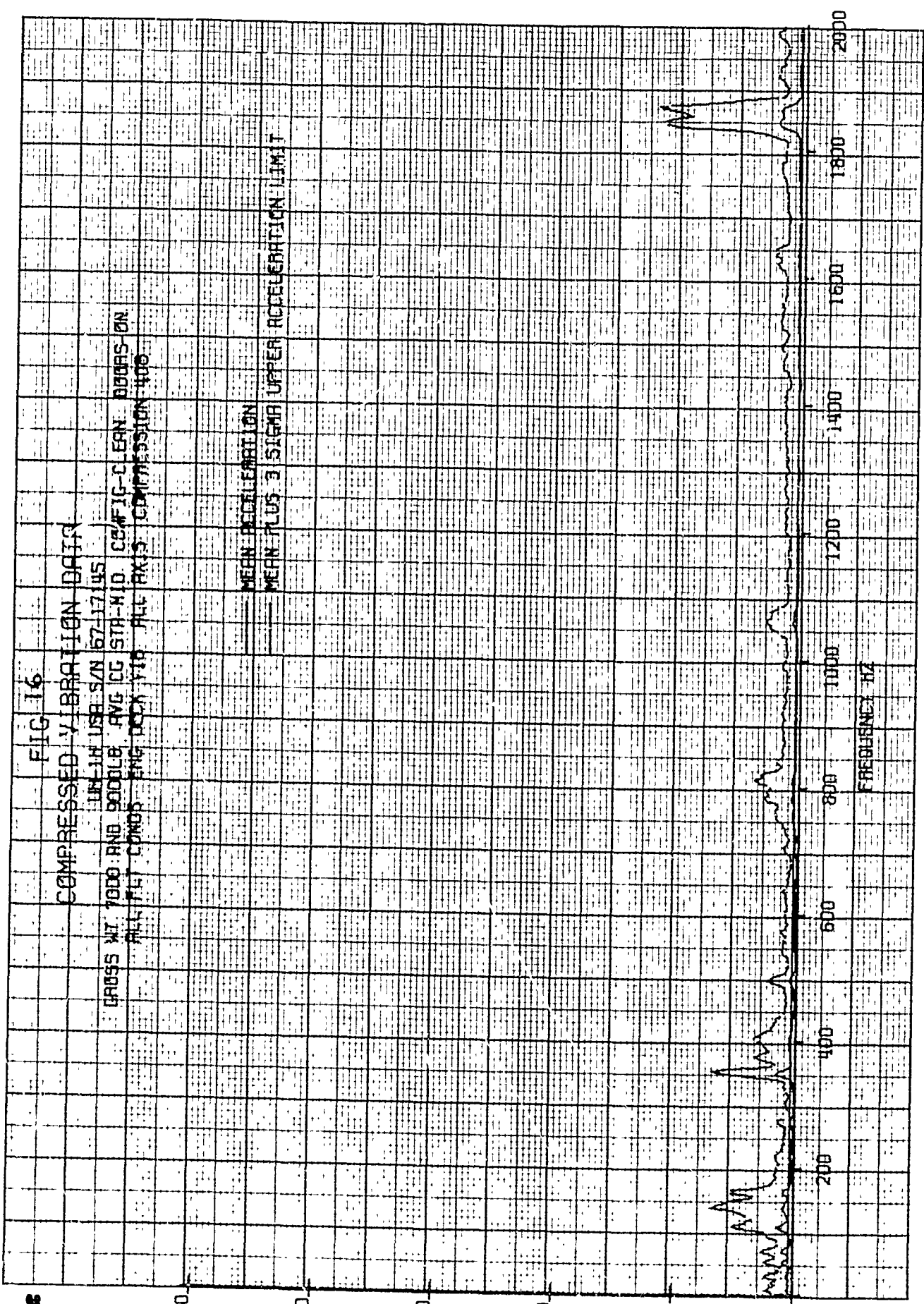


FIG. 17									
COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION									
LHT-3H USA S/N 6717145									
CROSS AT 7000 AND 9000 LB. AVG. EG. STA. NO. 10									
ALL FLT. COND'S ENG. DECK VIB. ALL AX'S COMPRESSION 400									

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 400	
FREQUENCY ~ HZ	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
116.0	VCruise R/D	7000	VERT	25	0.99	
136.0	LF (VL)	9000	VERT	25	1.44	
160.0	30° RT	9000	VERT	25	0.76	
352.0	45° LT	7000	LONG	44	2.25	
372.0	VCruise R/D	7000	VERT	25	0.71	
408.0	T/O B	9000	VERT	25	0.66	
812.0	OGE	9000	VERT	25	0.99	
1062.0	Vmin R/D	9000	VERT	25	0.62	
1844.0	Vbest R/C	9000	LAT	25	1.72	
1868.0	45° LT	7000	LAT	25	2.14	

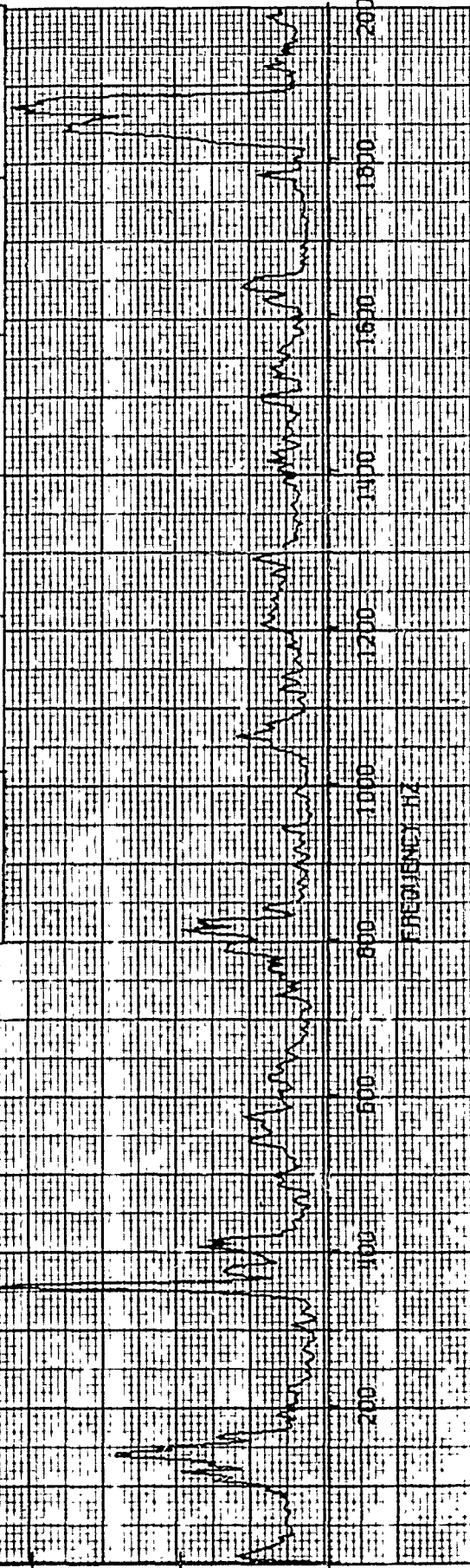


FIG 18

COMPRESSED VIBRATION DATA

TEST UNIT 7000 AND 3000L8 AVG CG STA-H10 COMPLETION 0000S ON
 ALL CT COMPS ENG FINISHED VIB ALL AXIS COMPRESSION 409

5.0

4.0

ACCELERATION G'S

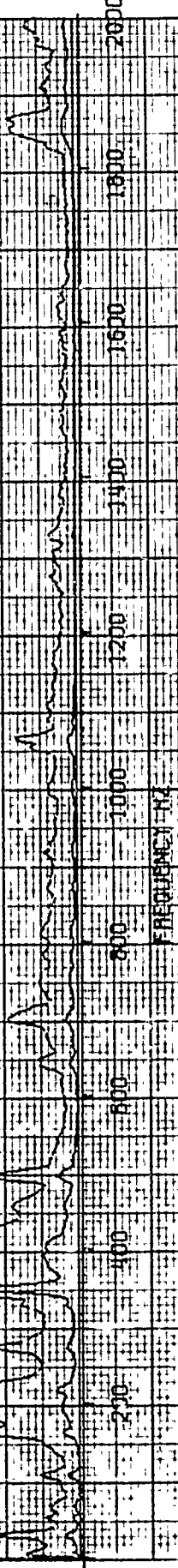
3.0

2.0

1.0

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT



2000

200

400

600

800

1000

1200

1400

1600

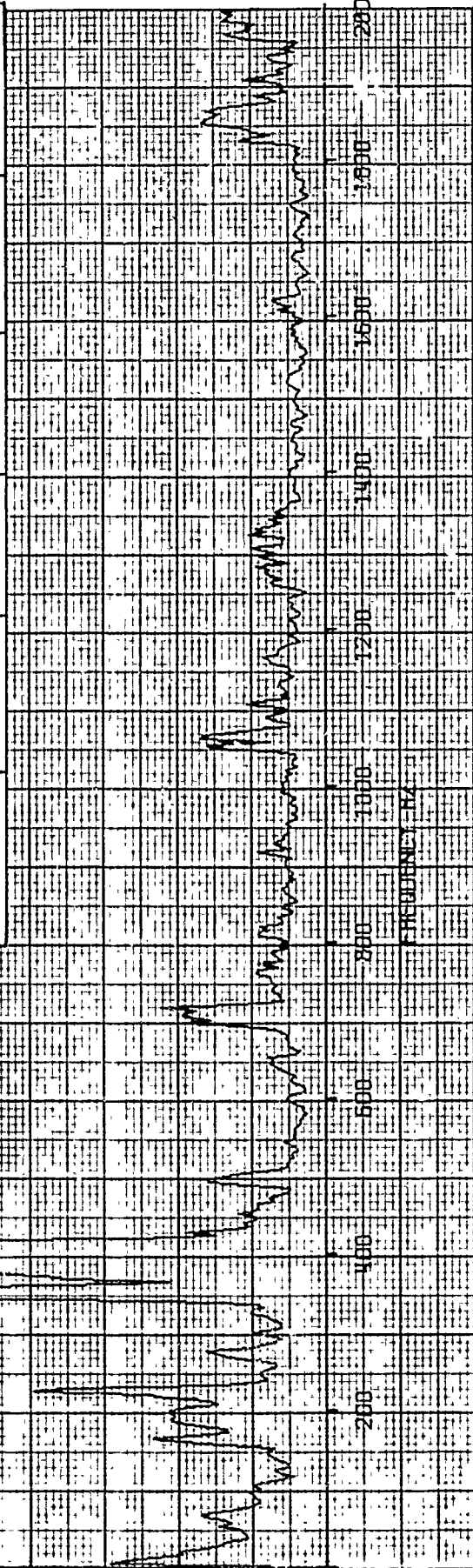
1800

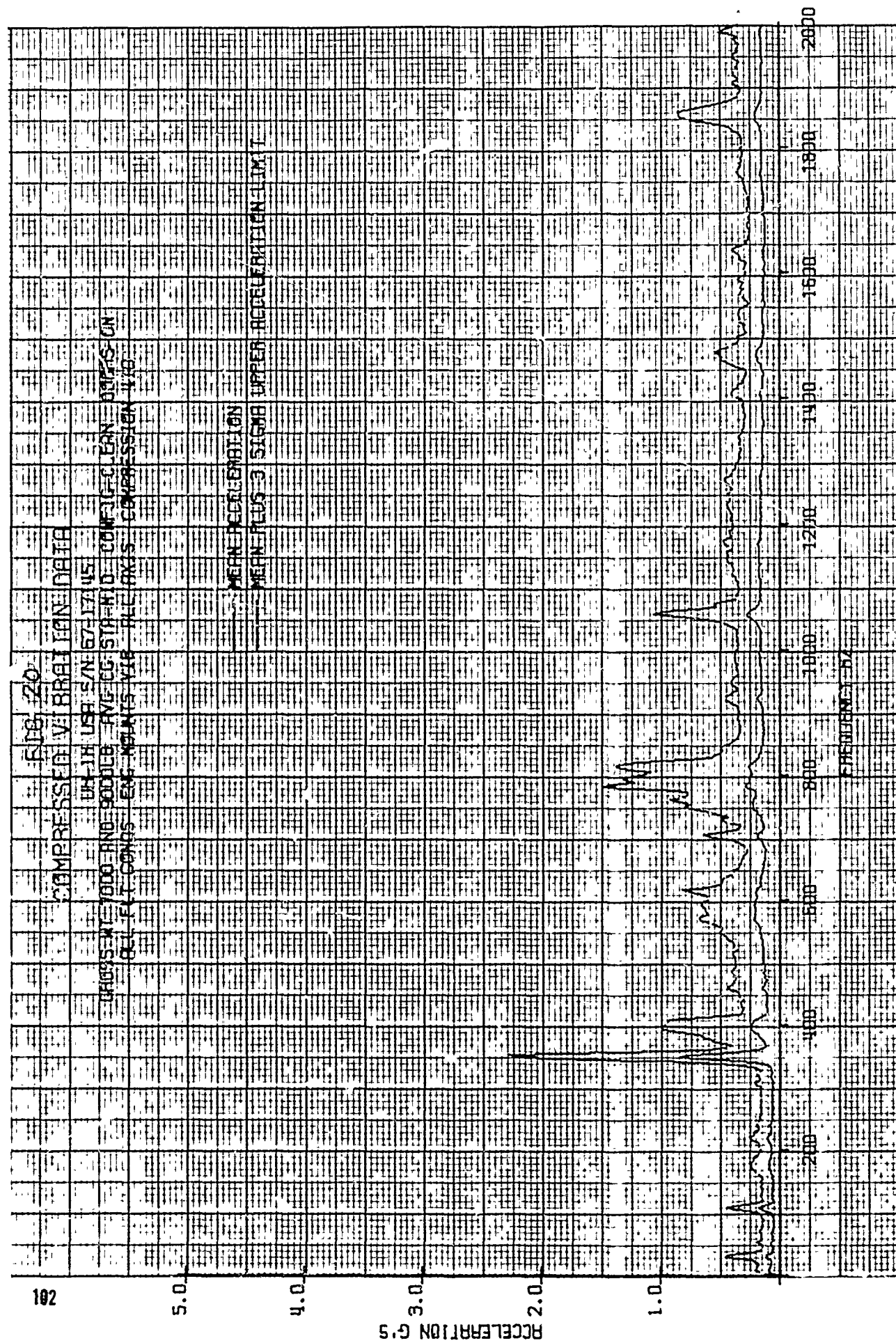
2000

FREQUENCY Hz

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION									
FIG 19	UNIT 1A	USE 5/N	57-17145						
	CROSS AT 7000 AND 9000	AVG CC	STR-N/O	CONFIG	CLEAN	DOORS ON			
	ALL FLT COMPS	ENG FIRE	ALL VIB	ALL AXIS	COMPRESSION	402			

CONDITIONS OF MAXIMUM ACCELERATIONS						COMPRESSION 402	
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g		
68.0	15° LT	9000	LAT	26	0.84		
164.0	LF (VH)	7000	LONG	27	1.17		
200.0	LF (7VH)	7000	LONG	27	1.06		
224.0	VMIN R/D	7000	LONG	27	1.98		
352.0	IGE	9000	VERT	27	3.94		
412.0	VBEST R/C	7000	VERT	27	4.44		
496.0	LF (7VH)	9000	LONG	27	0.80		
716.0	VMIN R/D	7000	LAT	27	1.11		
1064.0	LF (7VH)	7000	LAT	27	0.83		
1848.0	LDG B	7000	LAT	26	0.84		





COMPRESSION VIBRATION DATA - MAXIMUM ACCELERATION									
F128 21									
UH-1H USAF S/N 67-17145									
GROSS WT 7000 AND 8000 LB. AVG CG SIP-N/D. CONFIG-CLEAN. DOORS-ON									
ALL FLT CONDS. ENG. MONITS VIB. ALL AXES. COMPRESSION VIB.									
CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION VIB				
FREQUENCY ~ Hz	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	VIB AMPL ~ g				
352.0	LF (VL)	7000	LONG	44	2.25				
408.0	45° RT	9000	LONG	44	1.79				
568.0	T/O A	7000	LONG	29	1.18				
616.0	GND IDLE	9000	LAT	44	2.21				
704.0	VMIN R/D	7000	VERT	44	1.75				
788.0	45° RT	7000	VERT	29	3.34				
800.0	LF (VH)	7000	VERT	29	3.44				
808.0	T/O A	9000	VERT	29	3.21				
1056.0	VMIN R/D	7000	VERT	44	2.41				
1072.0	VCRUISE R/D	7000	VERT	44	1.83				
1852.0	VMIN R/D	7000	LONG	29	1.26				

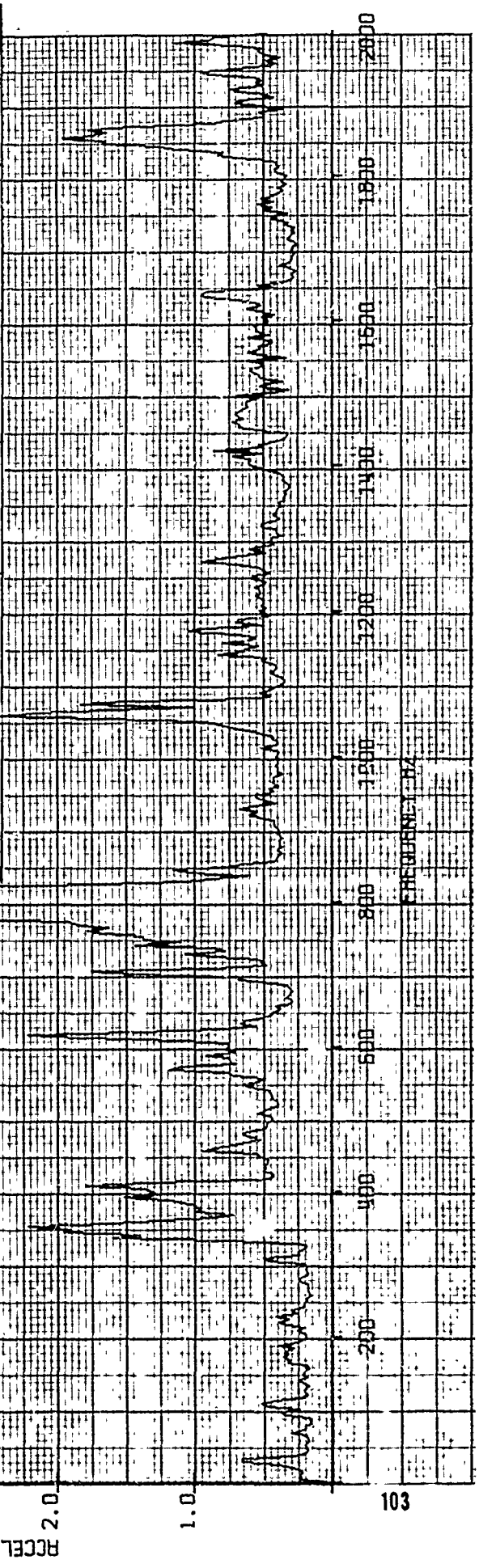


FIG 22

COMPRESSED VIBRATION DATA

CROSS WT 7000 AND 5000 LB AVE CG 519 MID CONF 10 CLEAN DORSION ON
ALL FLY 30005 TANK MOTOR SERVO 318 ALL AXES COMPRESSION 0.1

UNIT IN USR S/N 674-1745

MEAN DECELERATION

MEAN IN US 3 SIGMA UPPER ACCELERATION LIMIT

5.0

4.0

ACCELERATION G'S

3.0

2.0

1.0

200

400

600

800

1000

1200

1400

1600

1800

2000

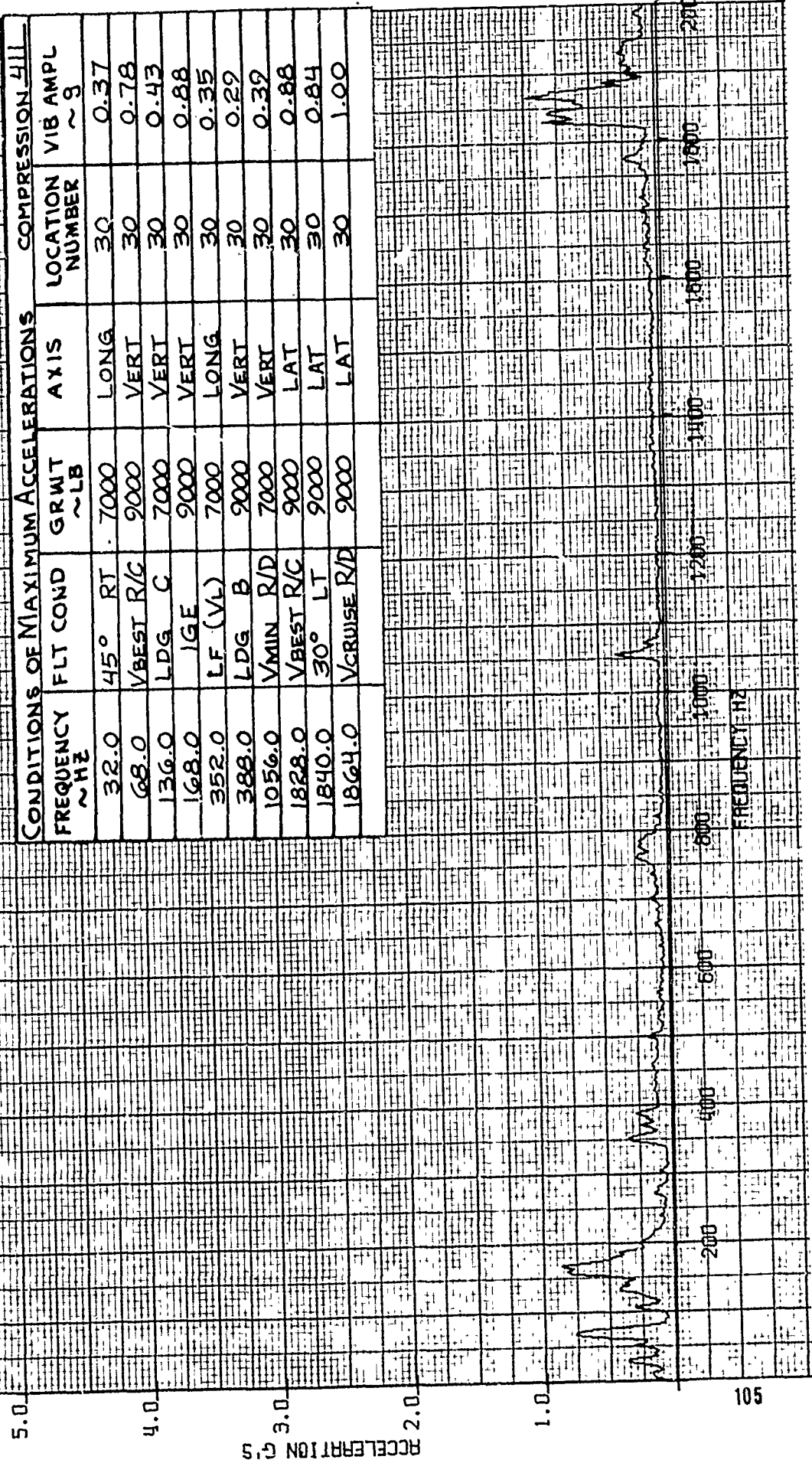
FREQUENCY Hz

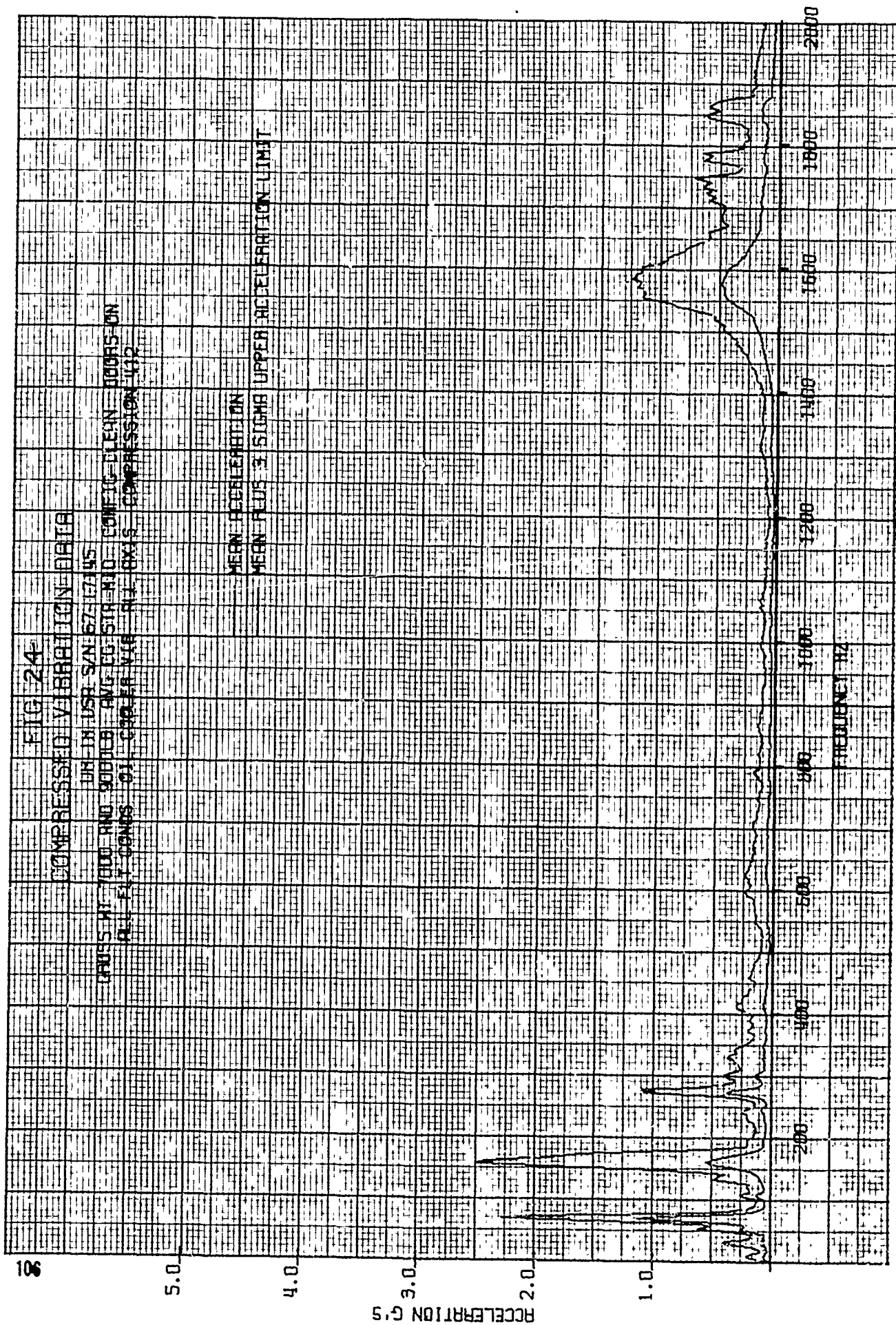
FIG. 23

COMPRESSED VIBRATION RATE MAXIMUM ACCELERATION

UH-1H L5H-S/N 57-17145
 GAUGES AT 1000 AND 3000 RPM
 ALL FLT BONDS TRAIL MOTOR SERVO VIB FLT AXIS DEPRESSION VIB

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 411	
FREQUENCY ~ Hz	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
32.0	45° RT	7000	LONG	30	0.37	
68.0	VBEST R/C	9000	VERT	30	0.78	
136.0	LDG C	7000	VERT	30	0.43	
168.0	IGE	9000	VERT	30	0.88	
352.0	LF (VL)	7000	LONG	30	0.35	
388.0	LDG B	9000	VERT	30	0.29	
1056.0	VMIN R/D	7000	VERT	30	0.39	
1828.0	VBEST R/C	9000	LAT	30	0.88	
1840.0	30° LT	9000	LAT	30	0.84	
1864.0	VCRUISE R/D	9000	LAT	30	1.00	





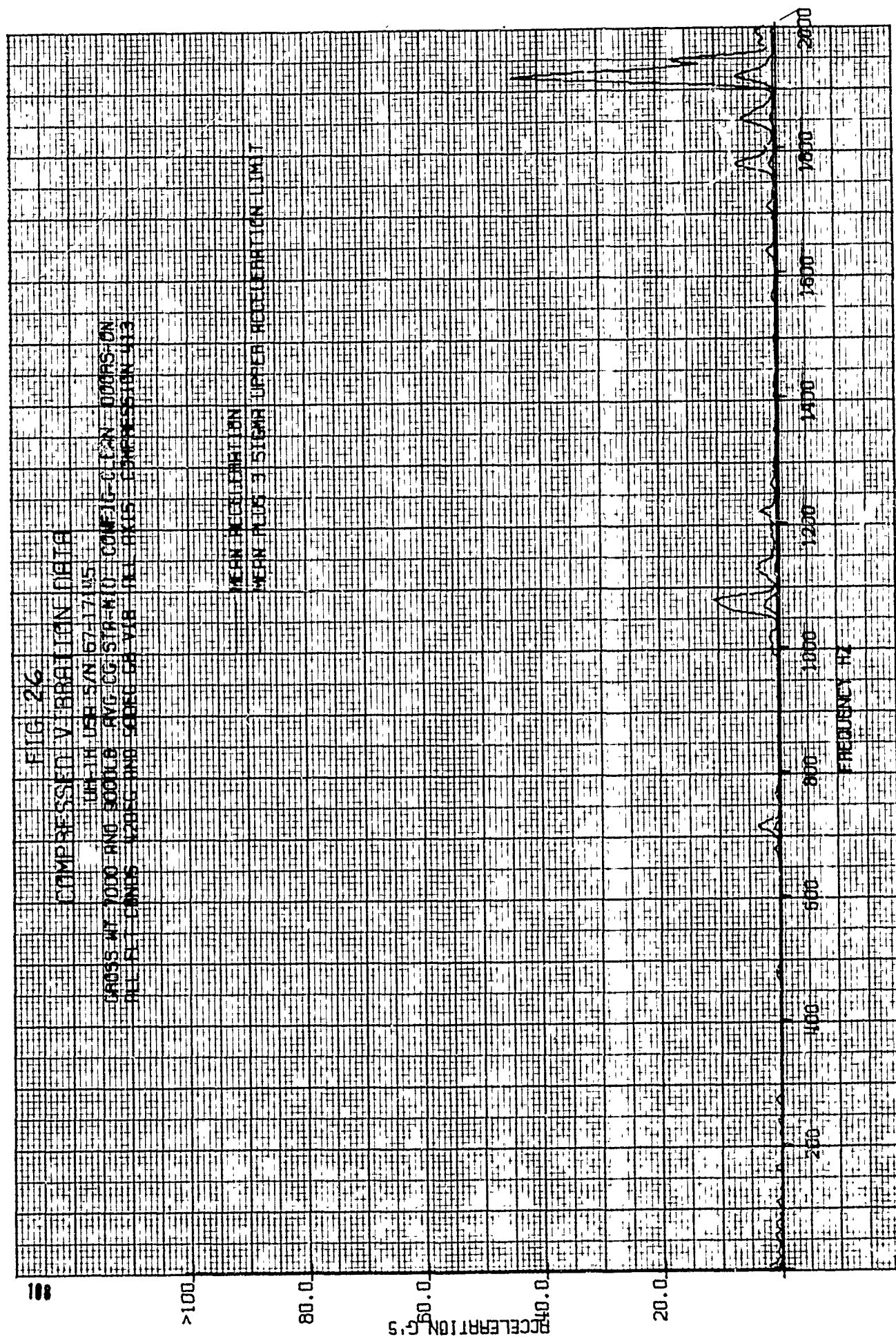
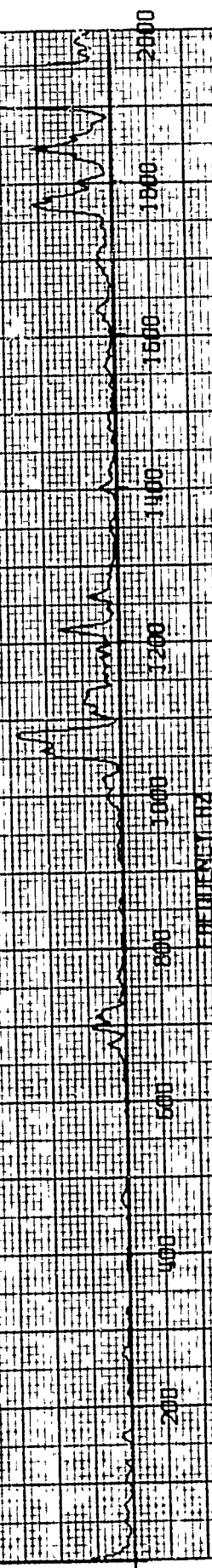


FIG 27

COMPRESSED VIBRATION RATE MAXIMUM ACCELERATION

UN IN USA SAN 57-17145
 CAUSAT 1000 AND 3000LB AVG CG STRUTS CONFIG CLEAN DOORS ON
 ALL FLT COND 12000 AND 30000 G/VIB ALL AXIS COMPRESSION 413

CONDITIONS OF MAXIMUM ACCELERATIONS						COMPRESSION 413
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g	
700.0	GND FLT IDLE	9000	LONG	33	4.51	
1060.0	T/O B	9000	LAT	32	10.94	
1080.0	LDG A	7000	LONG	33	14.47	
1124.0	LF (VL)	7000	VERT	33	5.07	
1216.0	GND FLT IDLE	9000	LAT	32	8.45	
1772.0	15° LT	7000	LAT	32	11.09	
1844.0	15° RT	7000	VERT	32	11.03	
1912.0	45° RT	7000	LAT	32	52.35	
1224.0	T/O B	9000	VERT	32	62.42	
1944.0	T/O A	9000	VERT	32	59.03	



COMPRESSED VIBRATION DATA

UH-1H UH-1H 67-17145
PROSS-WT 7000-RND-3000L6 RVC CG STA-MID CONF-IC-CLEAN DORS-ON
ALL-FLT-CONDG HYDRAULIC-SERVO-VIB ALL-RXLS-COMPRESSION-WAY

5.0

4.0

ACCELERATION G'S

3.0

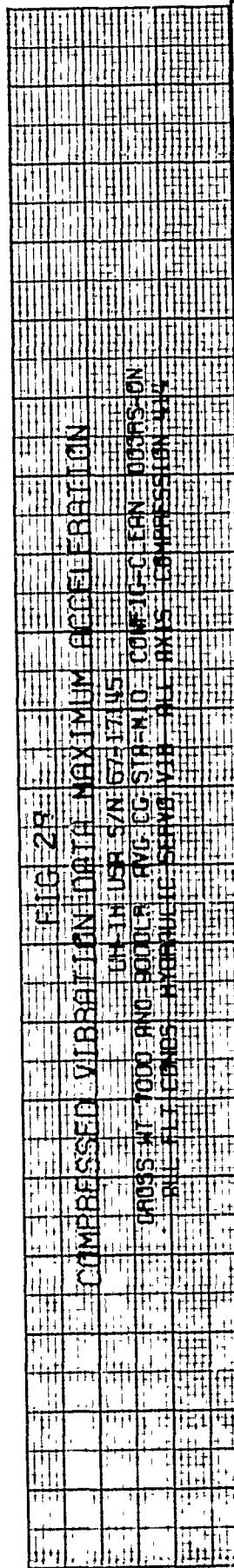
2.0

1.0

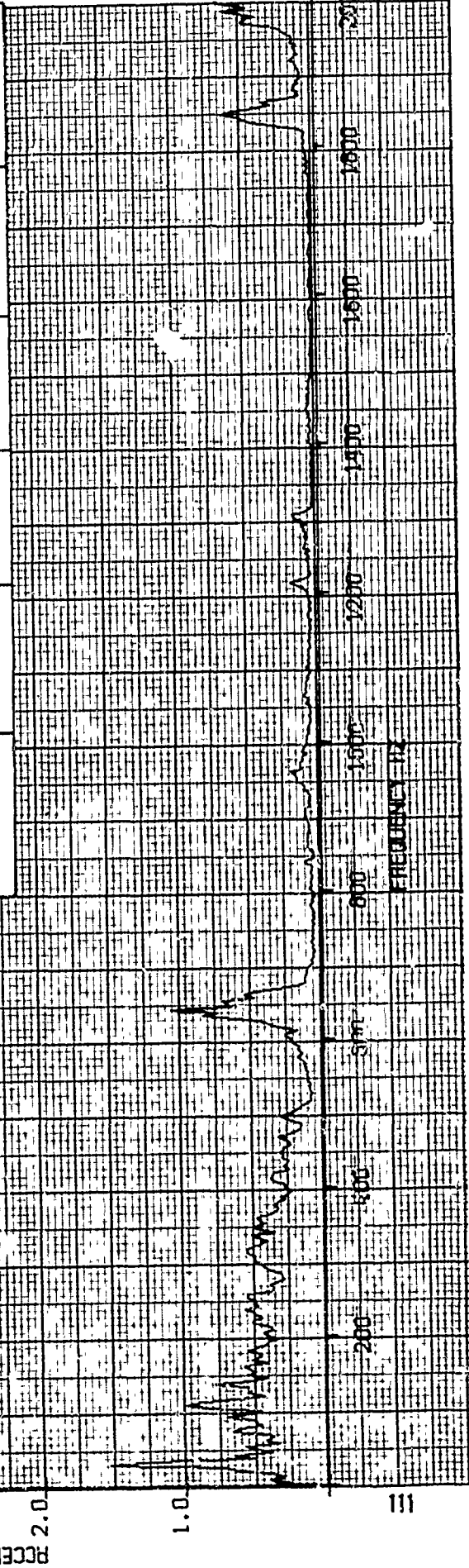
MEAN ACCELERATION

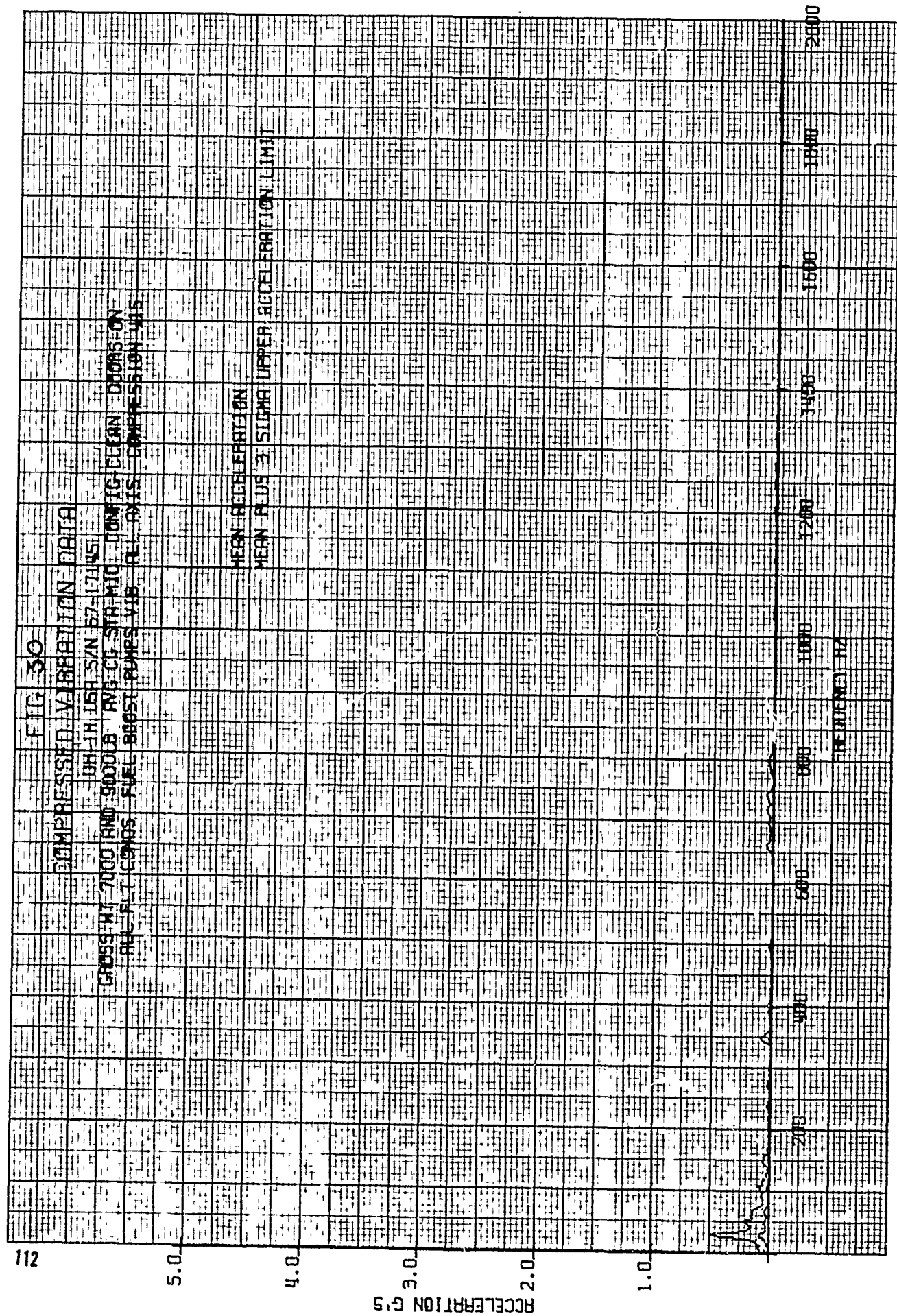
MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

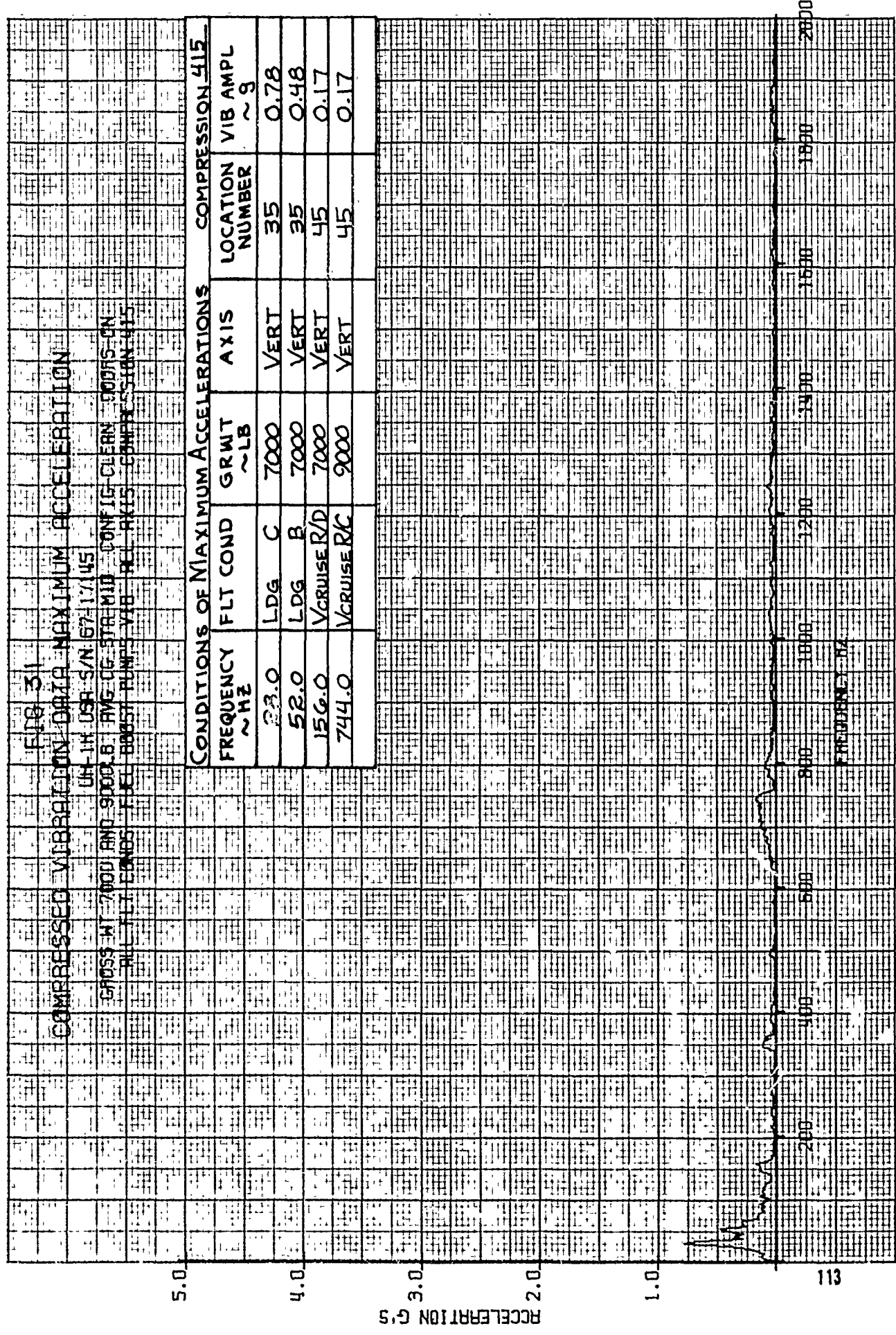




CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 414	
FREQUENCY ~ Hz	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	VIB AMPL ~ g	
28.0	LDG C	9000	LAT	34	1.54	
72.0	45° LT	9000	LONG	34	0.68	
92.0	45° RT	9000	VERT	34	0.71	
108.0	LDG B	9000	LONG	34	0.99	
136.0	45° RT	9000	VERT	34	0.80	
236.0	45° LT	9000	VERT	34	0.57	
312.0	45° RT	9000	VERT	34	0.55	
640.0	VMIN R/D	7000	VERT	34	1.07	
1844.0	OGE	9000	LONG	34	0.64	
1984.0	GND FLIDLE	9000	LONG	34	0.63	







ACCELERATION G'S

FIG 32

COMPRESSED VIBRATION DATA

JAN 11 1958 JAN 57-17195
GROSS WT 7000 PNO 9000 B AVG OF STR-MIC COMPTG CLEAN CORRS-ON
PULS COMPS REC-BENS-YOB REL-PAIS COMPRESSION-116

50.0

40.0

30.0

20.0

10.0

ACCELERATION G'S

MEAN ACCELERATION

MEAN RMS SIGMA UPPER RE-EL-SECTION-UNIT

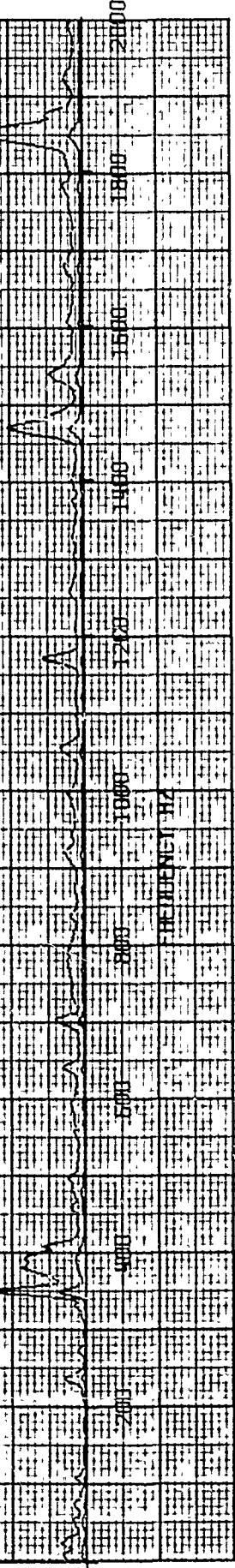
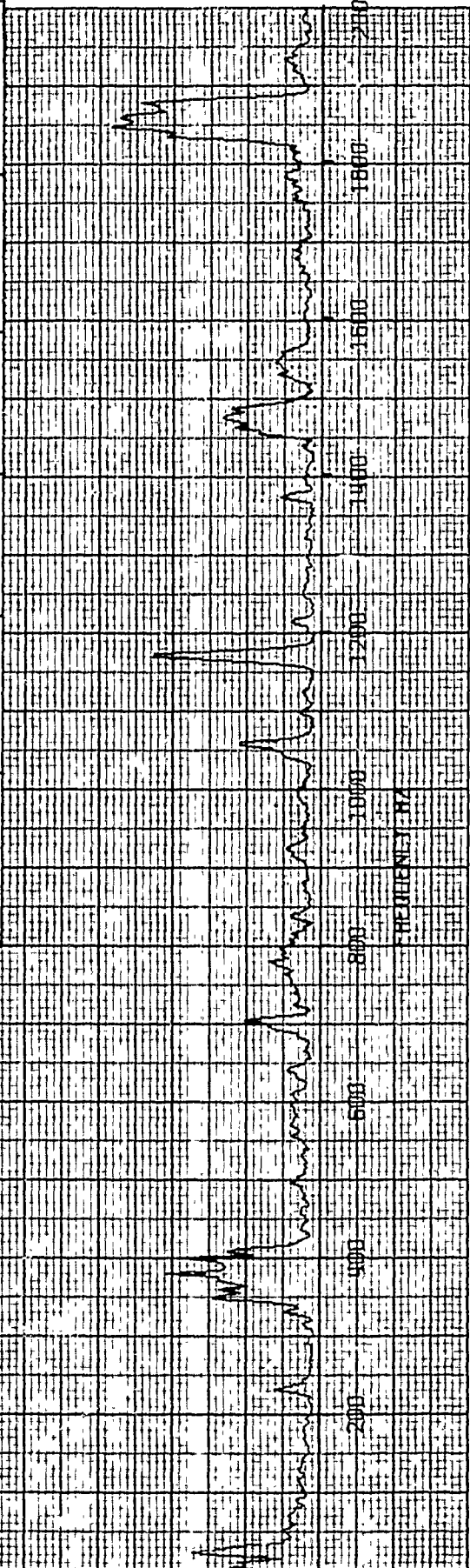
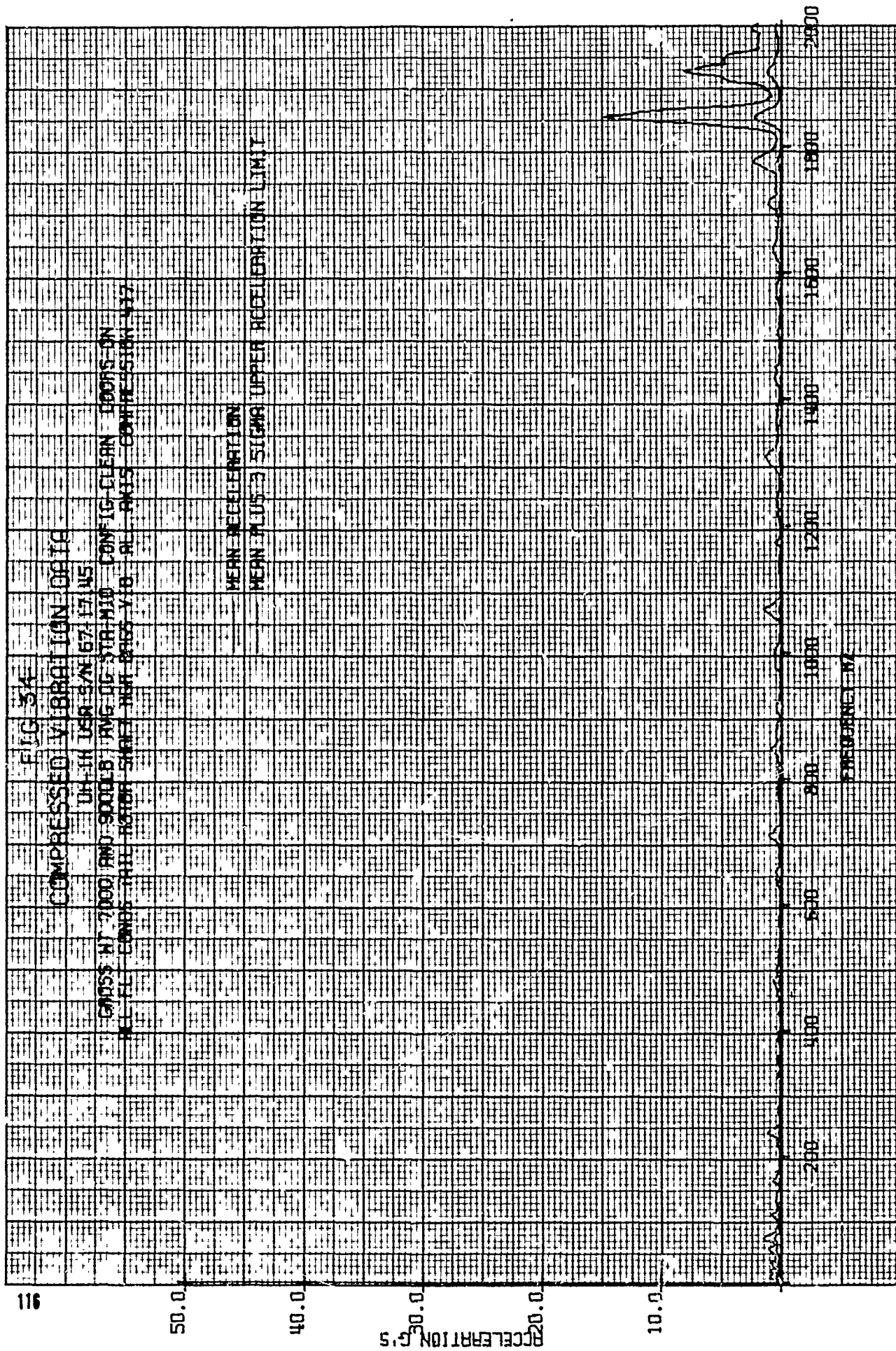


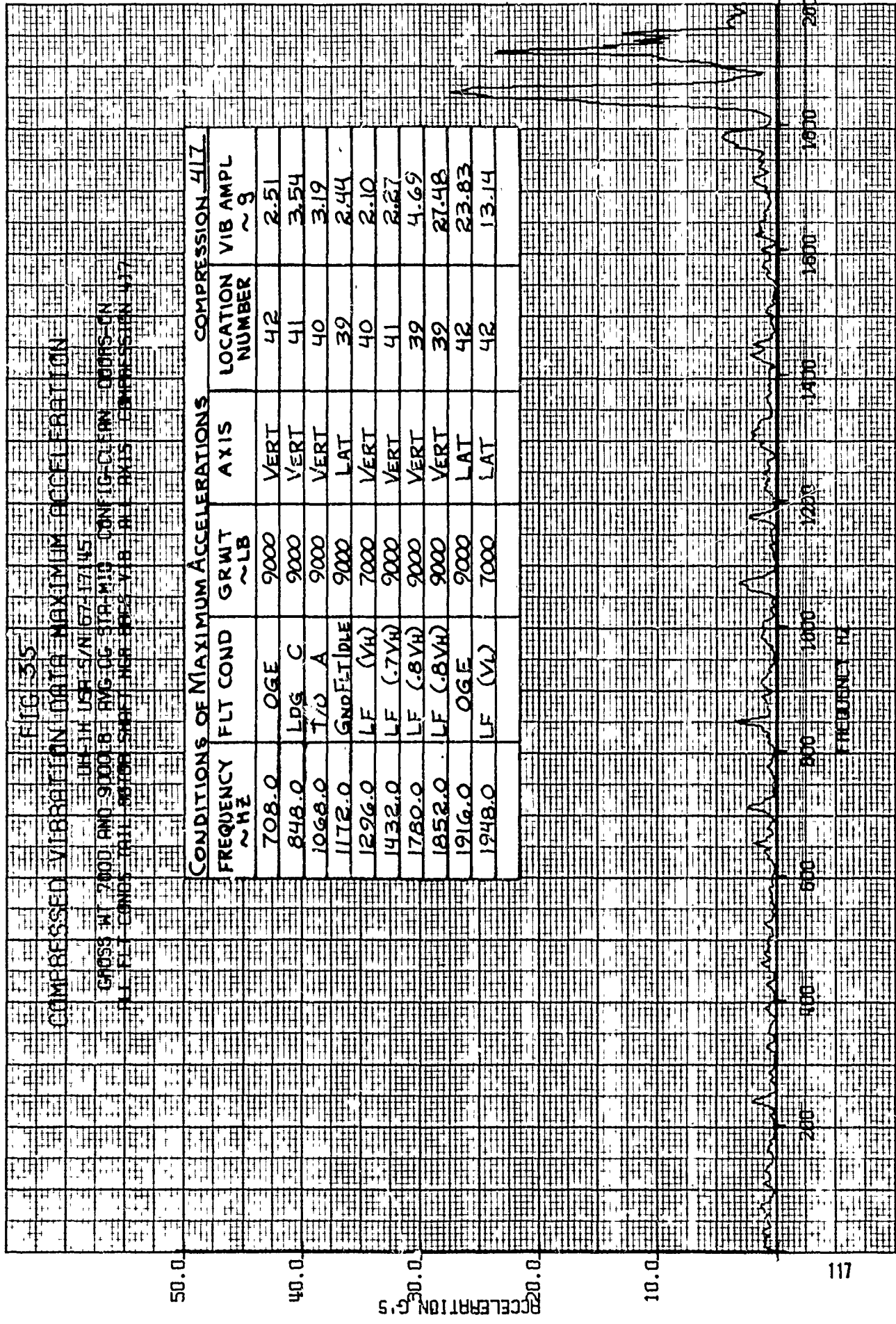
FIG 33
 COMPRESSED VIBRATION DATA - MAXIMUM ACCELERATION
 UNITH USA SN 57 17145
 GROSS WT 2000 LBS AND 9000 LBS
 ALL FL - CANS - THE TENS VIB - ALL DAYS - COMPRESSION WEG

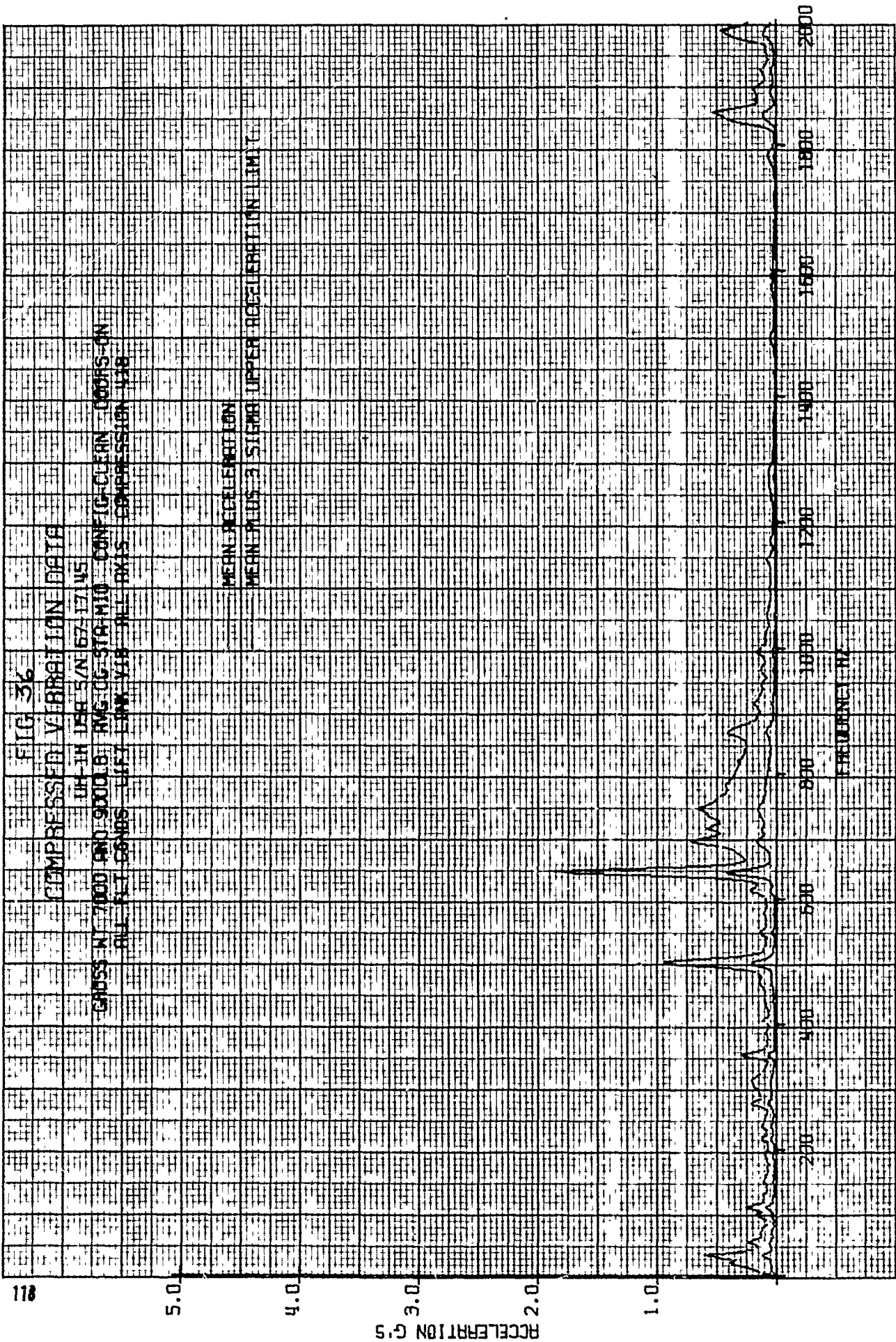
CONDITIONS OF MAXIMUM ACCELERATIONS						COMPRESSION 4/6	
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g		
24.0	LDG B	7000	LAT	36	8.59		
348.0	T/O B	9000	LONG	36	7.21		
380.0	LDG C	9000	VERT	36	10.36		
400.0	T/O B	9000	VERT	36	9.31		
1056.0	IGE	7000	LAT	38	5.40		
1168.0	GND FL/DLE	9000	LAT	37	11.42		
1472.0	LDG A	9000	LAT	38	6.71		
1844.0	30° LT	7000	LAT	37	14.33		
1856.0	VMIN R/D	7000	LAT	37	13.72		
1876.0	LDG A	9000	LAT	37	12.26		



ACCELERATION G'S







120

50.0

40.0

30.0

20.0

10.0

ACCELERATION G'S

FIG 38

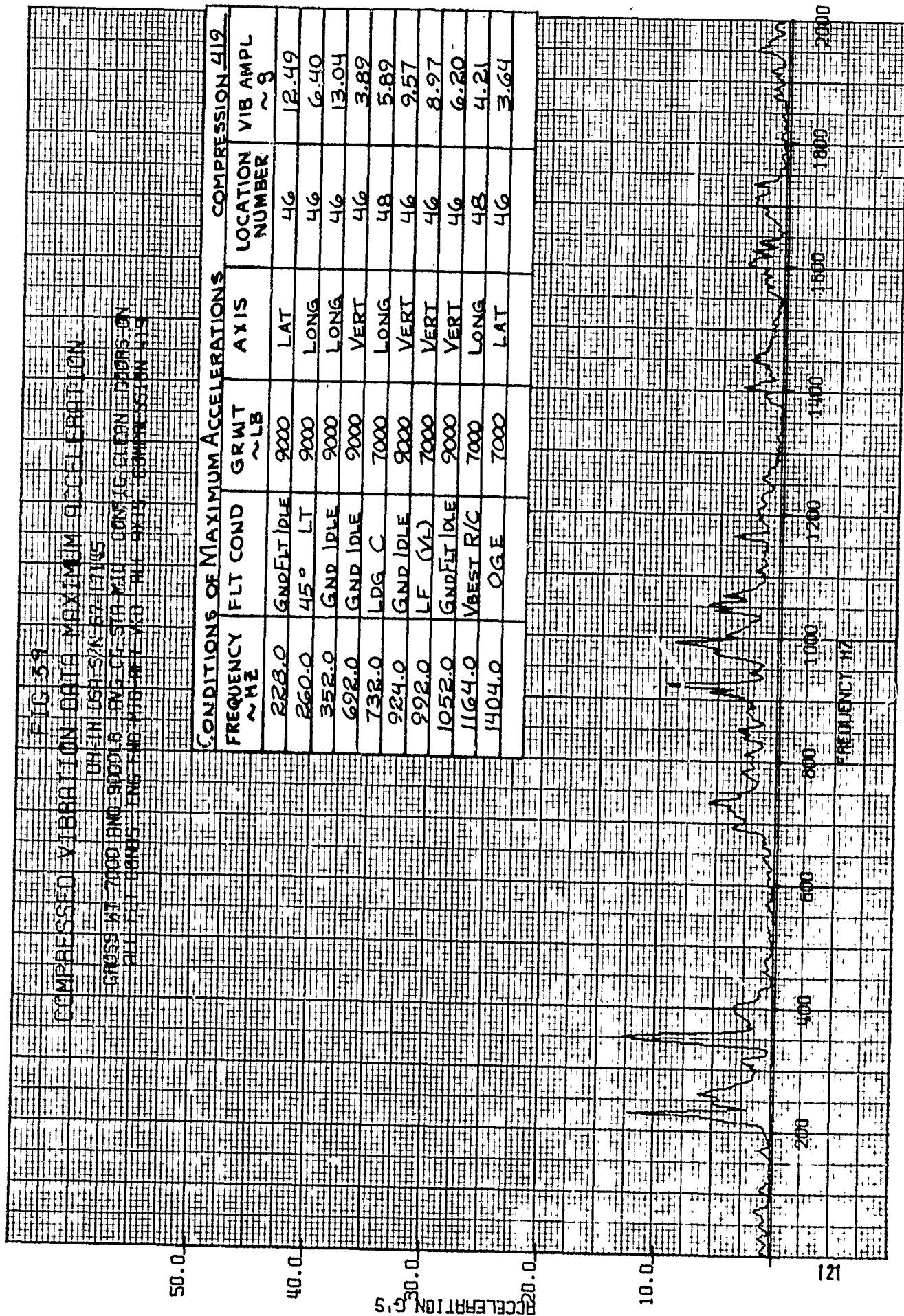
COMPRESSED VIBRATION DATA

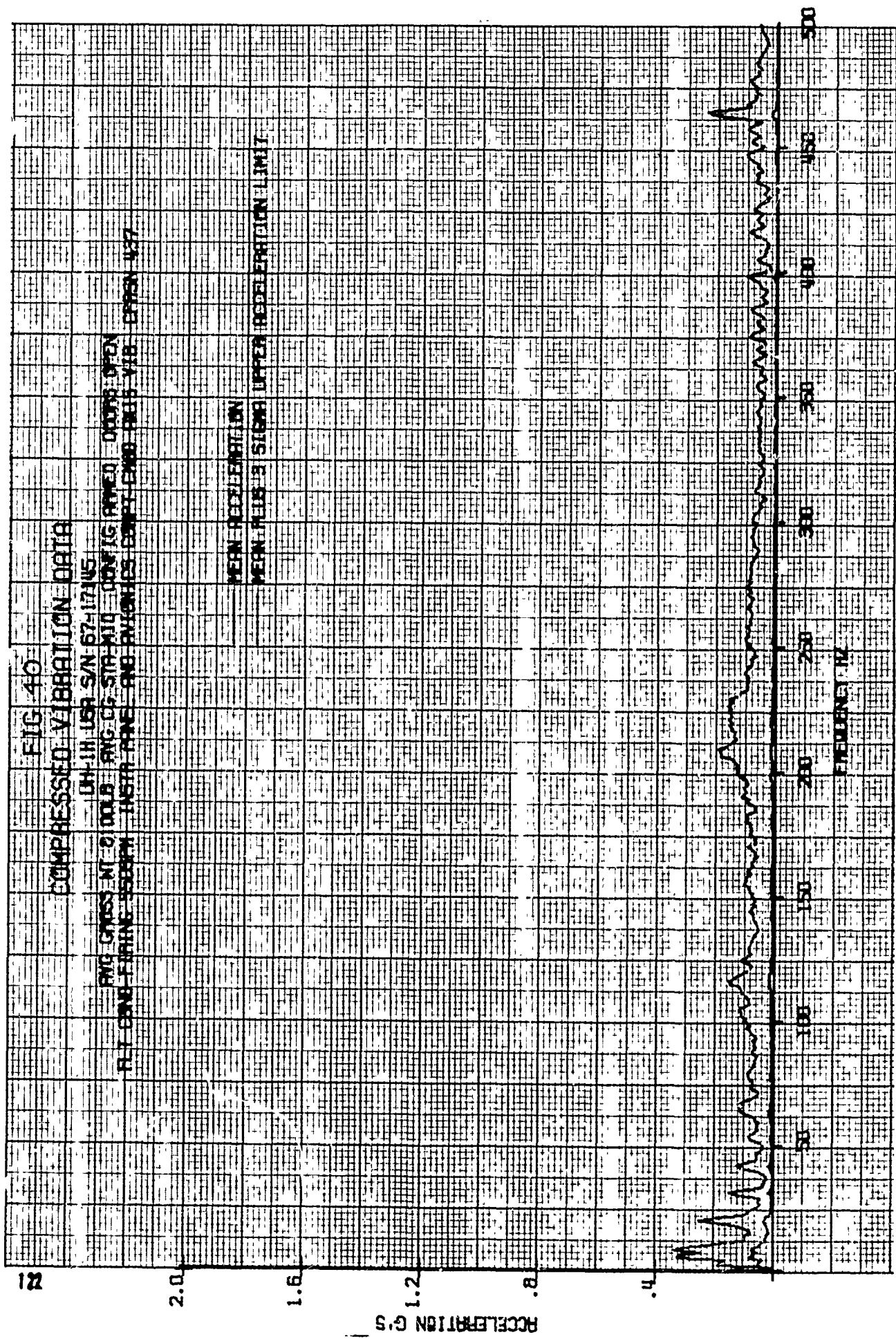
CROSS AT 7000 AND 9000 Hz
ALL FLY CONDS ENG FWD MID AFT MID ALL AXES COMPRESSION SYS
UN 1A USA S/N 67-1745
HVE-EG-51A MID LONRIG CLEAN DISRU-ON

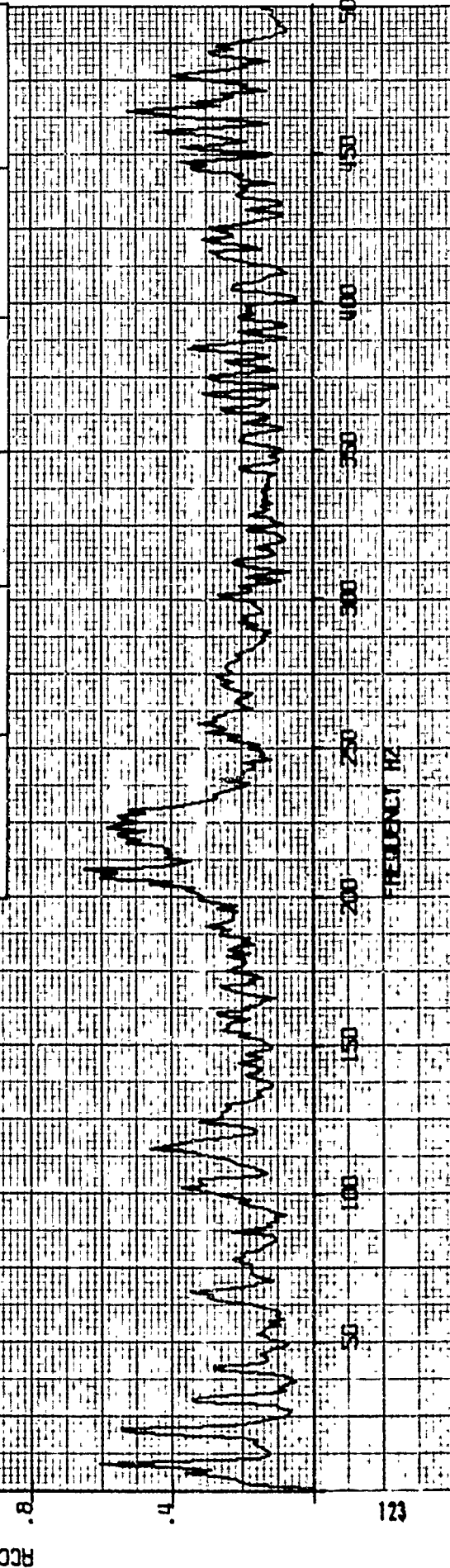
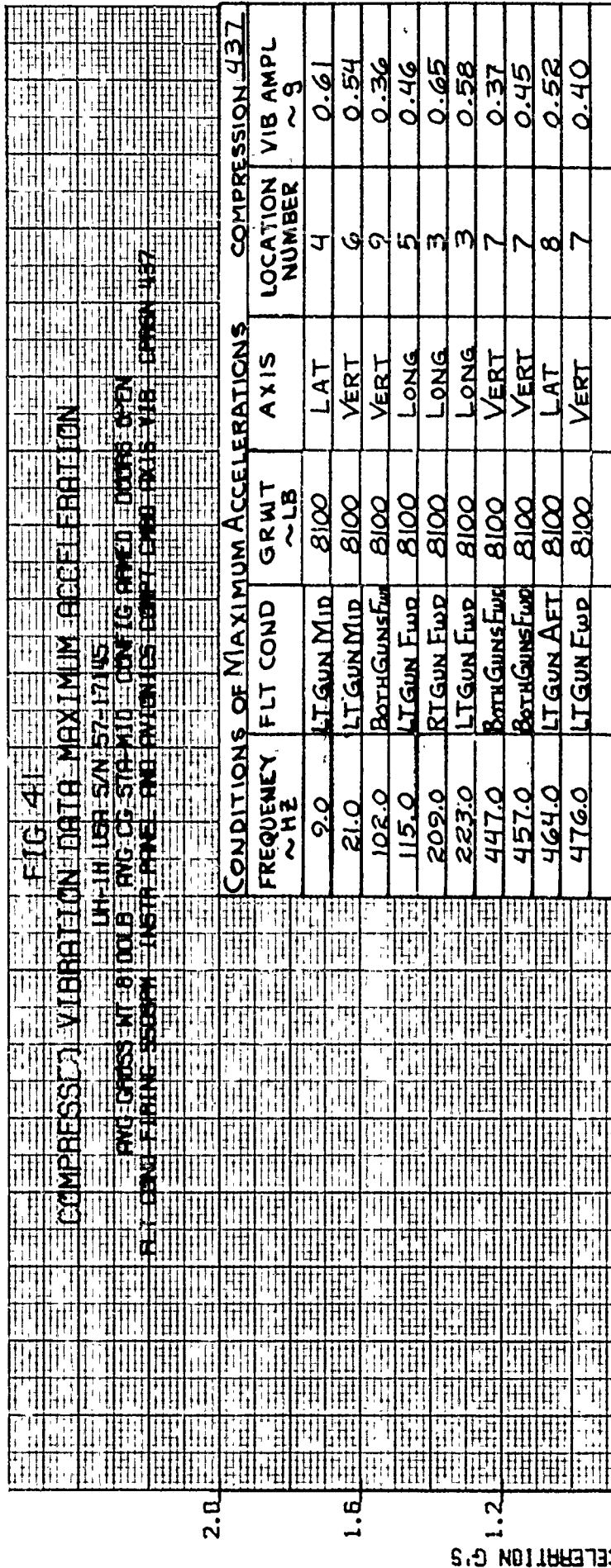
MEAN ACCELERATION
MEAN RMS 3 SIGMA UPPER ACCELERATION LIMIT

200 400 600 800 1000 1200 1400 1600 1800 2000

FREQUENCY Hz







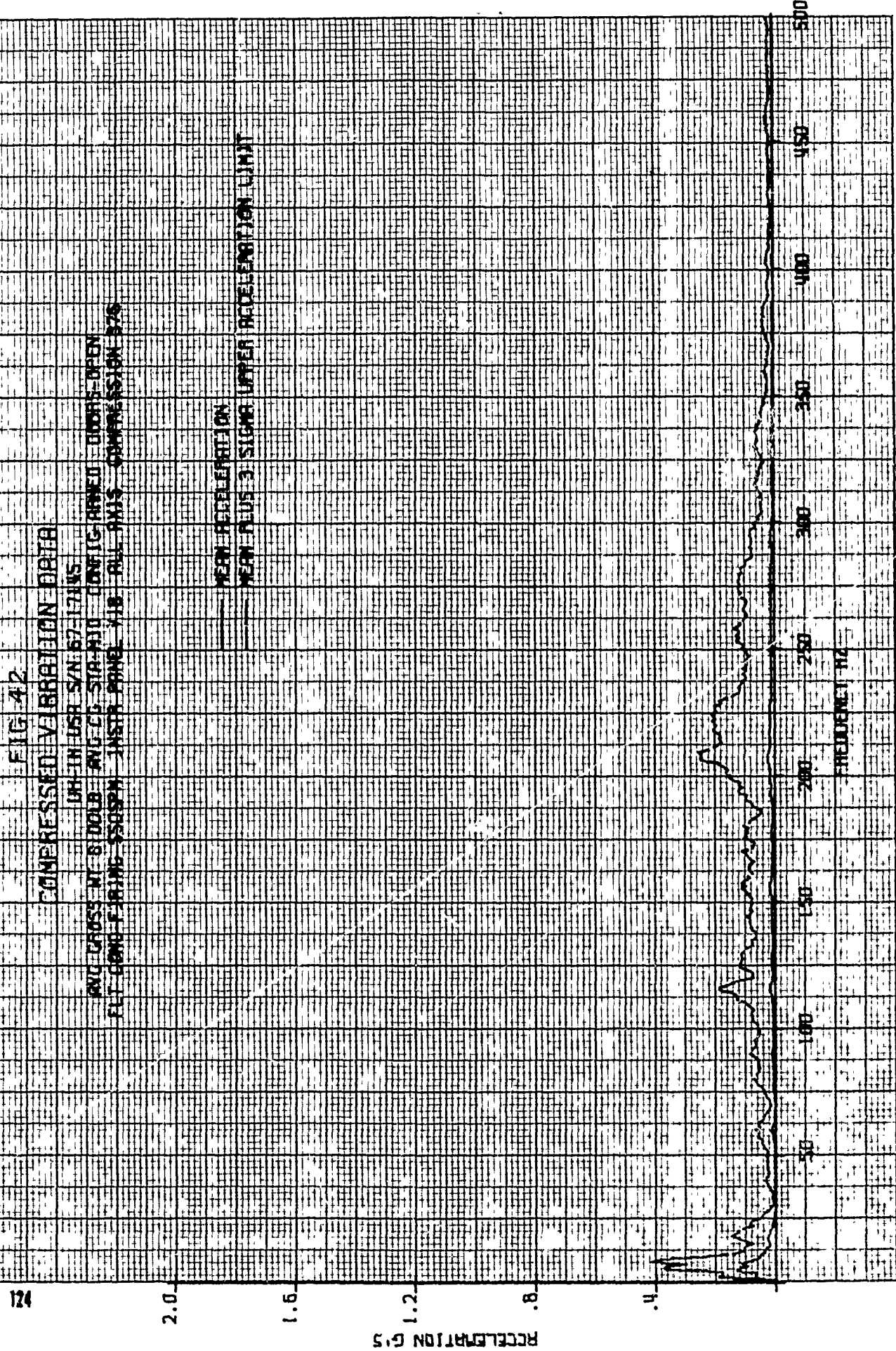


FIG 4-3									
COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION									
OR IN USR SN 67-17145									
AVG GROSS WT 8100 LB									
AVG OF STR MID LONG-ARMED DOORS OPEN									
FLT COND 5505074									
INSTR PANEL VIB ALL AXIS COMPRESSION 376									
CONDITIONS OF MAXIMUM ACCELERATIONS									
COMPRESSION 376									
FREQUENCY ~HZ									
FLT COND									
GRWT ~LB									
AXIS									
LOCATION NUMBER									
VIB AMPL ~g									
6.0									
LT GUN MID									
8100									
LONG									
5									
0.37									
9.0									
LT GUN AFT									
8100									
LAT									
4									
0.61									
115.0									
LT GUN FWP									
8100									
LONG									
5									
0.46									
125.0									
LT GUN FWP									
8100									
LONG									
5									
0.28									
162.0									
BOTH GUNS FWP									
8100									
LONG									
1									
0.24									
175.0									
LT GUN FWP									
8100									
LONG									
1									
0.24									
209.0									
RT GUN FWP									
8100									
LONG									
3									
0.65									
223.0									
LT GUN FWP									
8100									
LONG									
3									
0.58									
258.0									
BOTH GUNS FWP									
8100									
LONG									
3									
0.33									
274.0									
LT GUN FWP									
8100									
LONG									
3									
0.27									

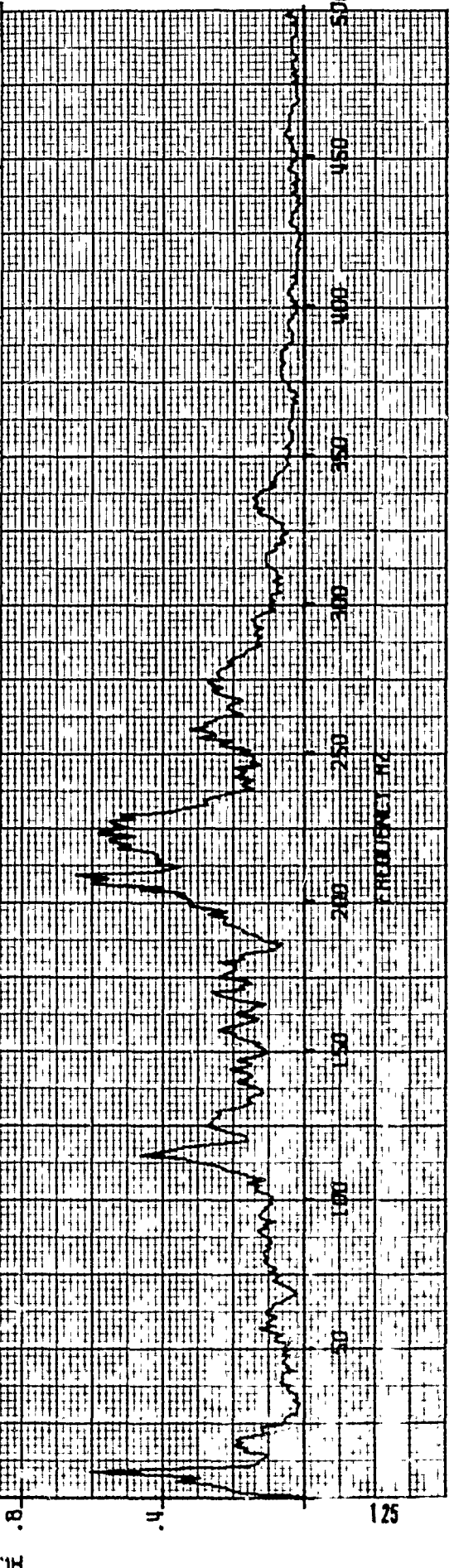


FIG 44

COMPRESSED VIBRATION DATA

UN-14 USA S/N 67-17115
 AVG GROSS WT 8100LB AVG CG STA-N10 CONFIG ARMED DOORS-OPEN
 FLT COND FIRING SEQUENCE AVIONICS COMPARTMENT V18 ALL RIS COMPRESSION 377

2.0

1.6

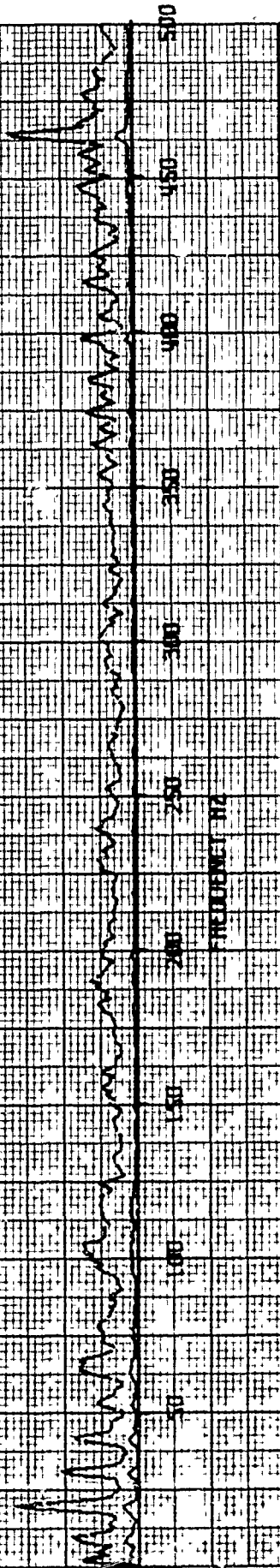
1.2

0.8

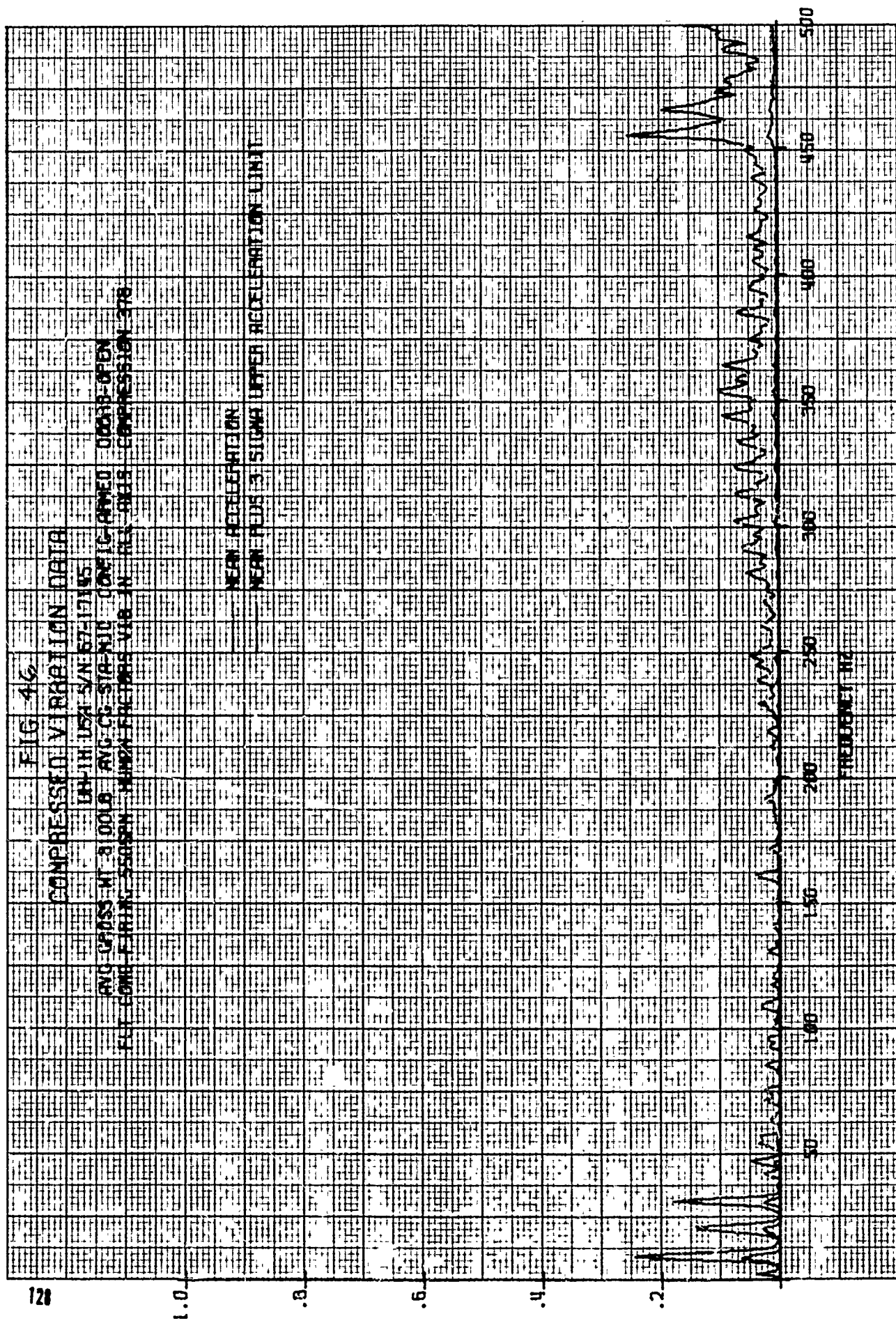
0.4

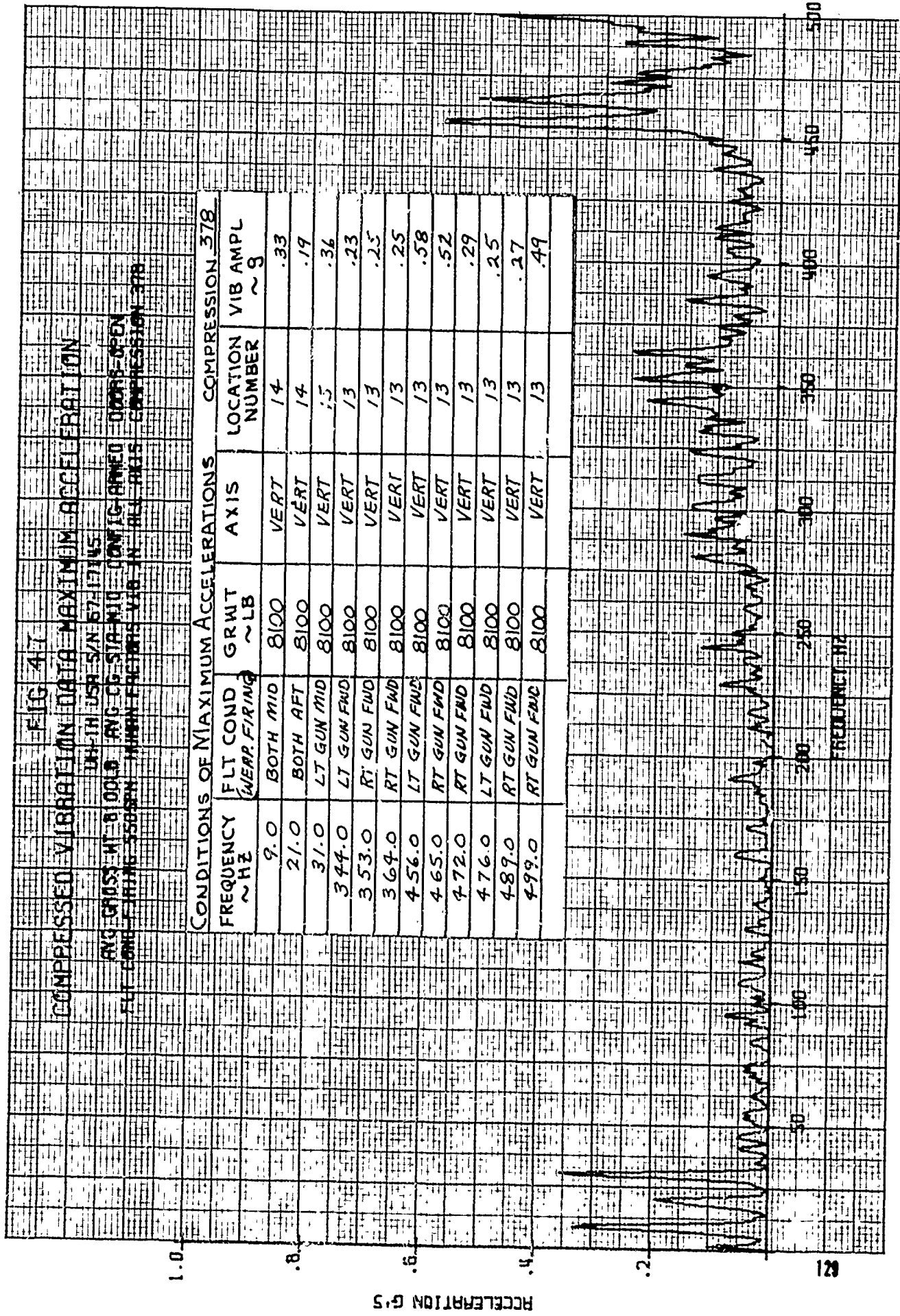
ACCELERATION G'S

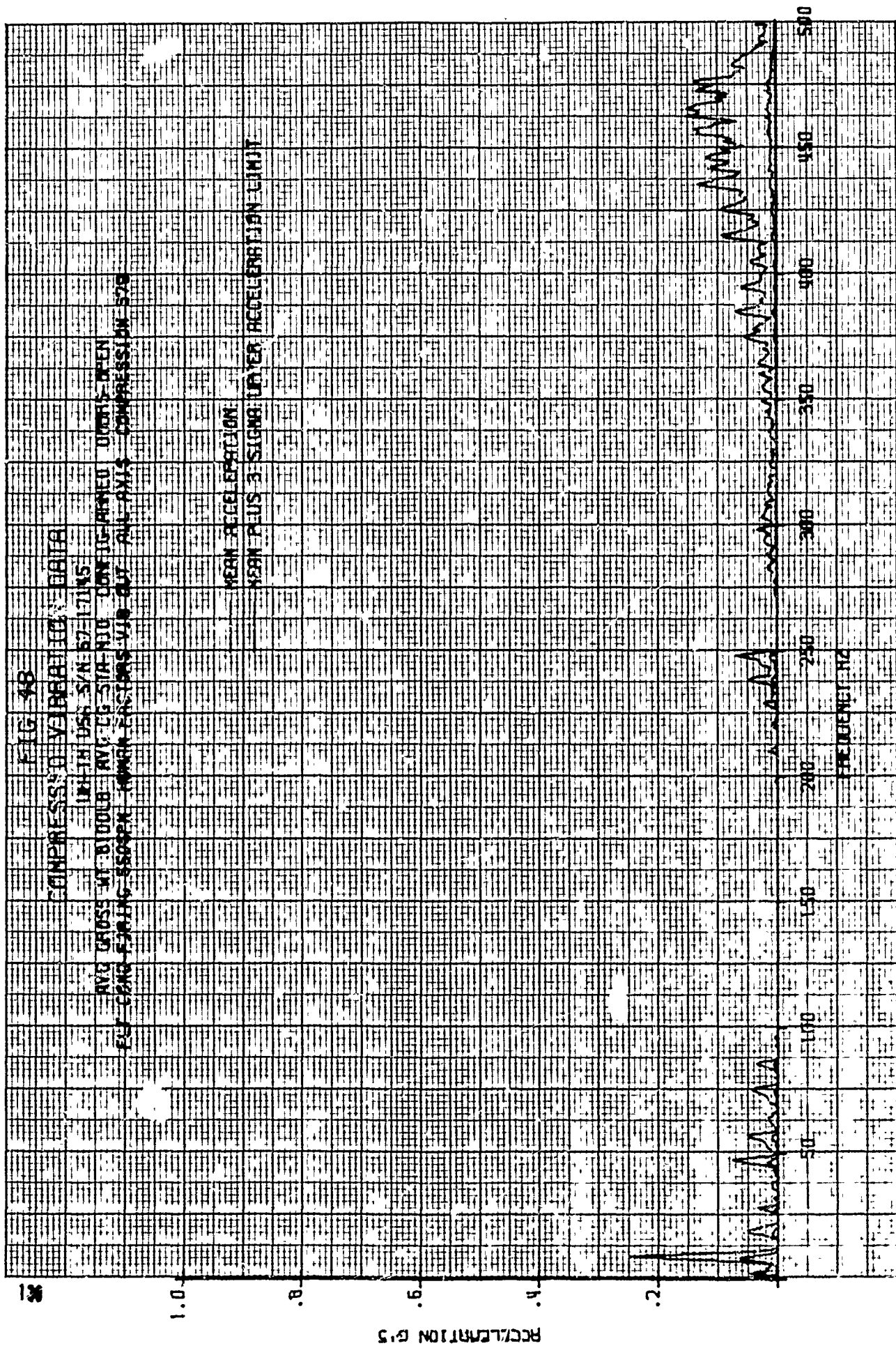
MEAN ACCELERATION
 MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

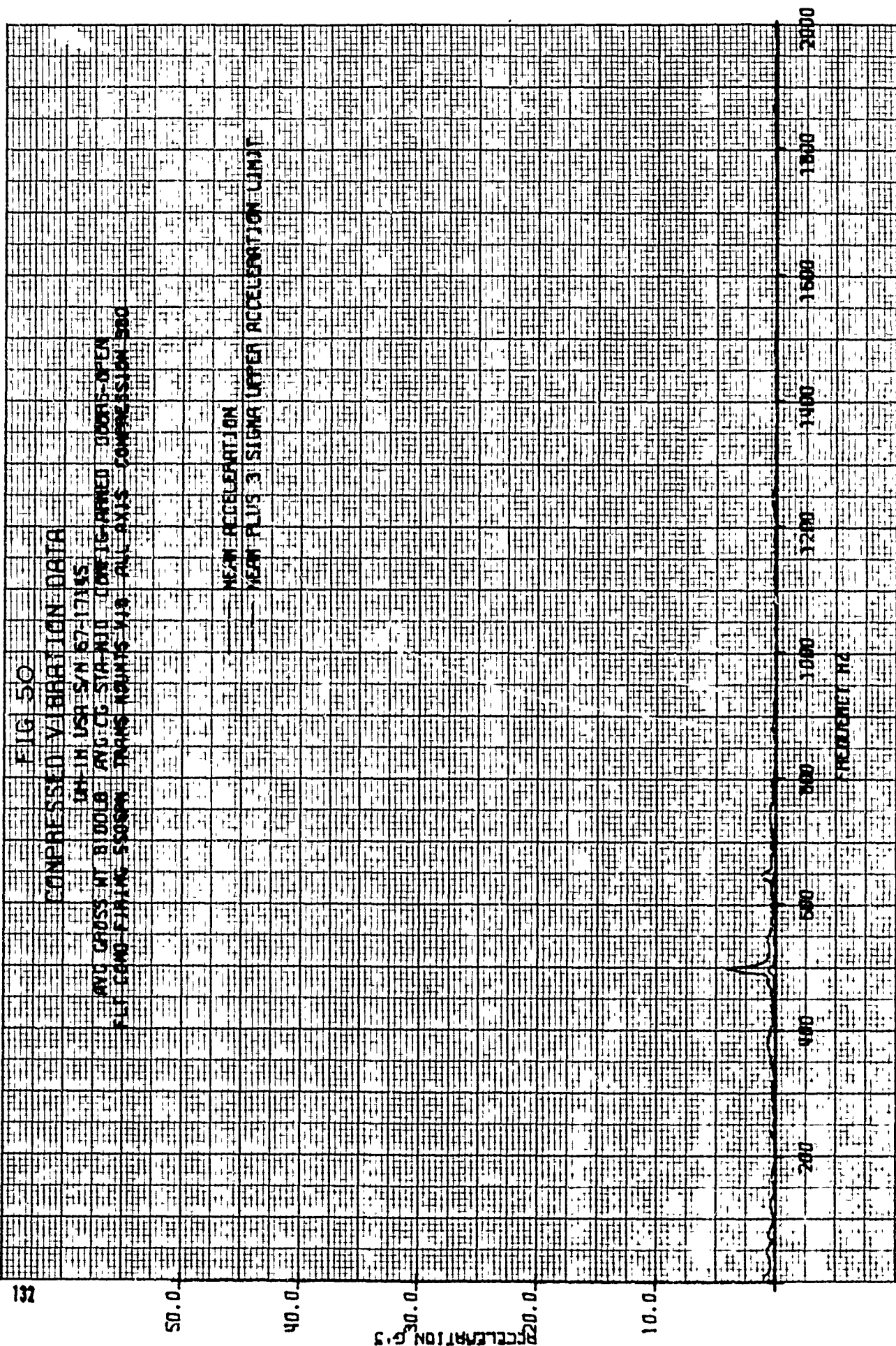


TIME SECONDS









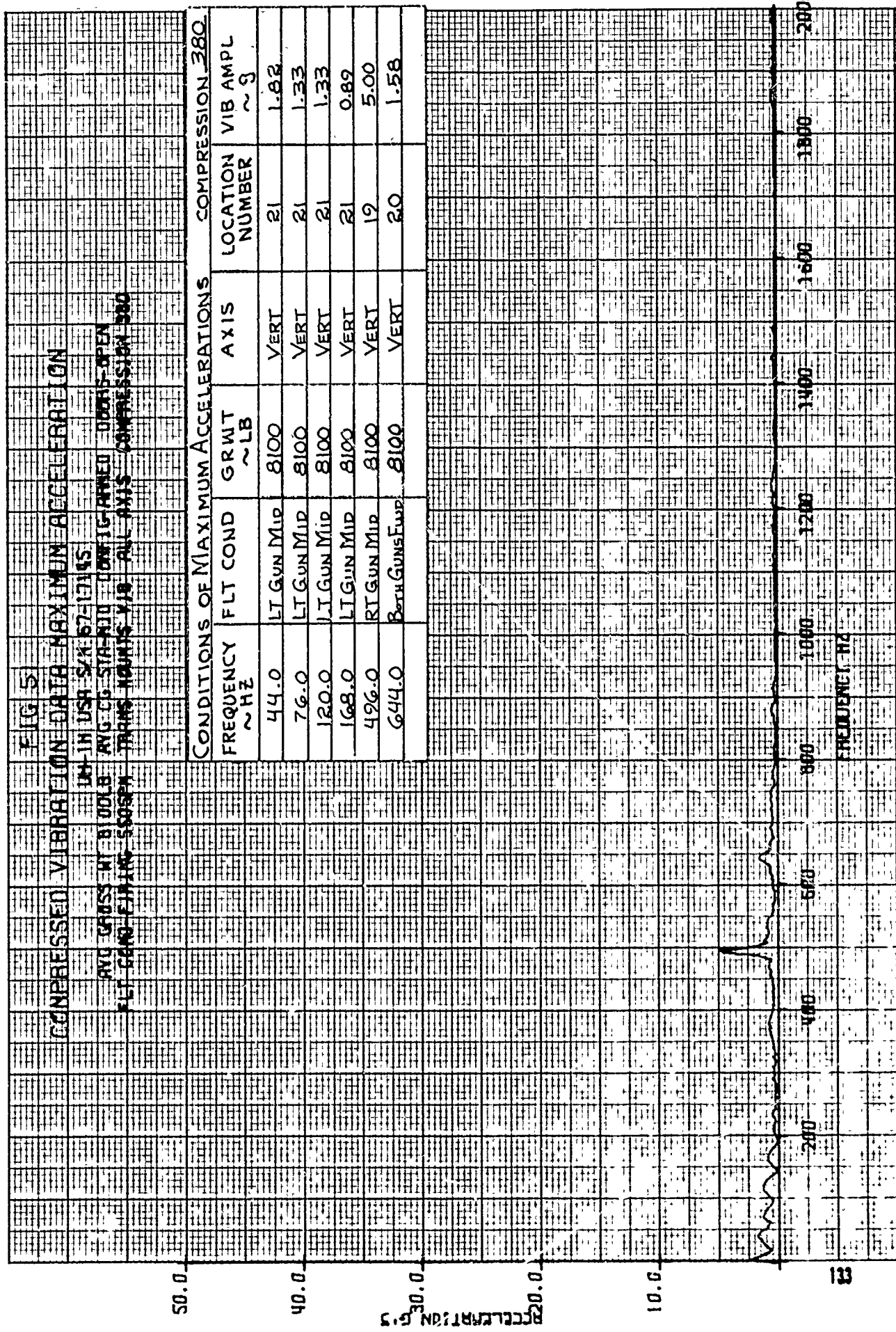
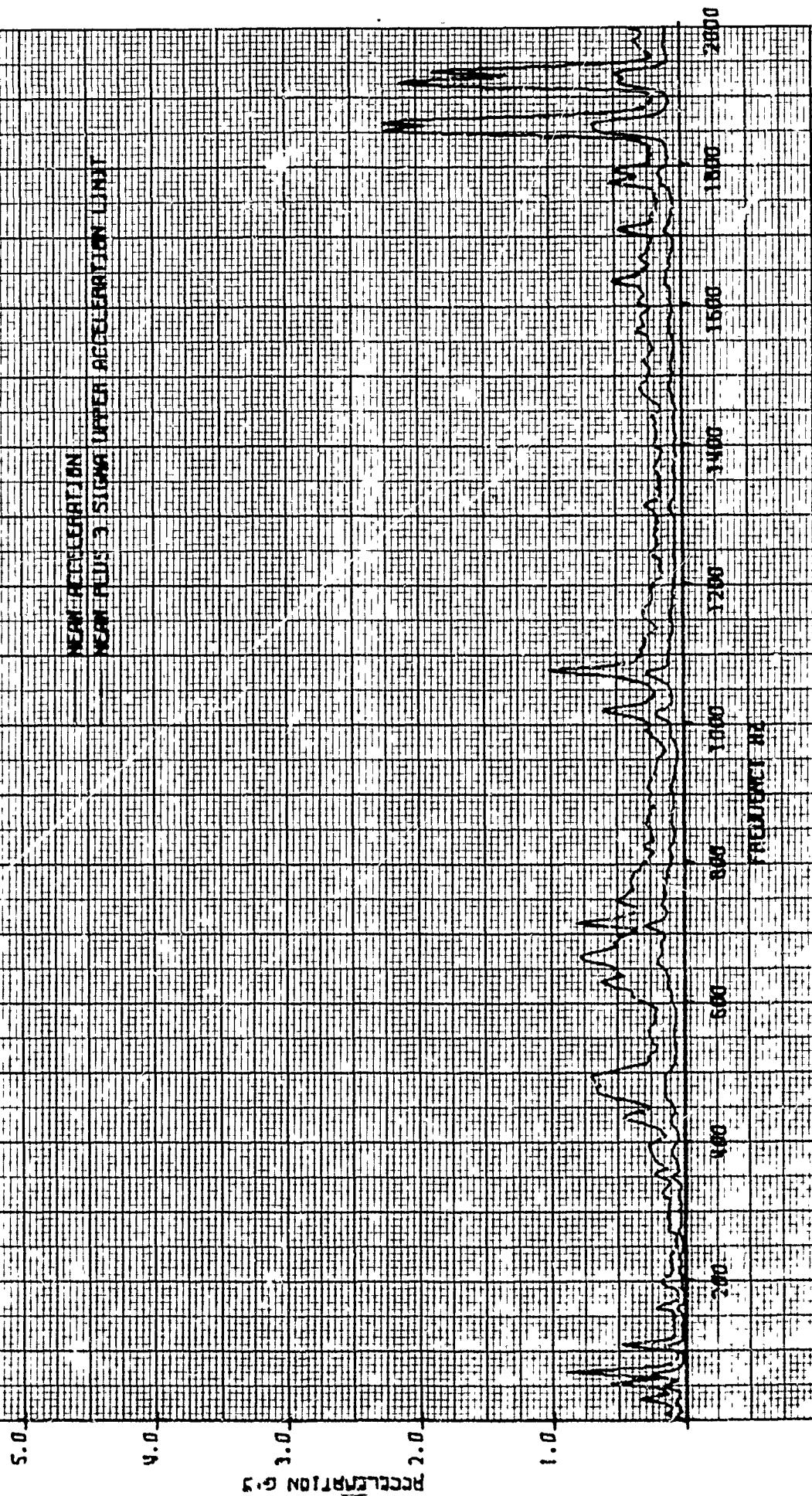


FIG 52

COMPRESSED VIBRATION DATA

IN-TR USA S/N 67-17185
 RVC GROSS WT 8.00LB RVC CG STA-M10 DOWN-ARMED 0.0000-0.01X
 FLT EMBL-FIRING 55055N TAIL BOOM REEFER #15 Y-18 REL AXIS COMPRESSION 301



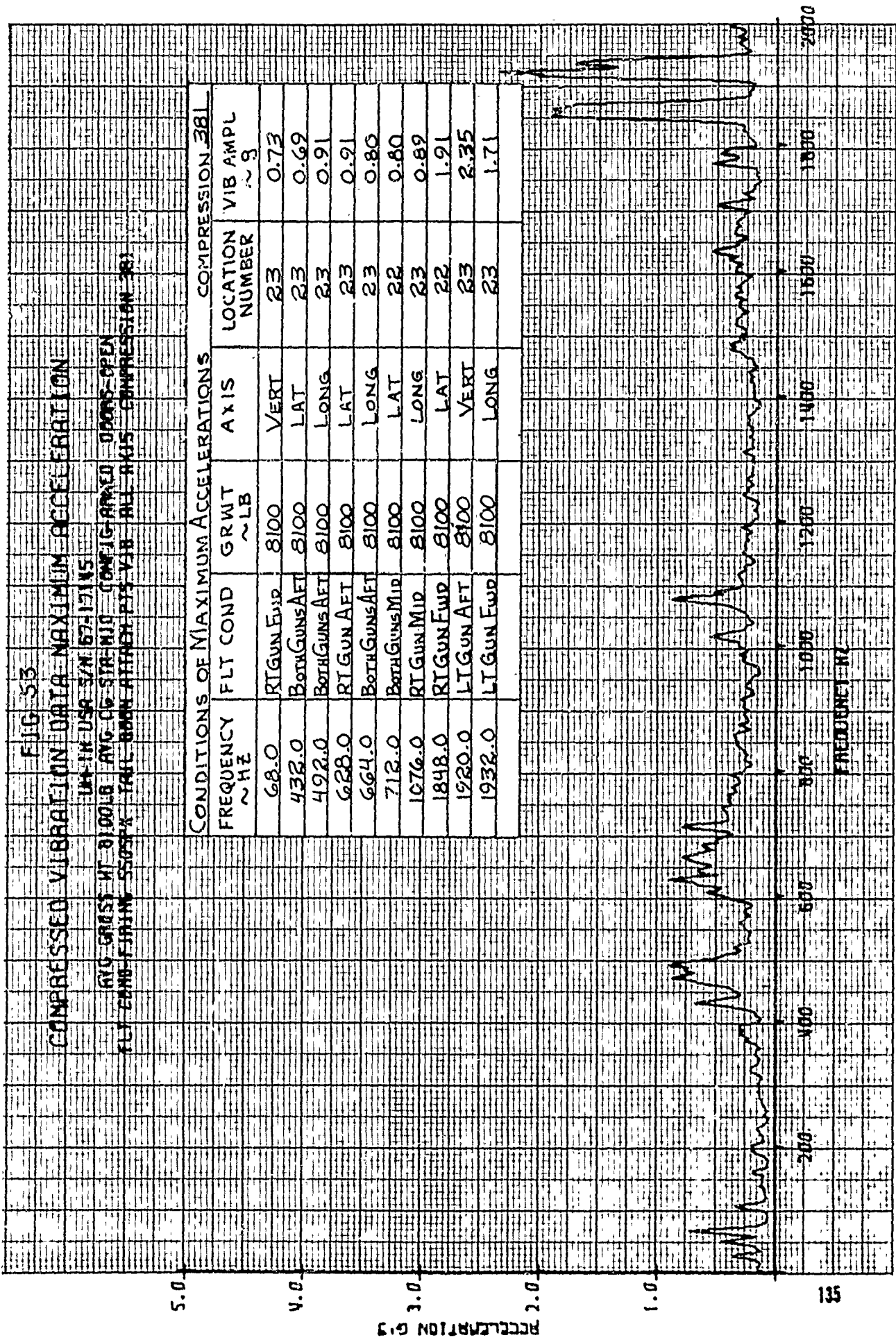


FIG. 54-

COMPRESSED VIBRATION DATA

UN-14 USA S/N 67-17145
AVG GROSS WT 800 LB
FLT COMB 1 STAGE 5500 RPM
AVG CG STA N10
DAY 10 ARMED DOORS OPEN
FLT COMB 1 STAGE 5500 RPM
ALL AXES COMPRESSION 300

MEAN ACCELERATION
MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

ACCELERATION G'S
5.0
4.0
3.0
2.0
1.0

0000

0001

0002

0003

0004

0005

0006

0007

0008

0009

0010

0011

0012

0013

0014

0015

0016

0017

0018

0019

0020

0021

0022

0023

0024

0025

0026

0027

0028

0029

0030

0031

0032

0033

0034

0035

0036

0037

0038

0039

0040

0041

0042

0043

0044

0045

0046

0047

0048

0049

0050

0051

0052

0053

0054

0055

0056

0057

0058

0059

0060

0061

0062

0063

0064

0065

0066

0067

0068

0069

0070

0071

0072

0073

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0075

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0080

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0090

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0093

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0095

0096

0097

0098

0099

0100

0101

0102

0103

0104

0105

0106

0107

0108

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0115

0116

0117

0118

0119

0120

0121

0122

0123

0124

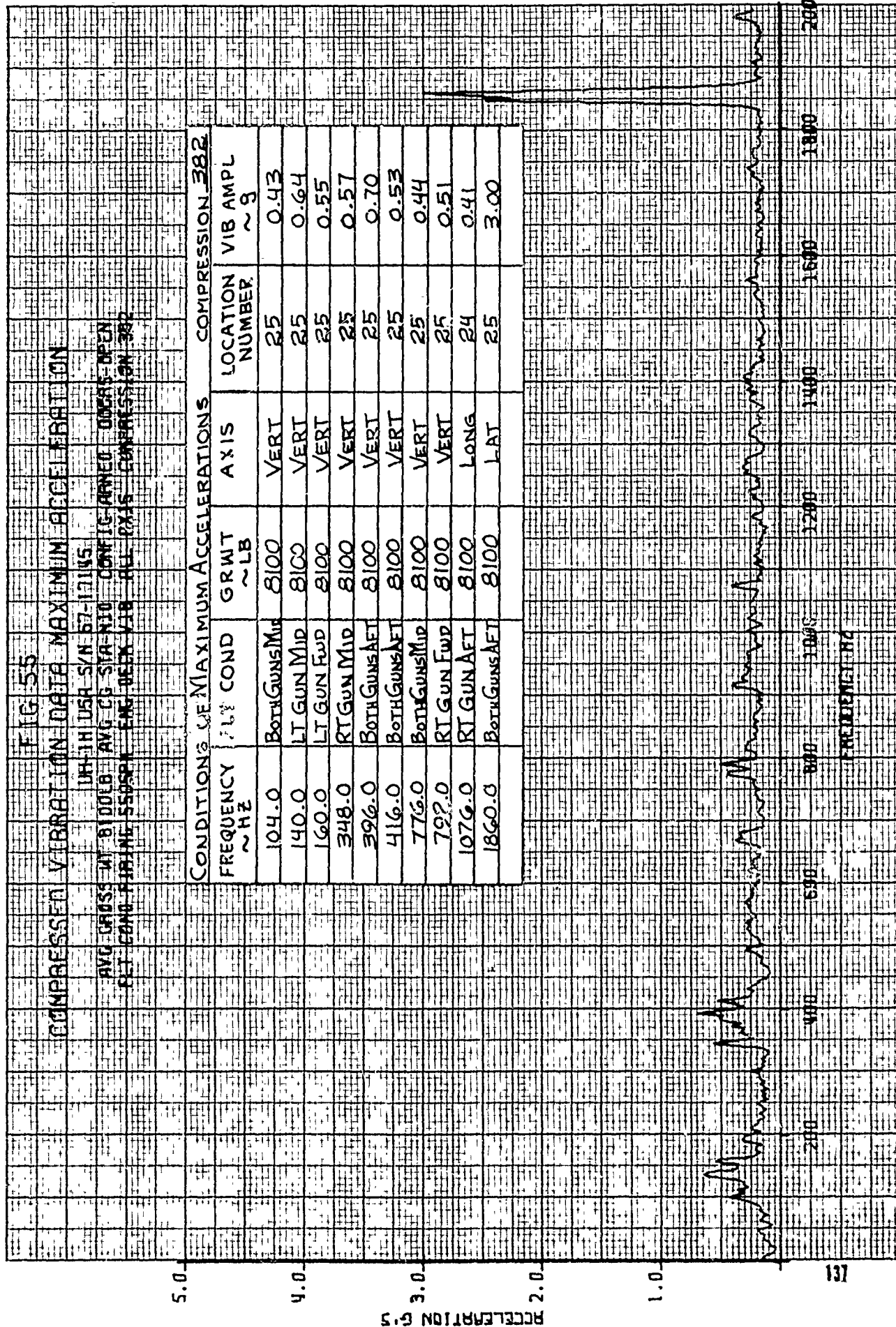


FIG 57
COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UN IN USE S/N 67-17115
AVG CG STR-MID COMBIG ARMED DOORS OPEN
FLT BAND FIRING 5500PM ENG FIREARMEL V38 ALL AXIS COMPRESSION 383

COMPRESSION 383

CONDITIONS OF MAXIMUM ACCELERATIONS

FREQUENCY ~ HZ	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	VIB AMPL ~ g
164.0	LT GUN FWD	8100	LONG	27	0.58
204.0	BOTH GUNS AFT	8100	LONG	27	0.95
220.0	BOTH GUNS AFT	8100	LONG	27	1.18
276.0	BOTH GUNS AFT	8100	LONG	27	0.77
348.0	BOTH GUNS AFT	8100	VERT	27	3.22
388.0	RT GUN AFT	8100	VERT	27	4.34
396.0	LT GUN FWD	8100	VERT	27	4.15
500.0	LT GUN FWD	8100	LONG	26	0.82
548.0	LT GUN FWD	8100	LONG	26	0.68
1860.0	BOTH GUNS FWD	8100	LAT	26	0.82

ACCELERATION G'S

1.0

2.0

4.0

5.0

1000

1200

1400

1600

1800

2000

FREQUENCY HZ



41

FIG 58

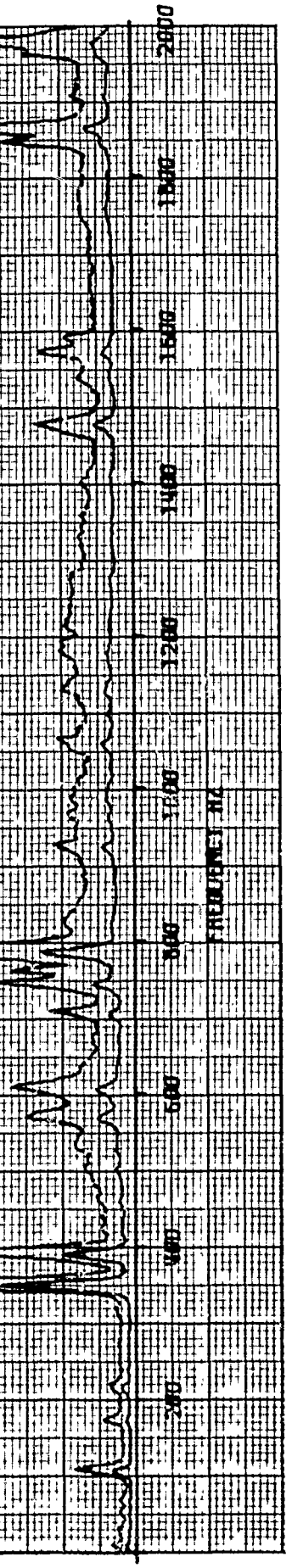
COMPRESSED VIBRATION DATA

6V6 GROSS WT 8.00 LB. UN IN USN S/N 67-17145
AVG. CG STA-MIT TONIG-ARMED DOORS-OPEN
FLT CODE-17145-550SPN ENG MEASUREMENTS-V18 ALL AXES COMPRESSION 300

ACCELERATION G'S

5.0
4.0
3.0
2.0
1.0

MEAN ACCELERATION
MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT



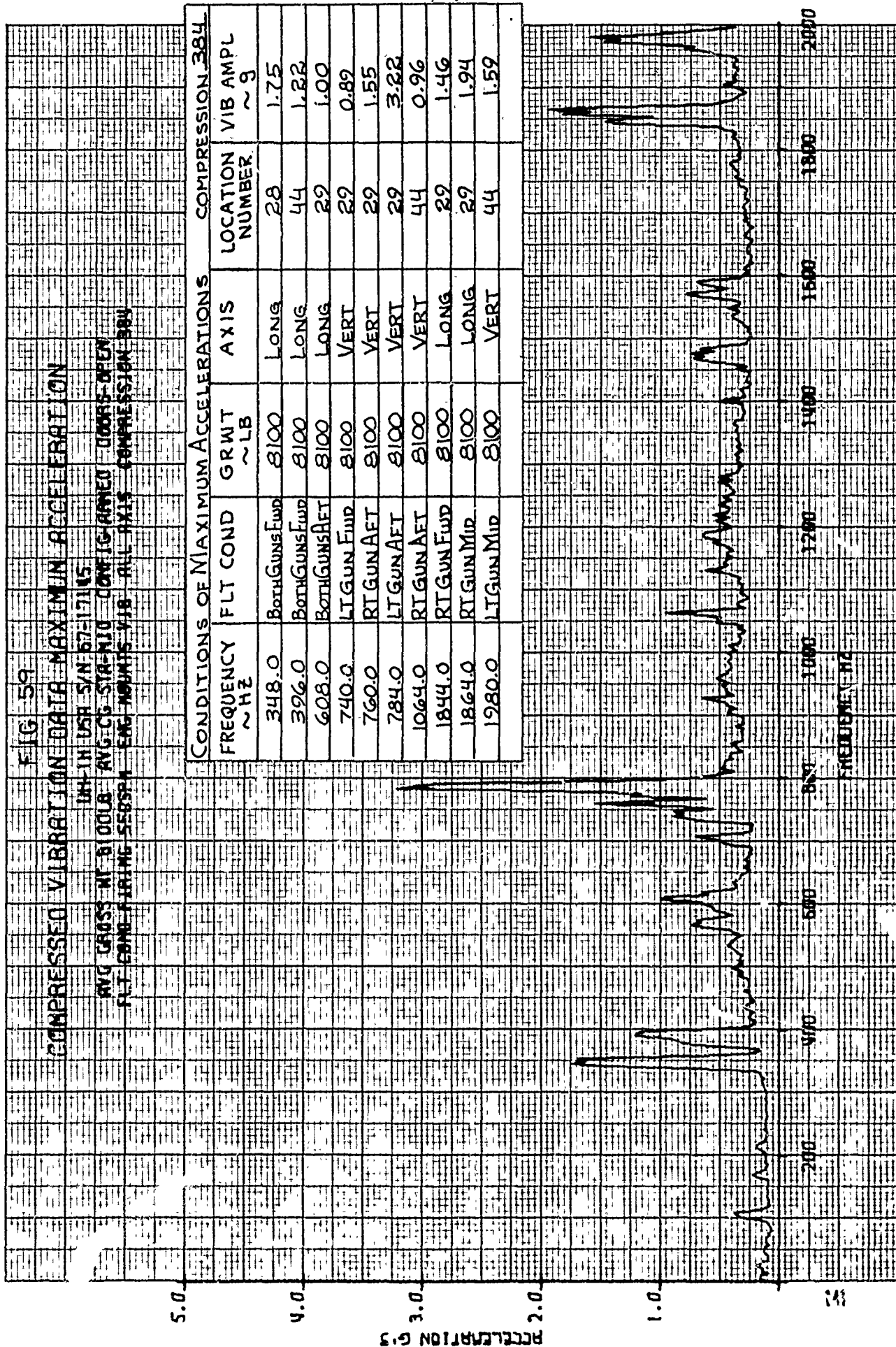
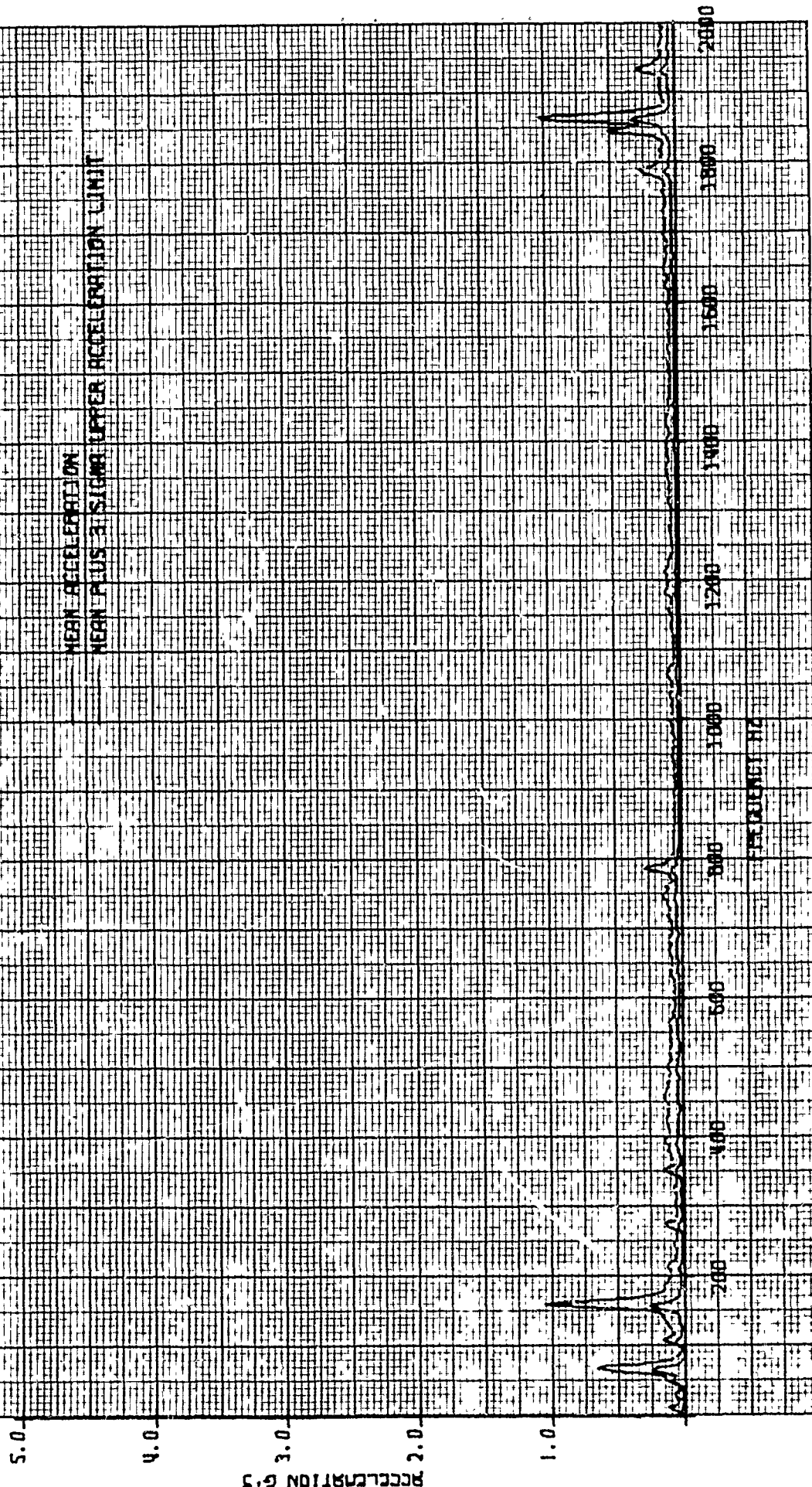


FIG 60

COMPRESSED VIBRATION DATA

UN-THRESH SYN 67-17145
 AVG GROSS WT 8100LB AVG CG STA-H20 CONFIG-ORIENT DOOR-OPEN
 FUE 0240 FUELING 5500PM TAIL ROTOR SERVO VIB RL 0015 COMPRESSION 30S

MEAN ACCELERATION
 MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT



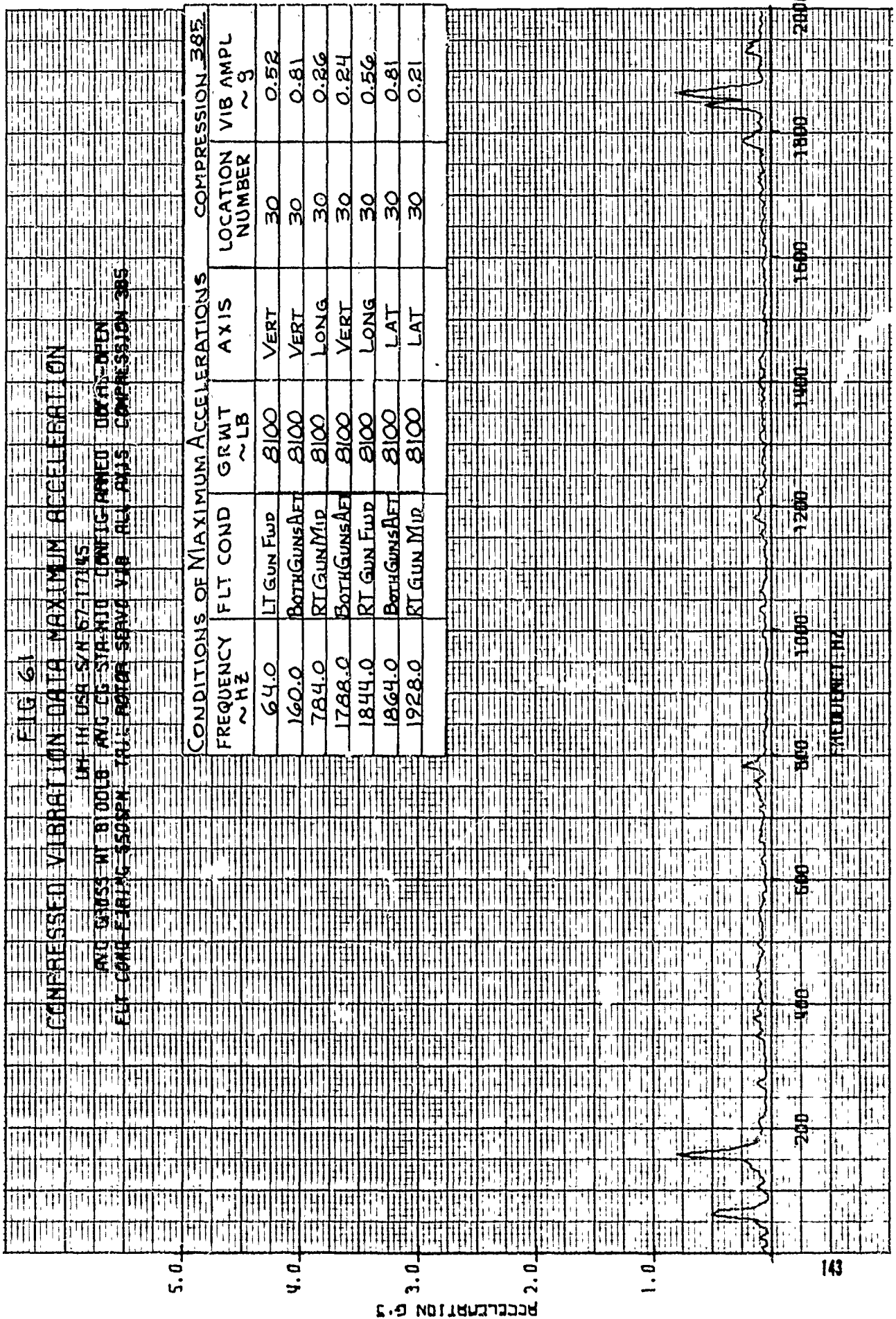
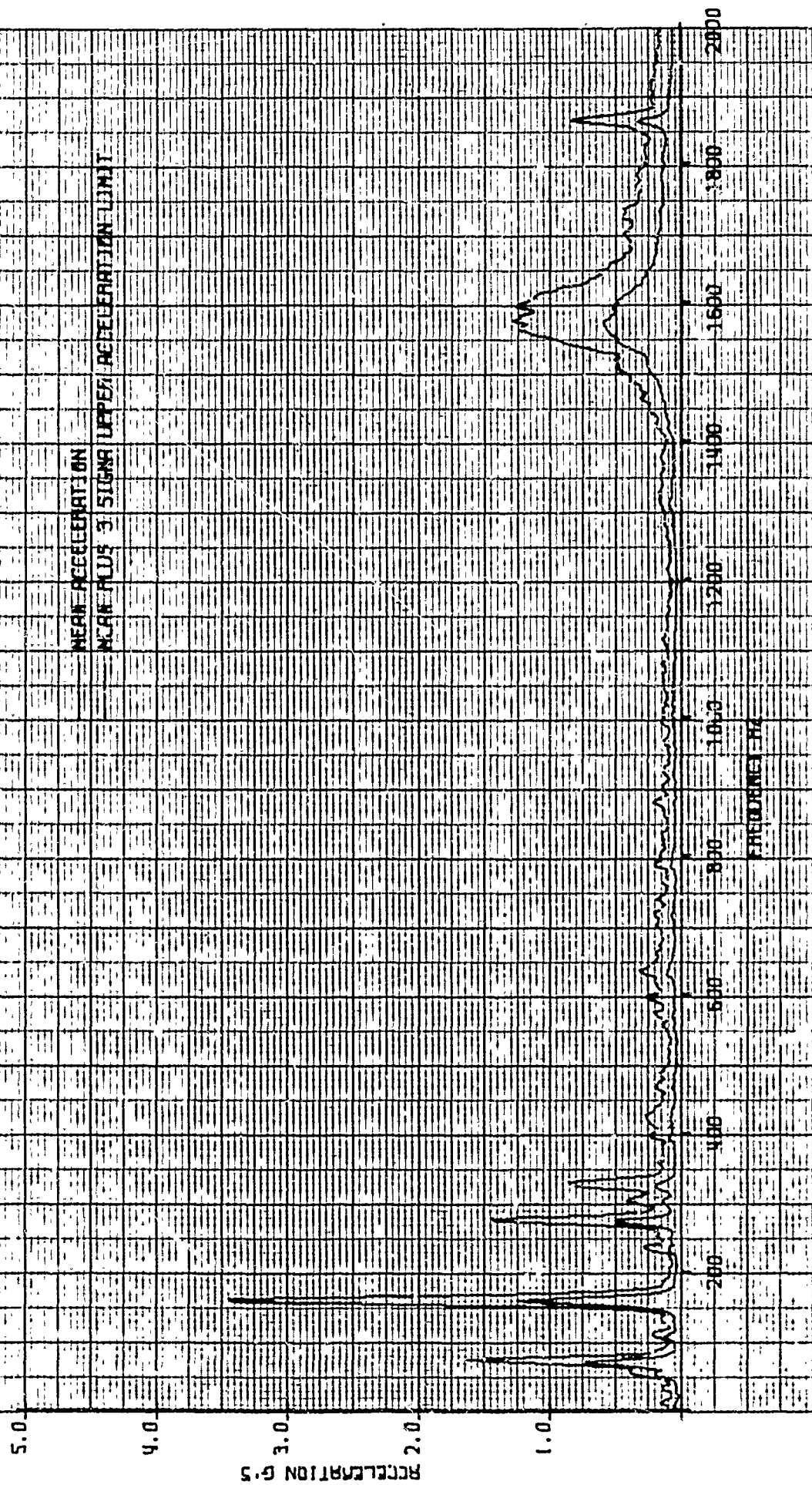
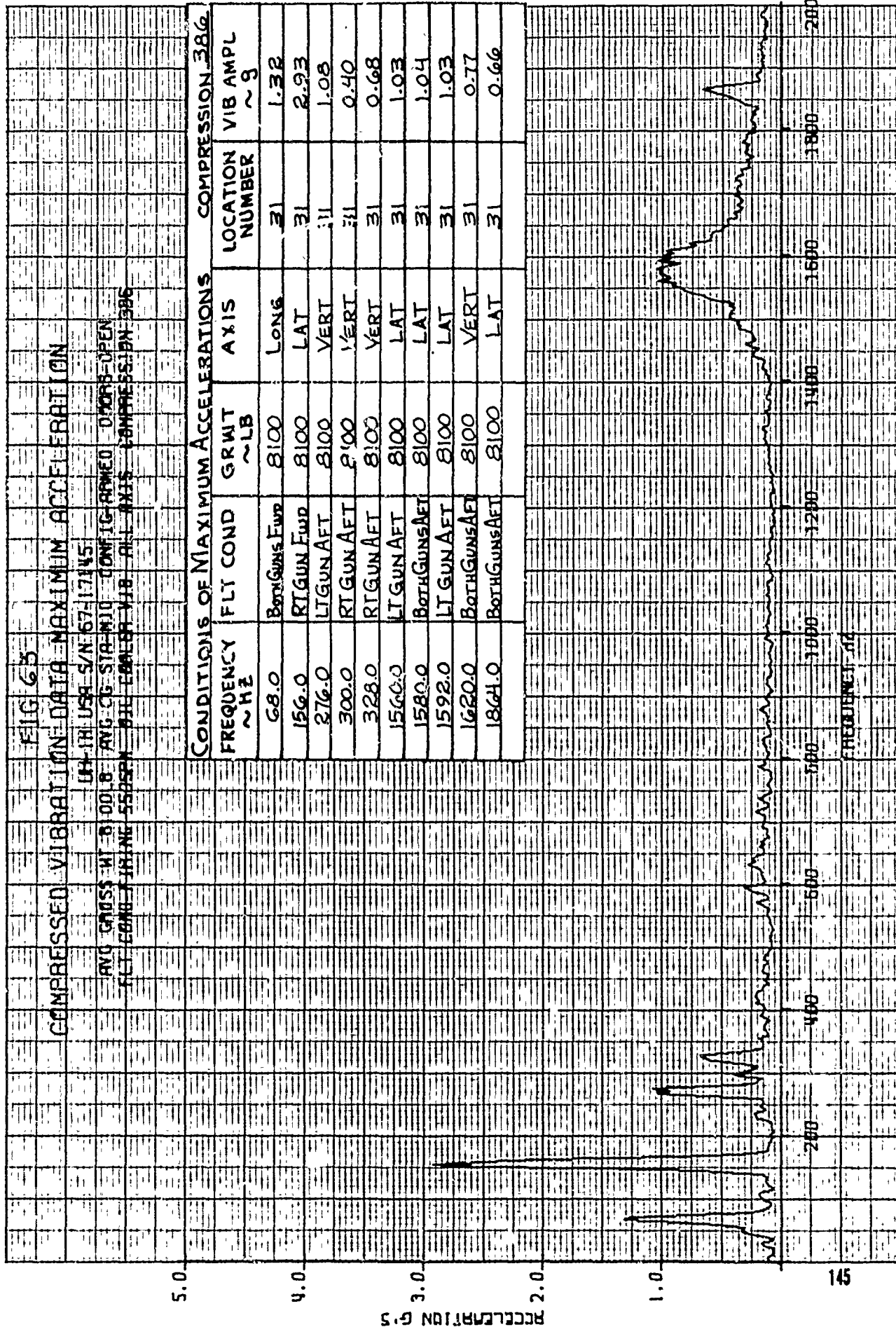


FIG 62

COMPRESSED VIBRATION DATA

PWC GROSS WT 3100LB, AVG CG STA-M10, CONFIG-ARMED, UNDRS-OPEN
 FLT EMBB FIRING 550SPN, 310 EMBB V18, ALL AXES COMPRESSION 385
 UH-1H USA S/N 67-171451





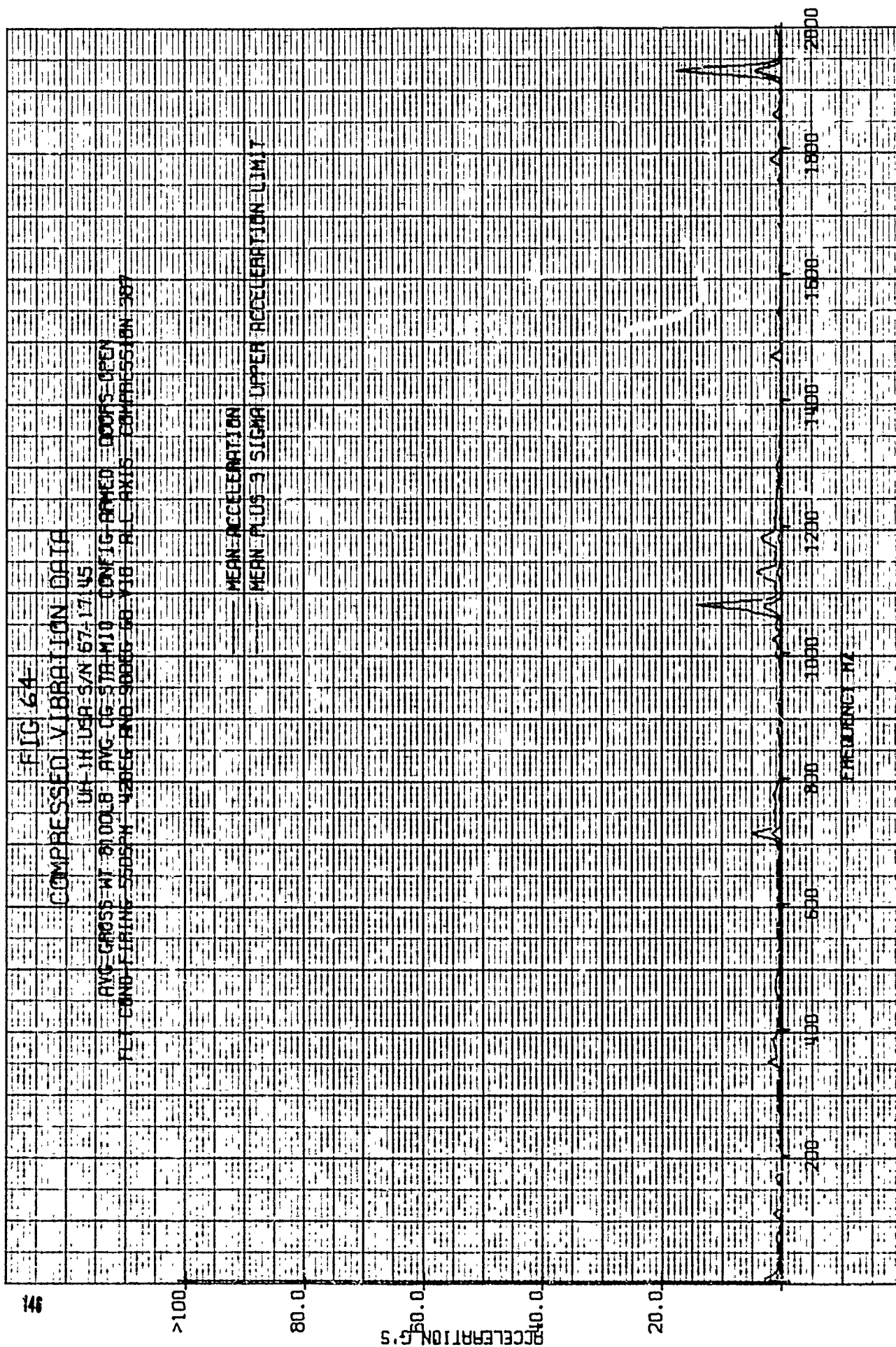


FIG 65

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UH-1H USA S/N 67-17145
 AVG GROSS WT 8100 LB AVG CG STR-M10 COMB IG-ARMED DOORS OPEN
 FLT COND FERRY 5505PM 0205G AND 9000G 58-138 ALL AXIS COMPRESSION 38Z

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 38Z	
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB AMPL ~g	
348.0	BOTH GUNS MID	8100	LONG	32	4.52	
1076.0	BOTH GUNS AFT	8100	LONG	31	11.58	
1128.0	BOTH GUNS AFT	8100	VERT	31	4.24	
1176.0	LT GUN FWD	8100	VERT	31	3.73	
1468.0	BOTH GUNS MID	8100	LONG	32	4.16	
1928.0	LT GUN AFT	8100	LONG	32	12.05	

>100

80.0

60.0
ACCELERATION G'S

40.0

20.0

0

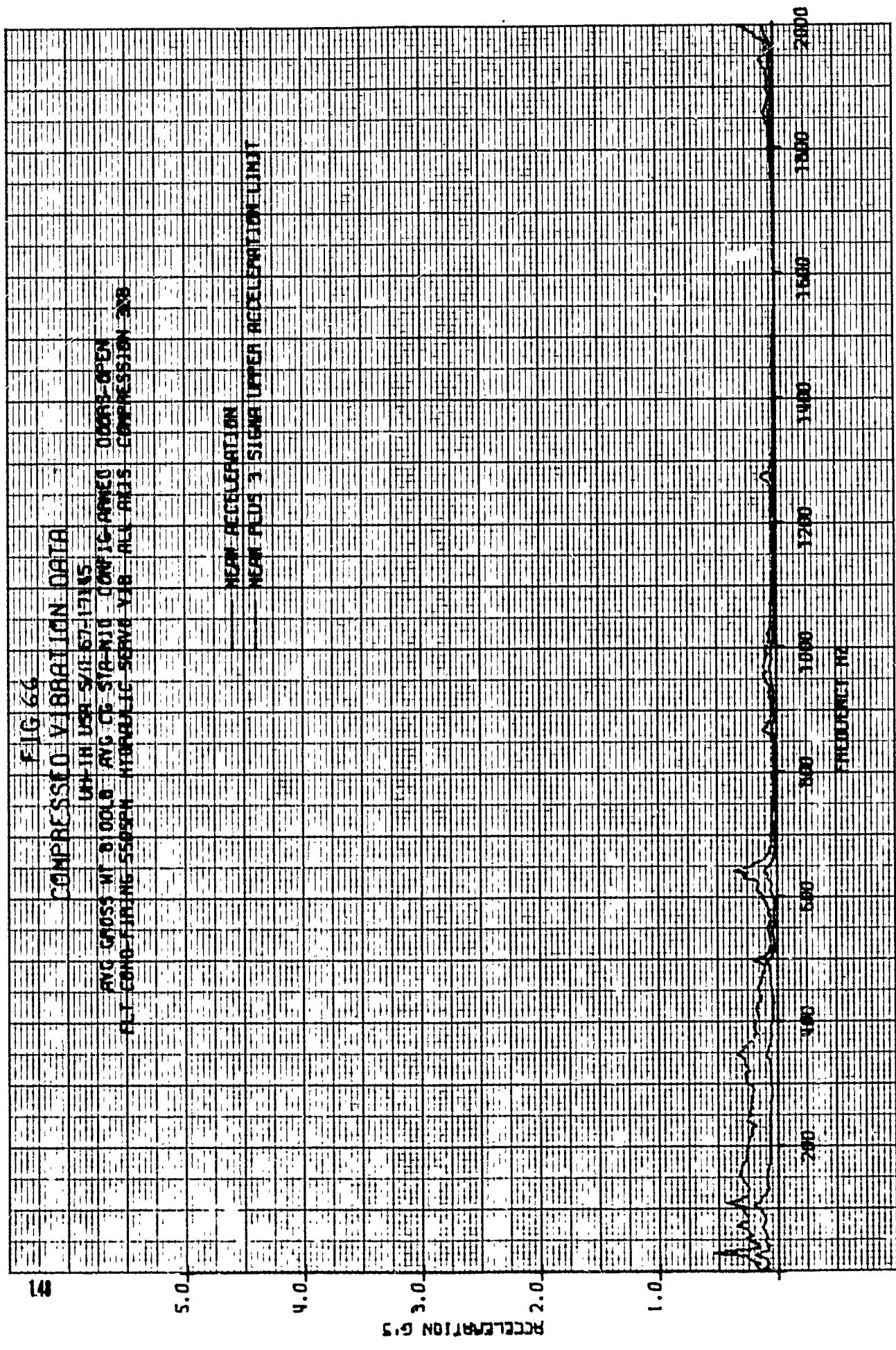


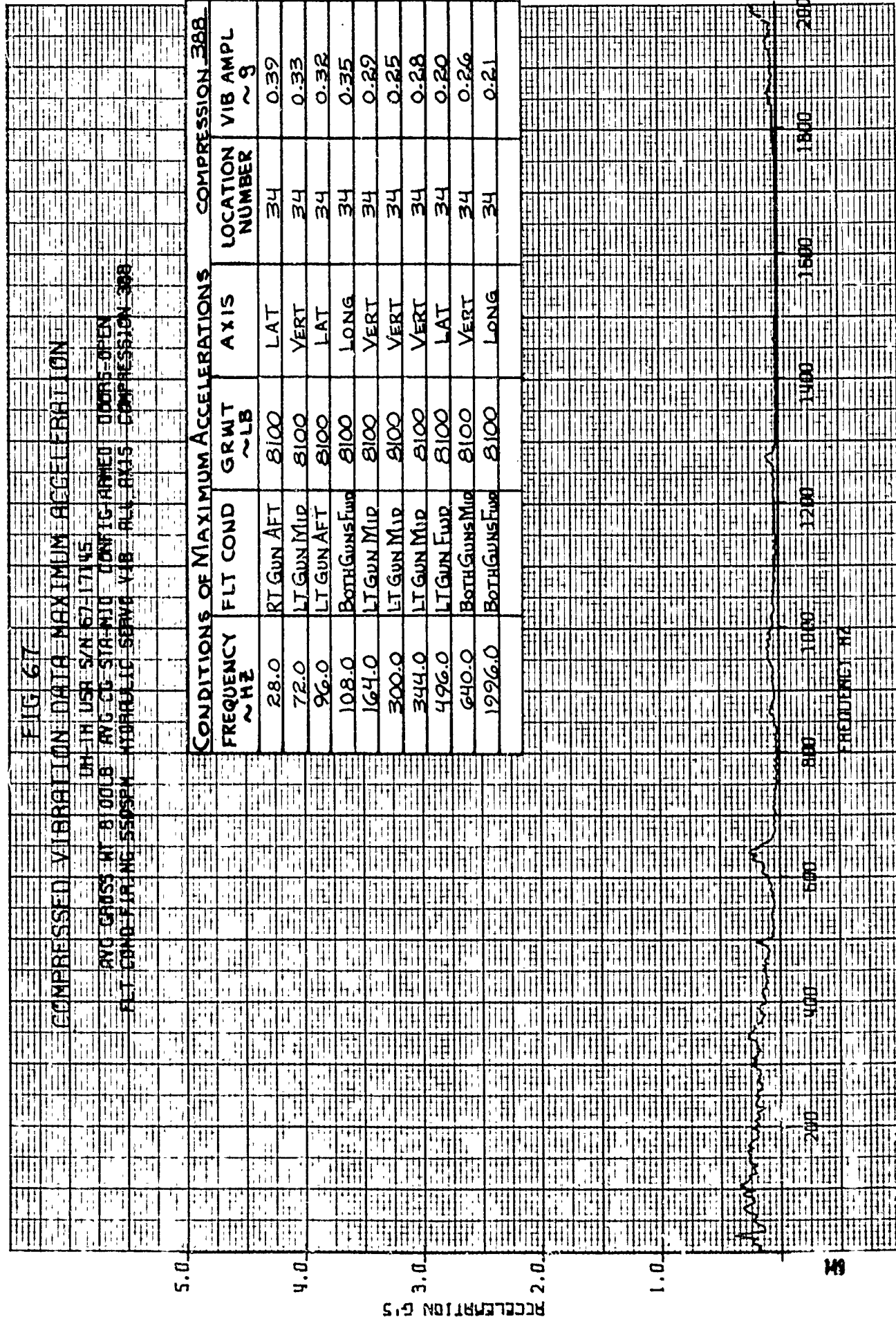
FIG 66

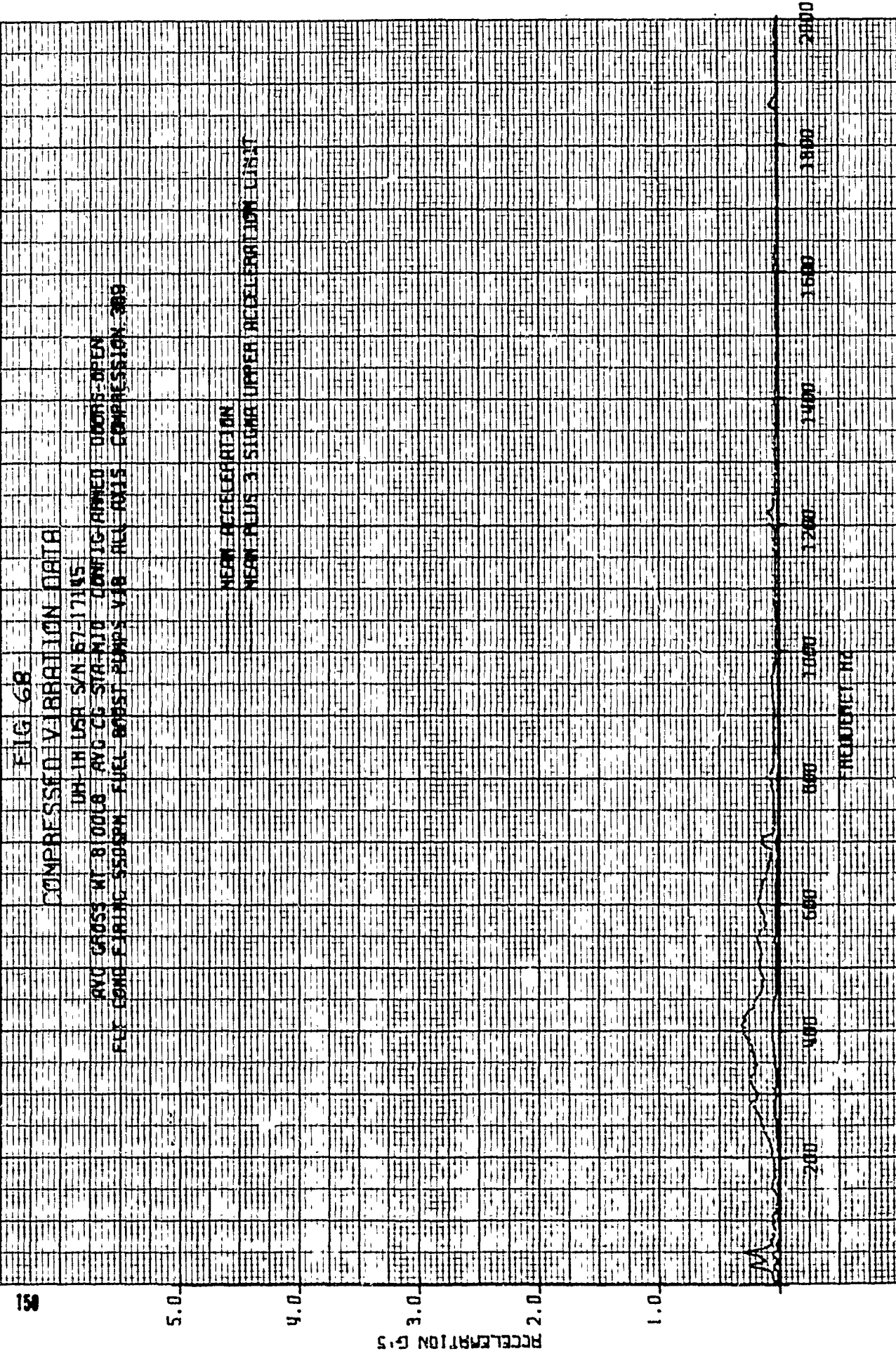
COMPRESSIO VIBRATION DATA

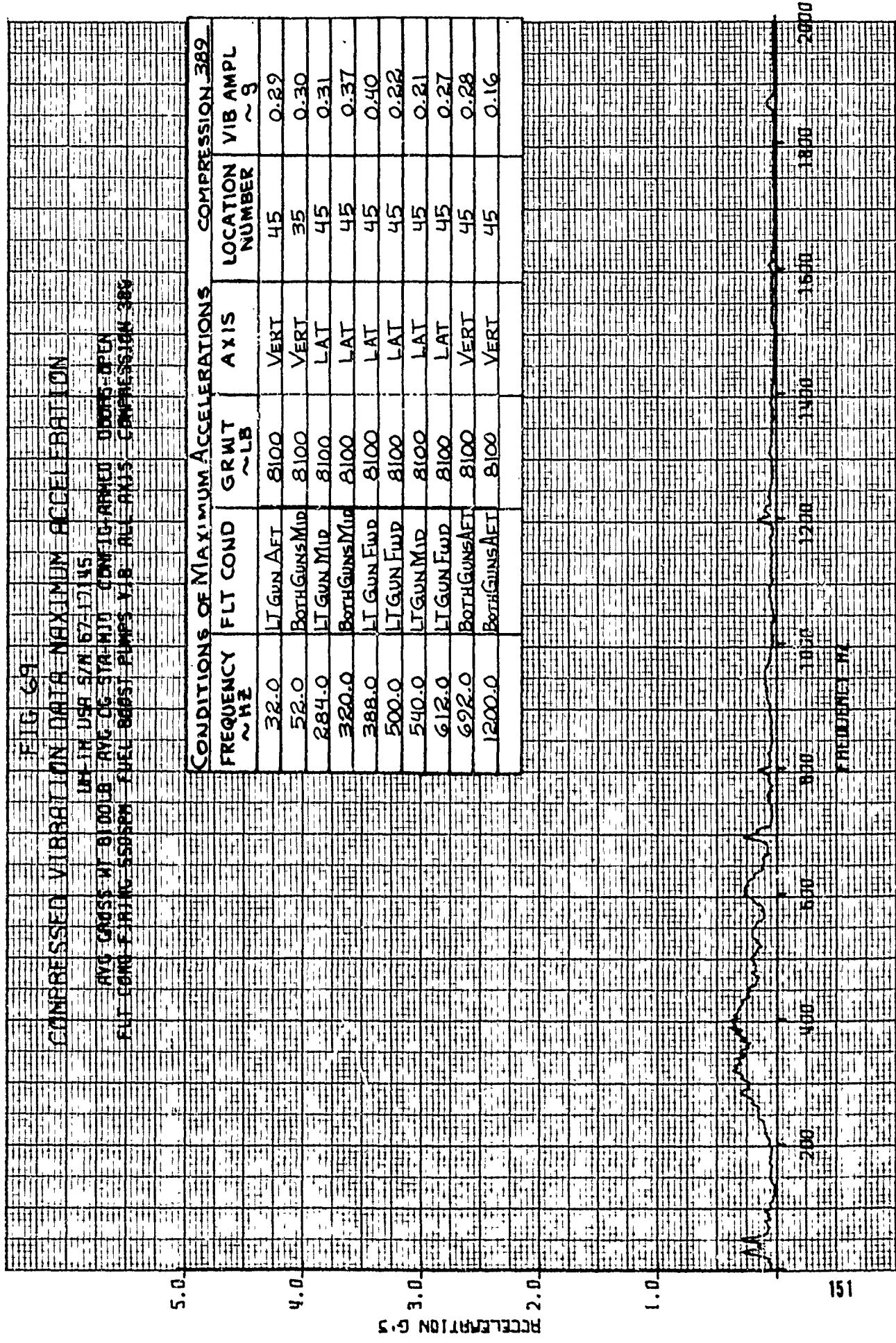
UH-1H UH-1H 5/11/67-17115
AVG GROSS WT 8100LB
AVG CG STA-N10
HYDRAULIC SERVO Y18 ALL RELS
COMPRESSION 2ND

MEAN RECELERATION
MEAN PLUS 3 SIGMA UPPER RECELERATION LIMIT









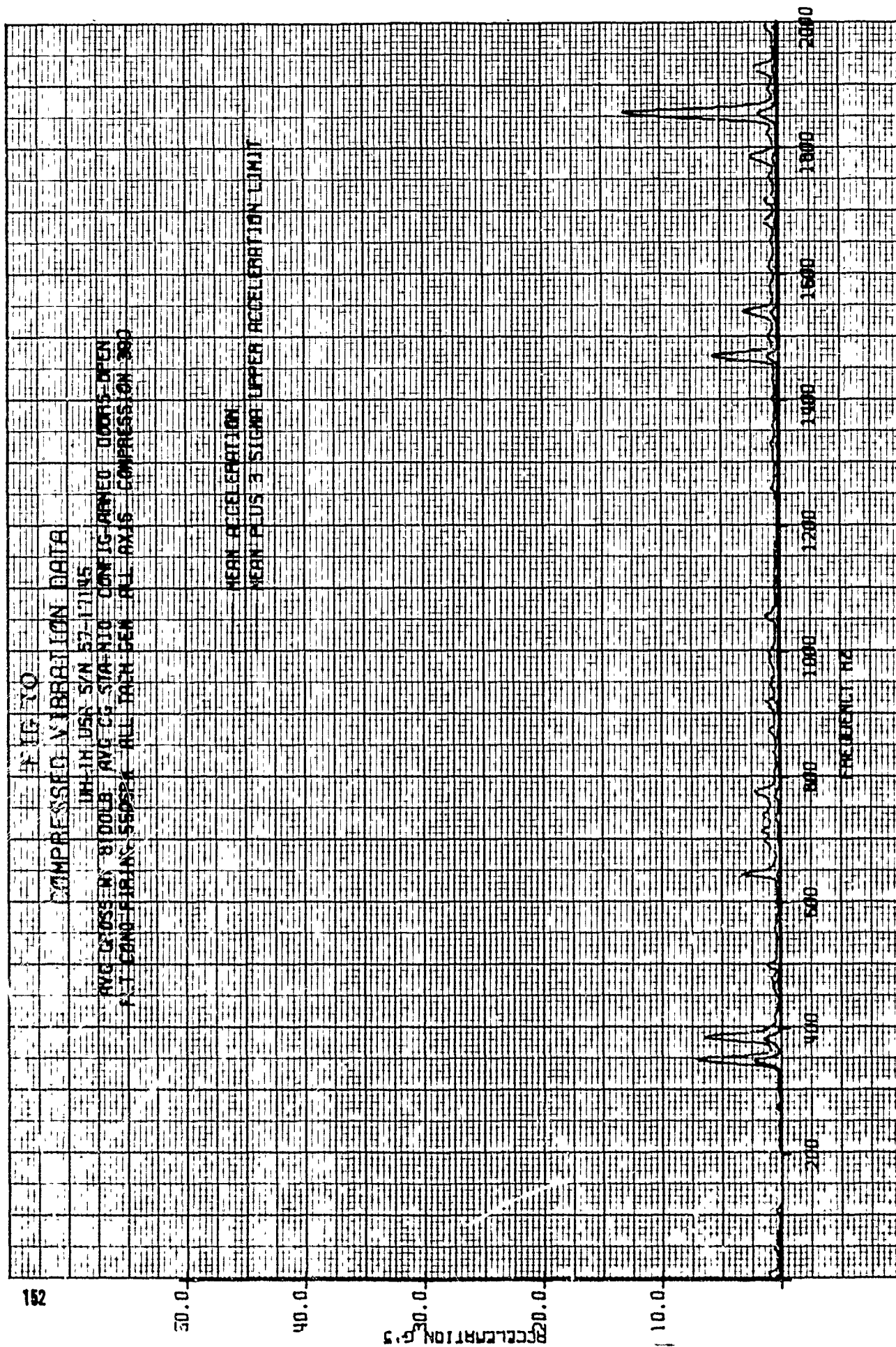


FIG. 71

UR-1H	USA	S/N 57-17145	CONFIG-ARMED	DOORS OPEN
AVG	CROSS	WT 8 00LB	AVG CG S/A-N10	ALL AXES
WT	CROSS	WT 5500LN	ALL FROM GEN	COMPRESS 30N 300

CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION
FREQUENCY ~ HZ	FLT COND	GRWT ~ LB	AXIS	LOCATION NUMBER	VIB AMPL ~ g
352.0	LT GUN FWR	8100	VERT	36	6.04
388.0	BOTH GUNS FWR	8100	VERT	38	5.86
644.0	BOTH GUNS MID	8100	LONG	38	6.90
696.0	BOTH GUNS MID	8100	LONG	38	3.05
712.0	BOTH GUNS MID	8100	LONG	38	3.21
776.0	BOTH GUNS FWR	8100	VERT	38	2.48
1468.0	BOTH GUNS MID	8100	VERT	38	5.16
1540.0	BOTH GUNS MID	8100	VERT	38	2.74
1784.0	RT GUN FWR	8100	LONG	37	2.40
1856.0	LT GUN MID	8100	LONG	37	13.14

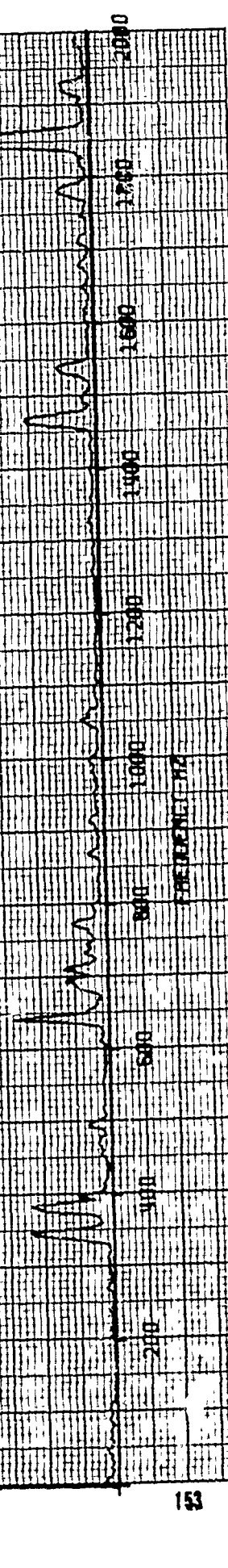


FIG 712 COMPRESSED VIBRATION DATA

AVG GROSS WT 8100LB AVG OG STA M10 CONFIG ARMED DOORS (PE)
FLT DEMO FLING 550SPM THE DET SHORT HER BRCS VIB ALL AXIS COMPRESS 8M 30

50.0

40.0

30.0

20.0

10.0

MEAN ACCELERATION
MEAN PLUS 3 SIGMA UPPER RECELERATION LIMIT

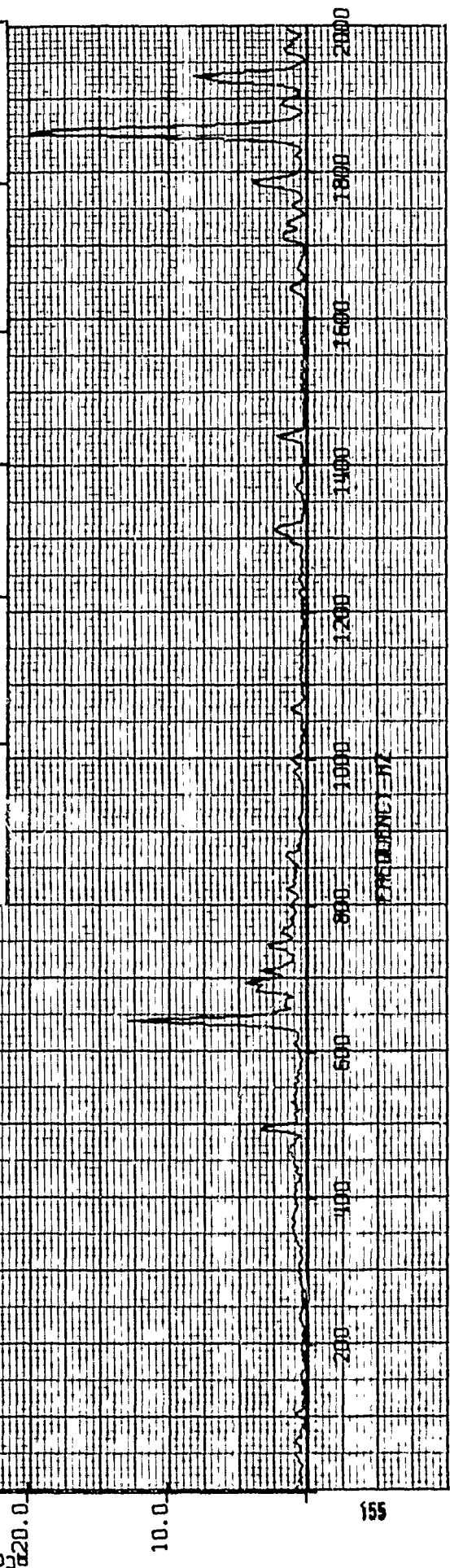
200 400 600 800 1000 1200 1400 1600 1800 2000

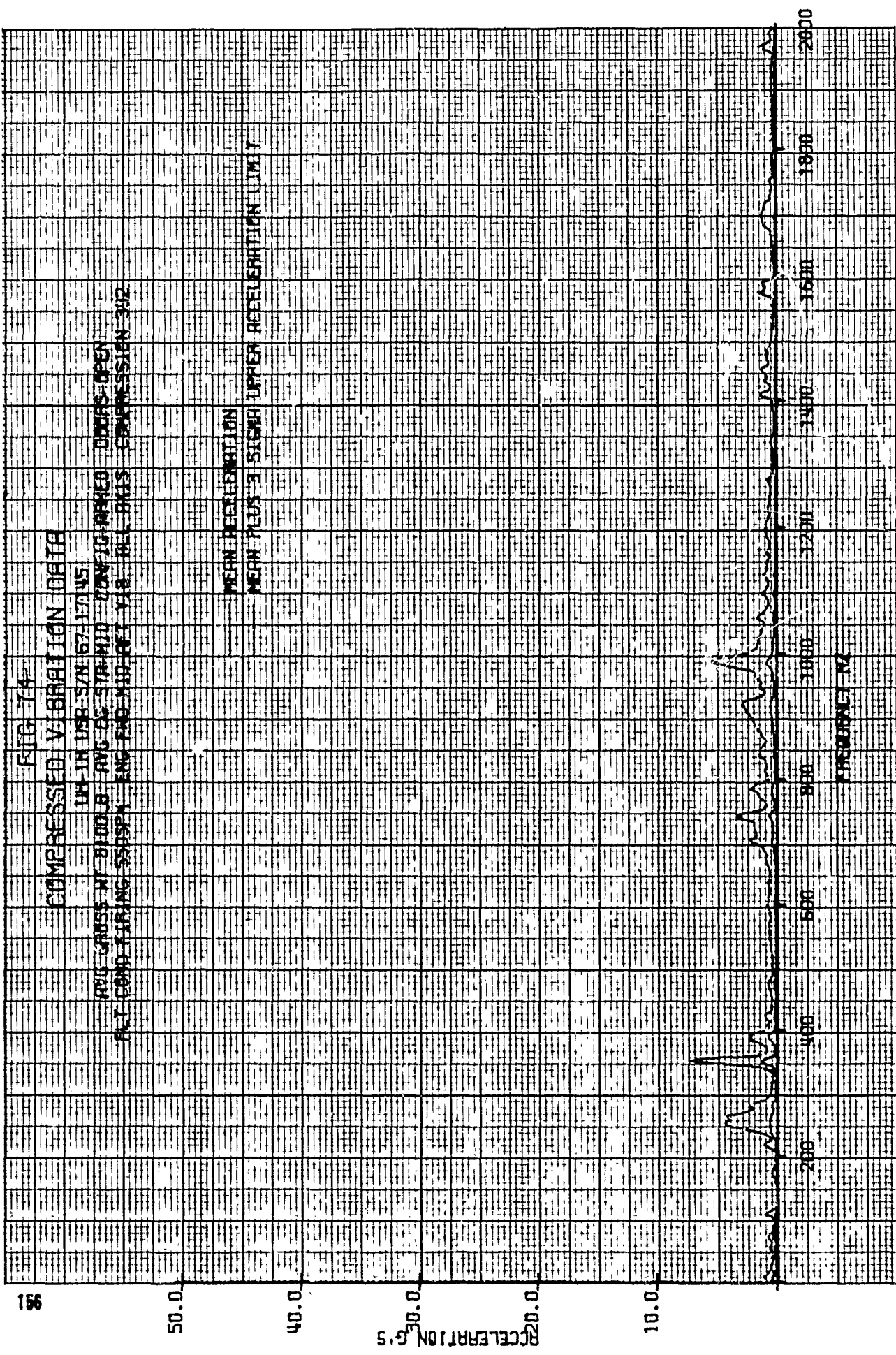
CONFIDENCE INT

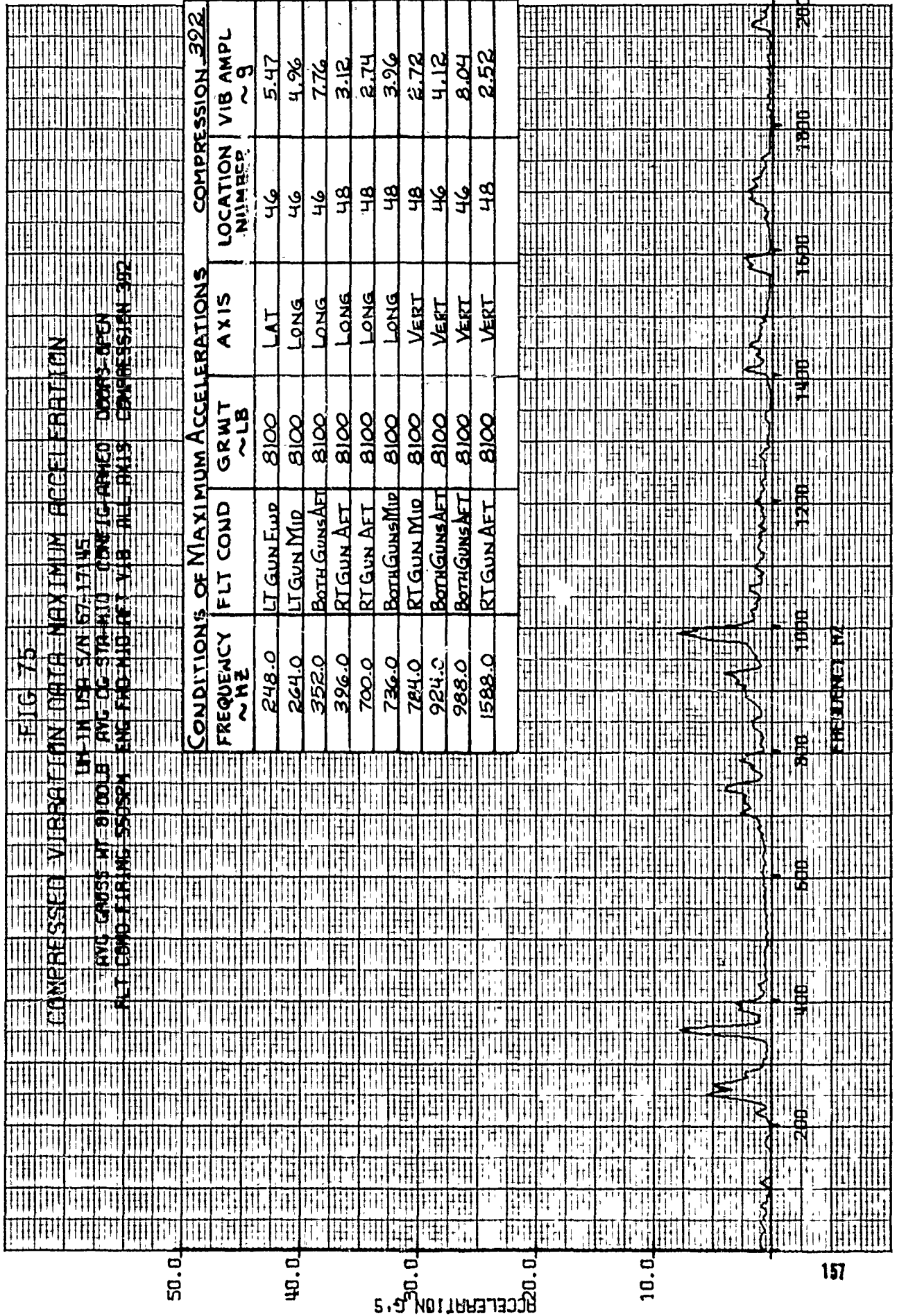


COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION
 UH-1H USA S/N 57-171N5
 AVG GROSS WT 8100LB
 AVG CG STA 410 CONFIG ARMED DOORS OPEN
 FLT COND FIRING SEQUENCE TAXI RPT SHORT PER BRCS VIB ALL AXIS COMPRESSION 391

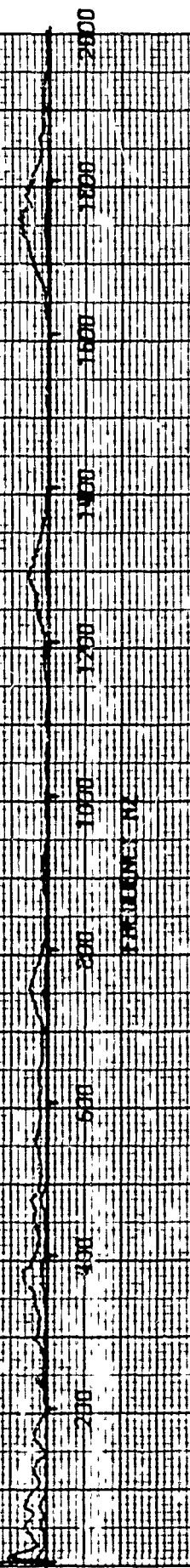
CONDITIONS OF MAXIMUM ACCELERATIONS					COMPRESSION 391
FREQUENCY ~HZ	FLT COND	GRWT ~LB	AXIS	LOCATION NUMBER	VIB A.P.D. ~g
496.0	RT GUN MID	8100	VERT	39	3.33
644.0	RT GUN MID	8100	VERT	39	12.69
696.0	RT GUN MID	8100	VERT	39	4.43
712.0	RT GUN MID	8100	VERT	39	3.35
748.0	RT GUN MID	8100	VERT	39	2.66
1312.0	BOTH GUNS AFT	8100	VERT	40	2.21
1440.0	RT GUN AFT	8100	VERT	41	2.10
1788.0	RT GUN AFT	8100	VERT	40	3.92
1852.0	BOTH GUNS FWD	8100	VERT	39	19.90
1932.0	RT GUN MID	8100	VERT	42	8.13

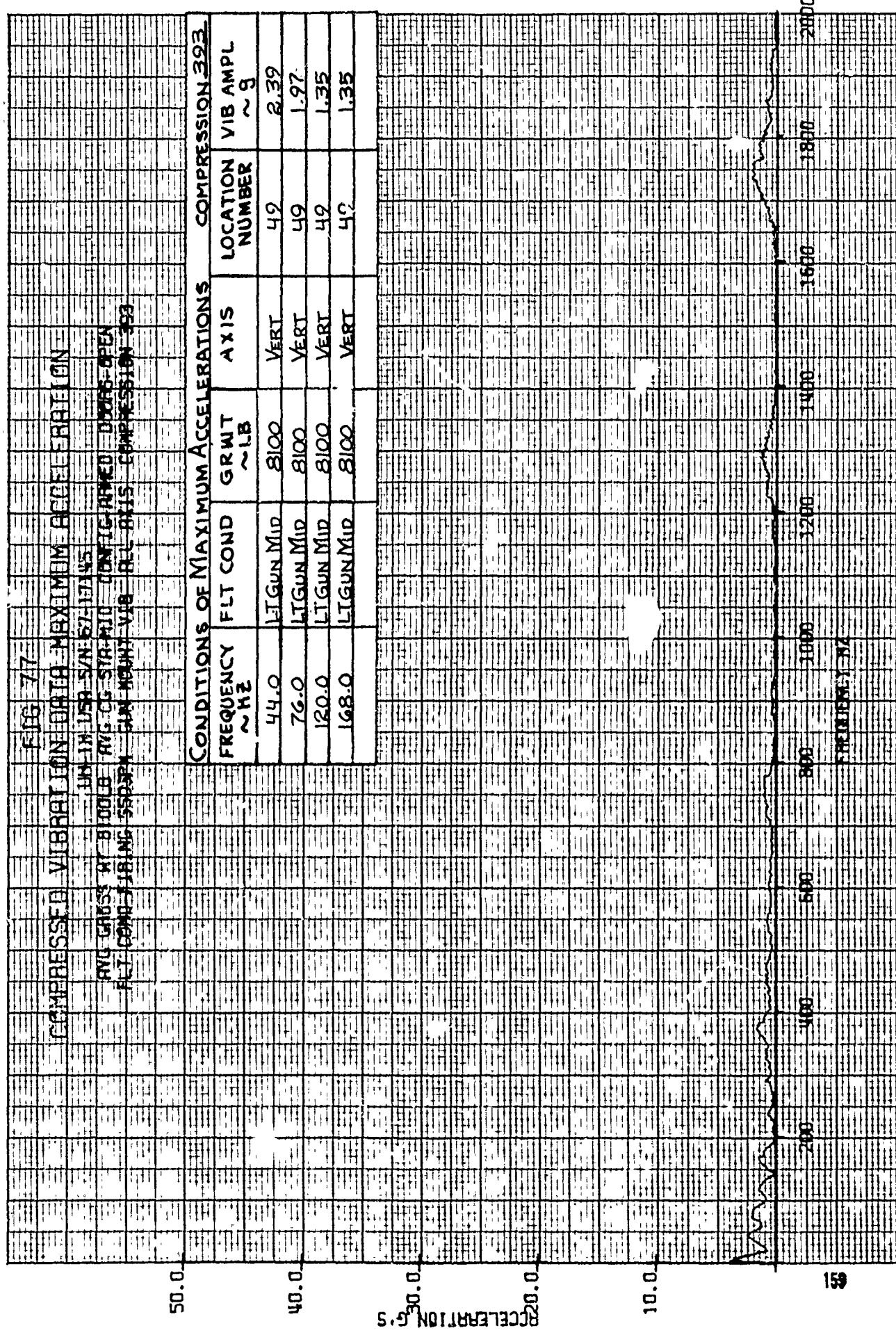






MEAN PLUS 3 SIGMA UPPER RECESSIONS IN 1





160

ACCELERATION G'S

5.0

4.0

3.0

2.0

1.0

FIG 78

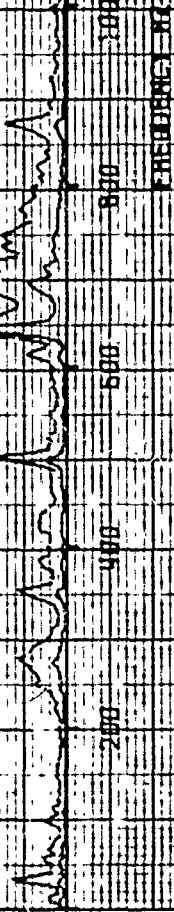
COMPRESSED VIBRATION DATA

UT-1H USA S/N 67-17145

AVG GROSS WT 8.00LB AVG CG STA-M10 COMP LG-ARMED -ODDS-OPEN
CLT 5000 FILING 5505M CLT LINK-V18 ALL AXIS COMPRESSION 401

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT



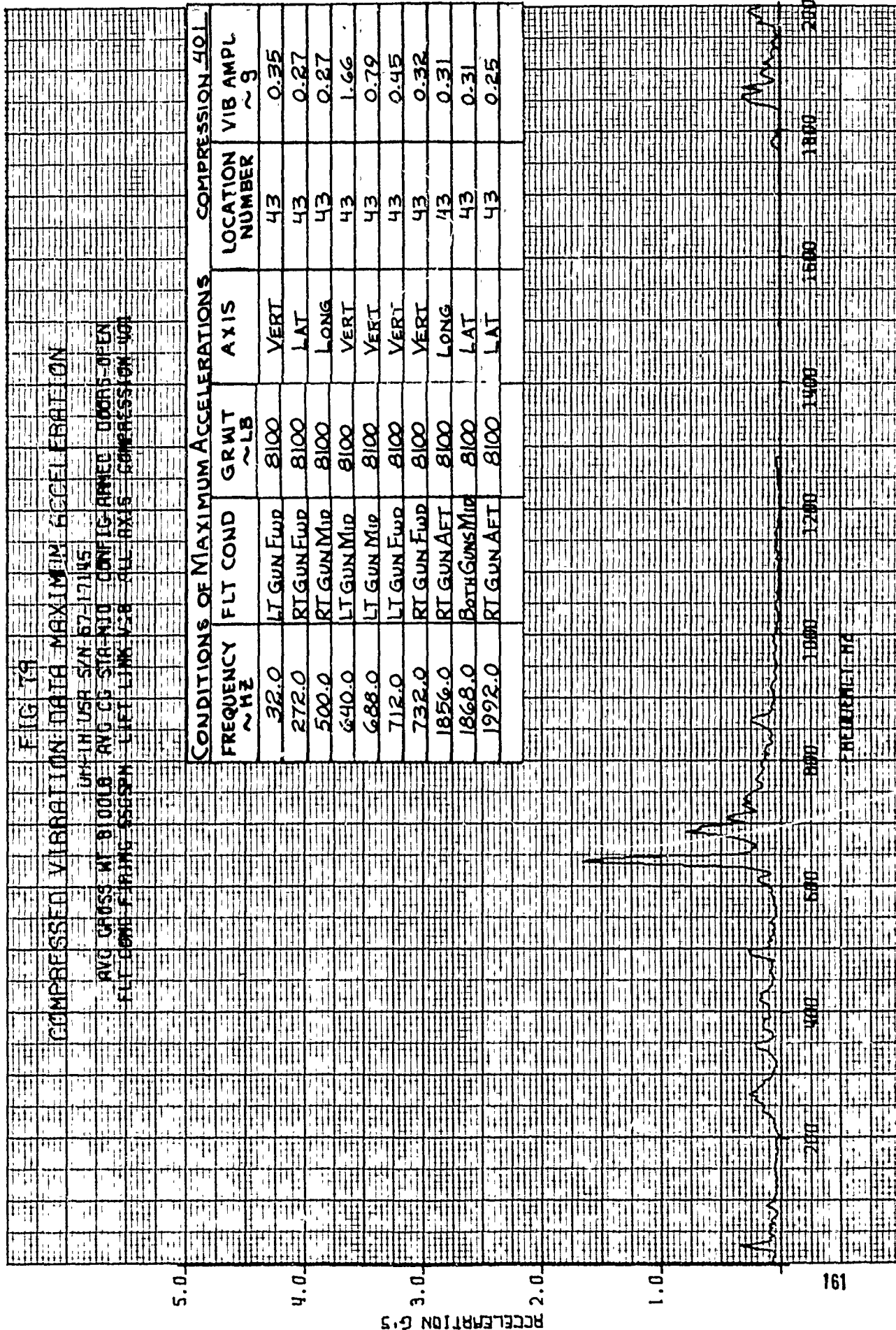
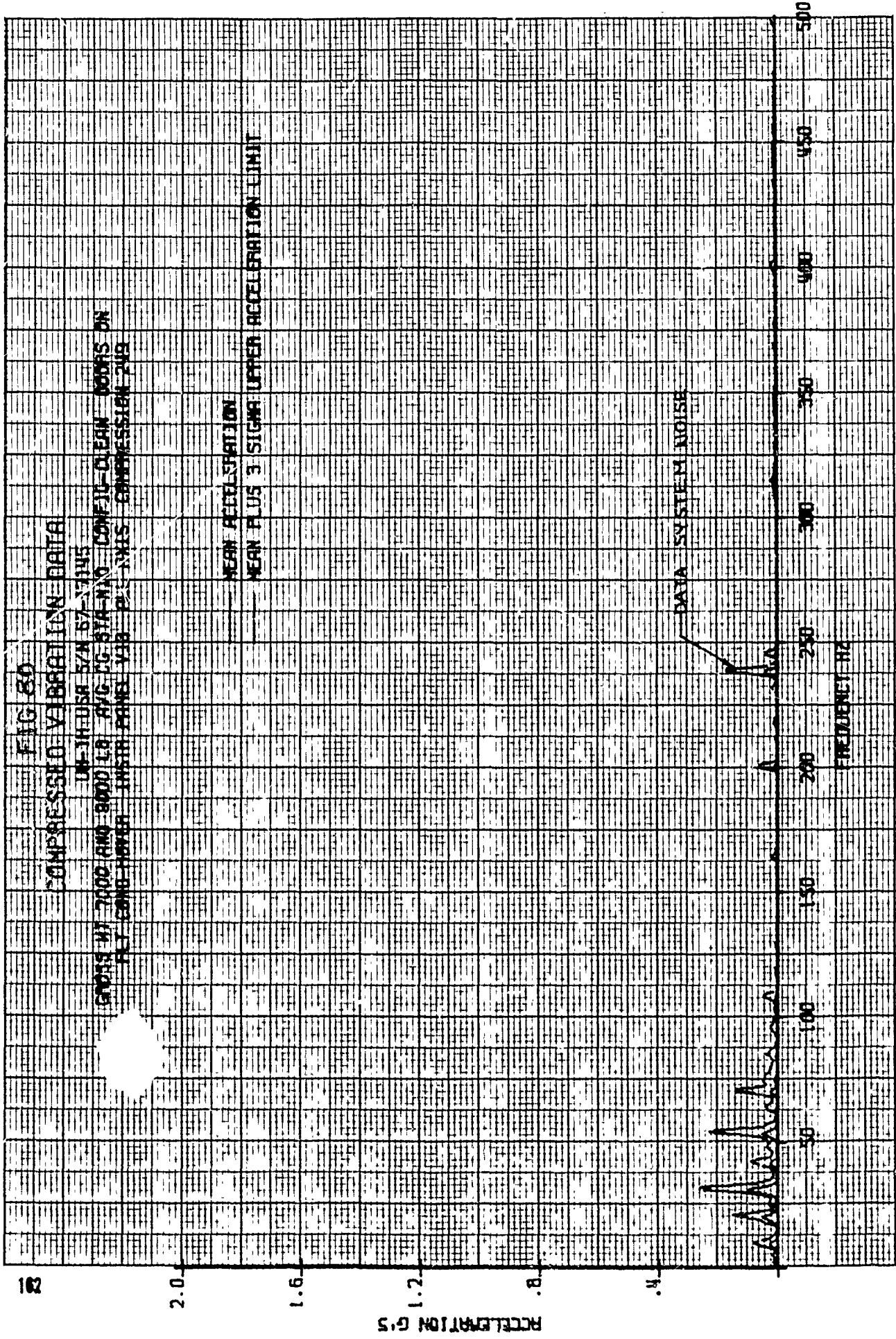


FIG 80

COMPRESSED VIBRATION DATA

UR-1H USA 52A 67-141US
 GROSS WT 7000 AMO 8000 LB AVG TC 87A-M10 CONFID-CLEAN BOMBS ON
 PET COND-HWY88 INSTR PANEL V38 2X-1X15S COMPRESSION P19



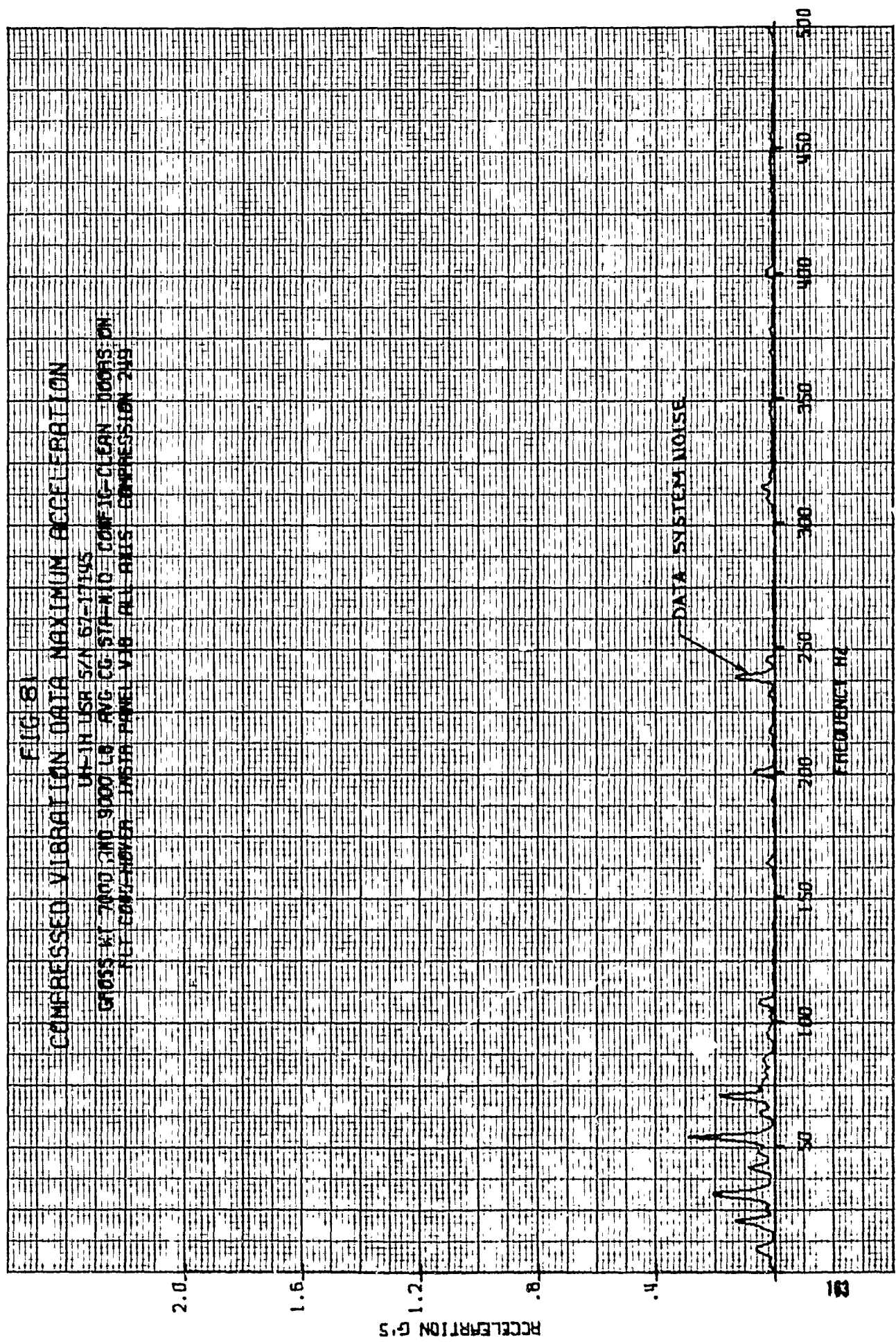


FIG 82

COMPRESSED VIBRATION DATA

UH IN USA S/N 67-17145
GROSS WT 7000 LBS AVG CG STA-N10 COMB-CLEAN DOORS-IN
CG COMB-LEVEL FET ENSTH PANEL VIB REL RMS COMPRESSION 250

MEAN ACCELERATION
MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE

FREQUENCY HZ

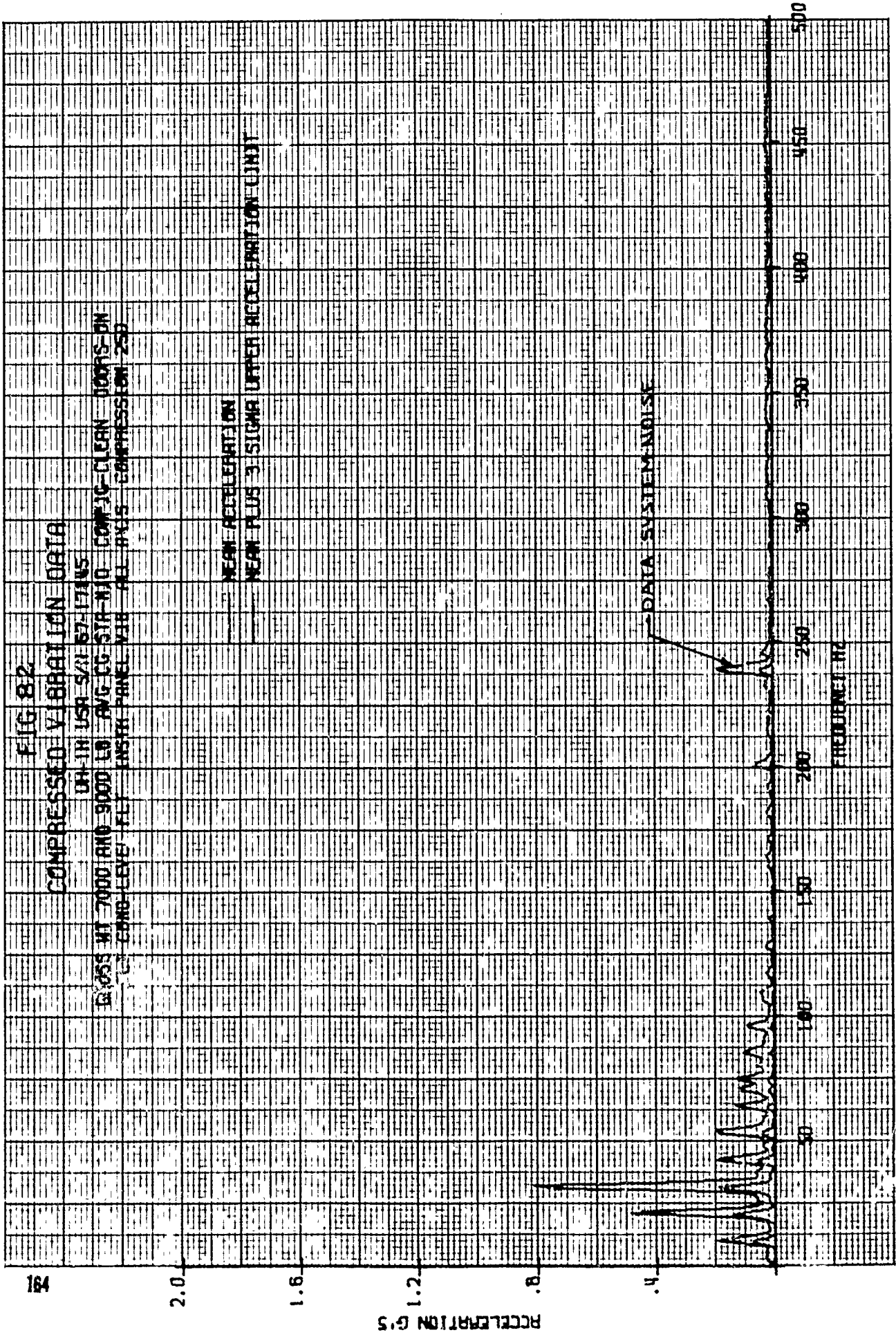


FIG 8.5

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UH-1H UH-1H S/N 57-17145
 GROSS WT 2400 LBS AVG CG STA-M10 CONF:IG-CLEAN DOORS-ON
 FLT COND-LEVEL FLT INSTR: PANEL VIB ALL AXES COMPRESSION 250

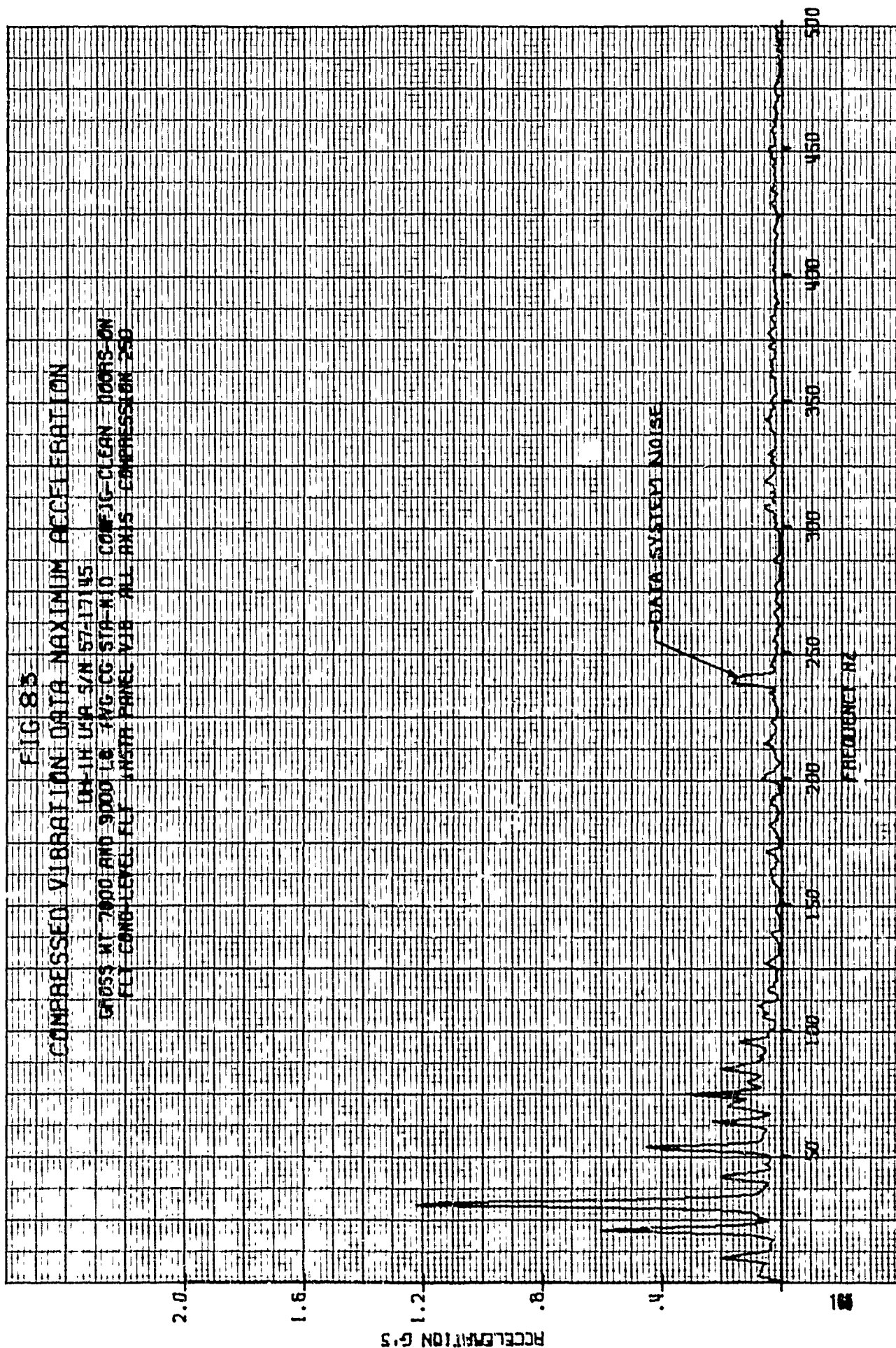


FIG 84-

COMPRESSION VIBRATION DATA

LINE 11-058 8/24 67-3/115
GROSS WT 2000 LBS 8000 LB AVG CG 314 INCH COMFIO-CLEAN 00015-DW
FLT COMB-CLIMB INSTR PANEL VIB ALL POS COMPRESSION 251

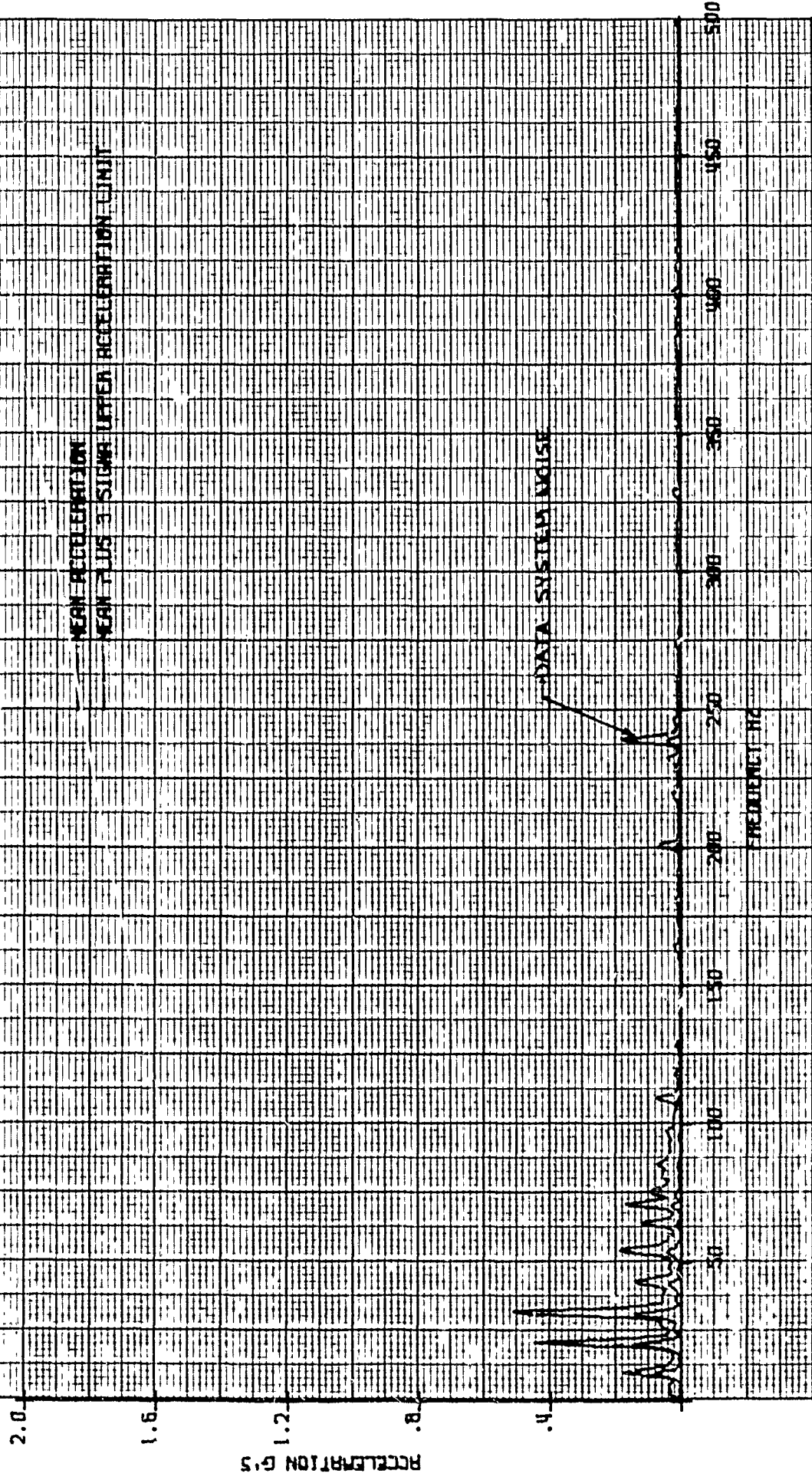


FIG 8'S

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UH-1H-LISA S/N 67-13145
GROSS WT 7000 AND 9000 LB AVG CG STA M10 COME-IC-CLEAN DOORS ON
ACT COMB-CLIMB INSTR PANEL VIB REL AXES COMPRESSION 251

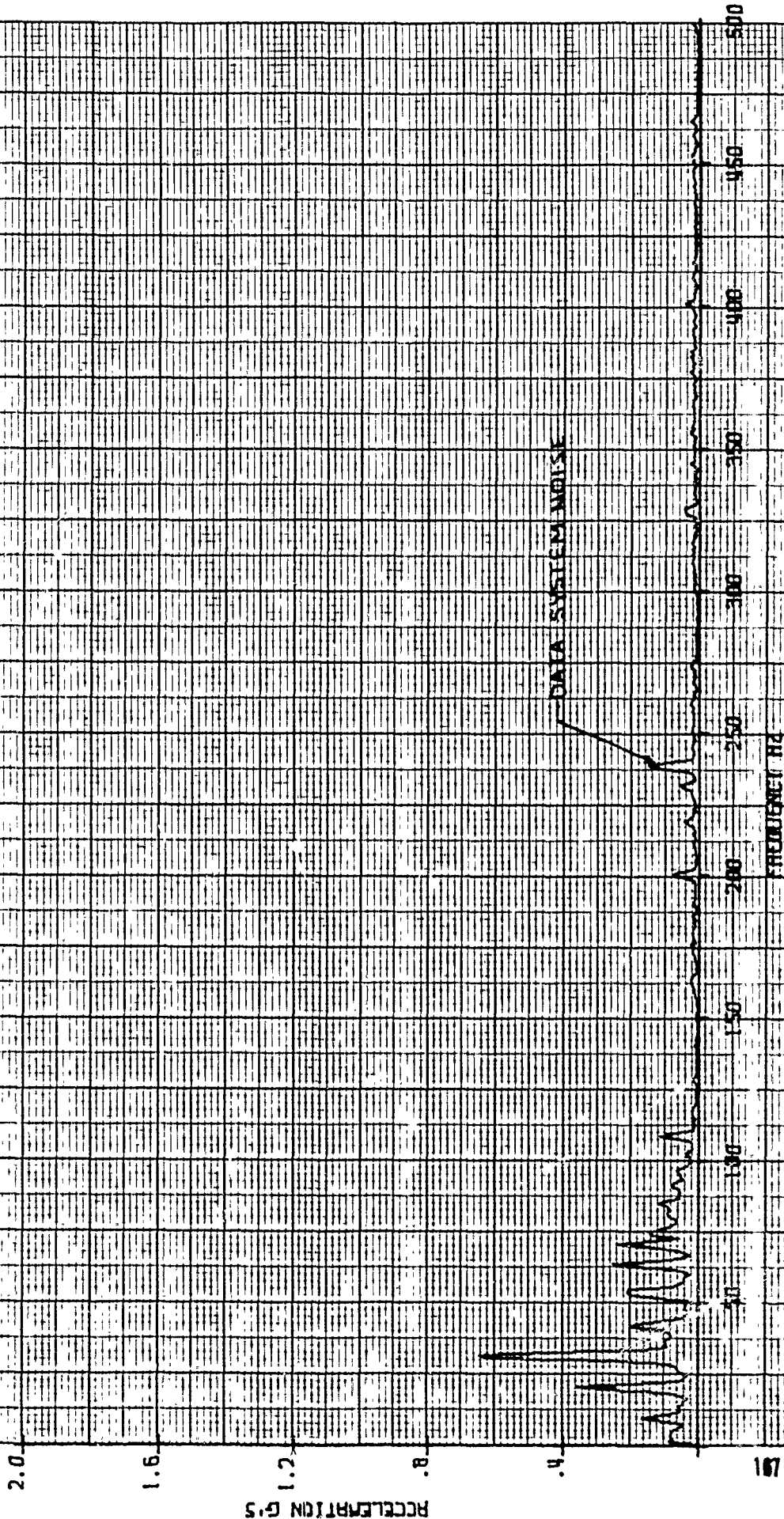
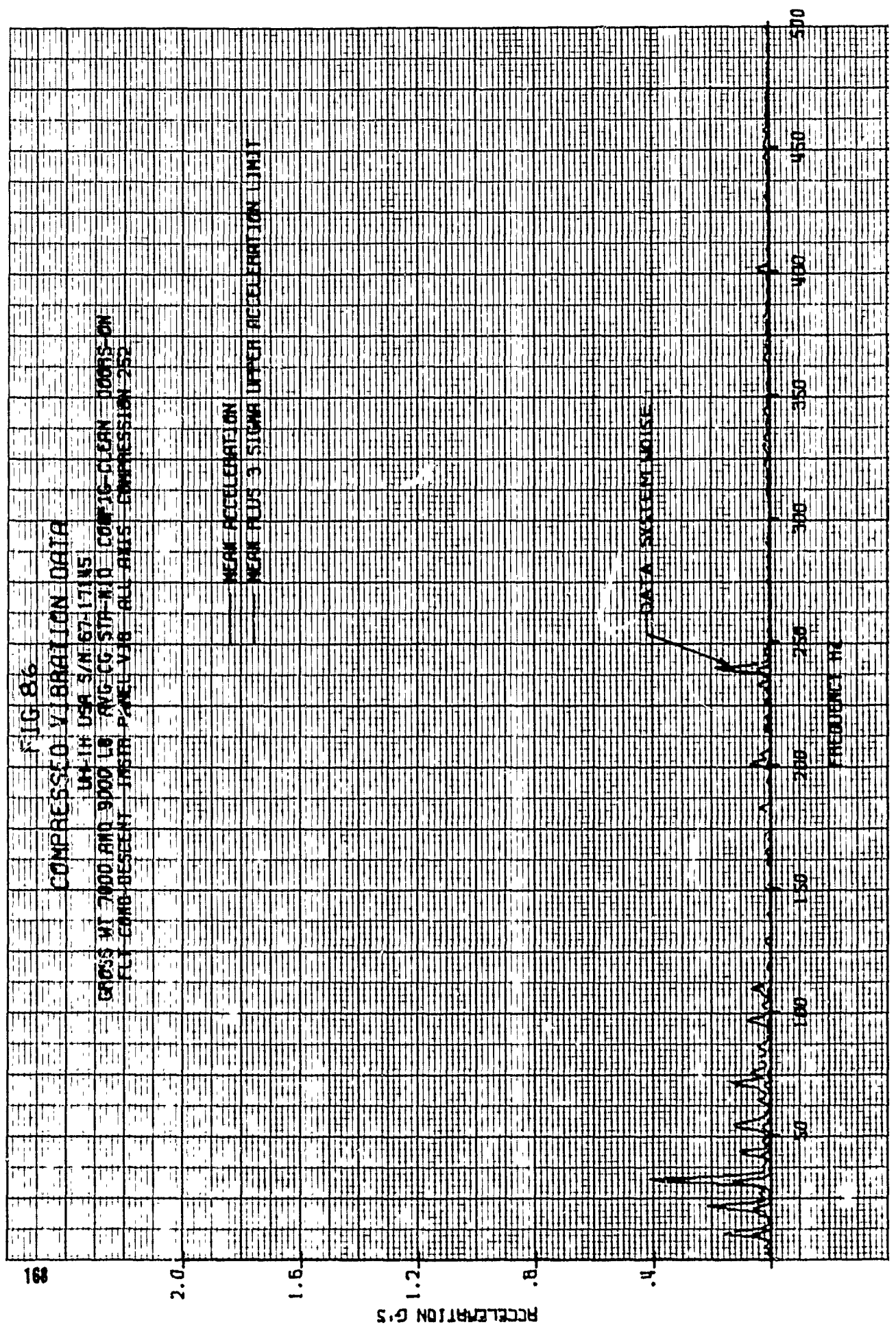


FIG 86

COMPRESSOR VIBRATION DATA

GROSS WT 7000 LBS AVG CG STA-M10 COMP 16-CLEAN DOORS-ON
FLY-COMB-DESCENT INSTR PANEL VIB ALL AXES COMPRESSION 252
UN-IN USA S/N 67-17115

MEAN ACCELERATION
MEAN RMS 3 SIGMA UPPER ACCELERATION LIMIT



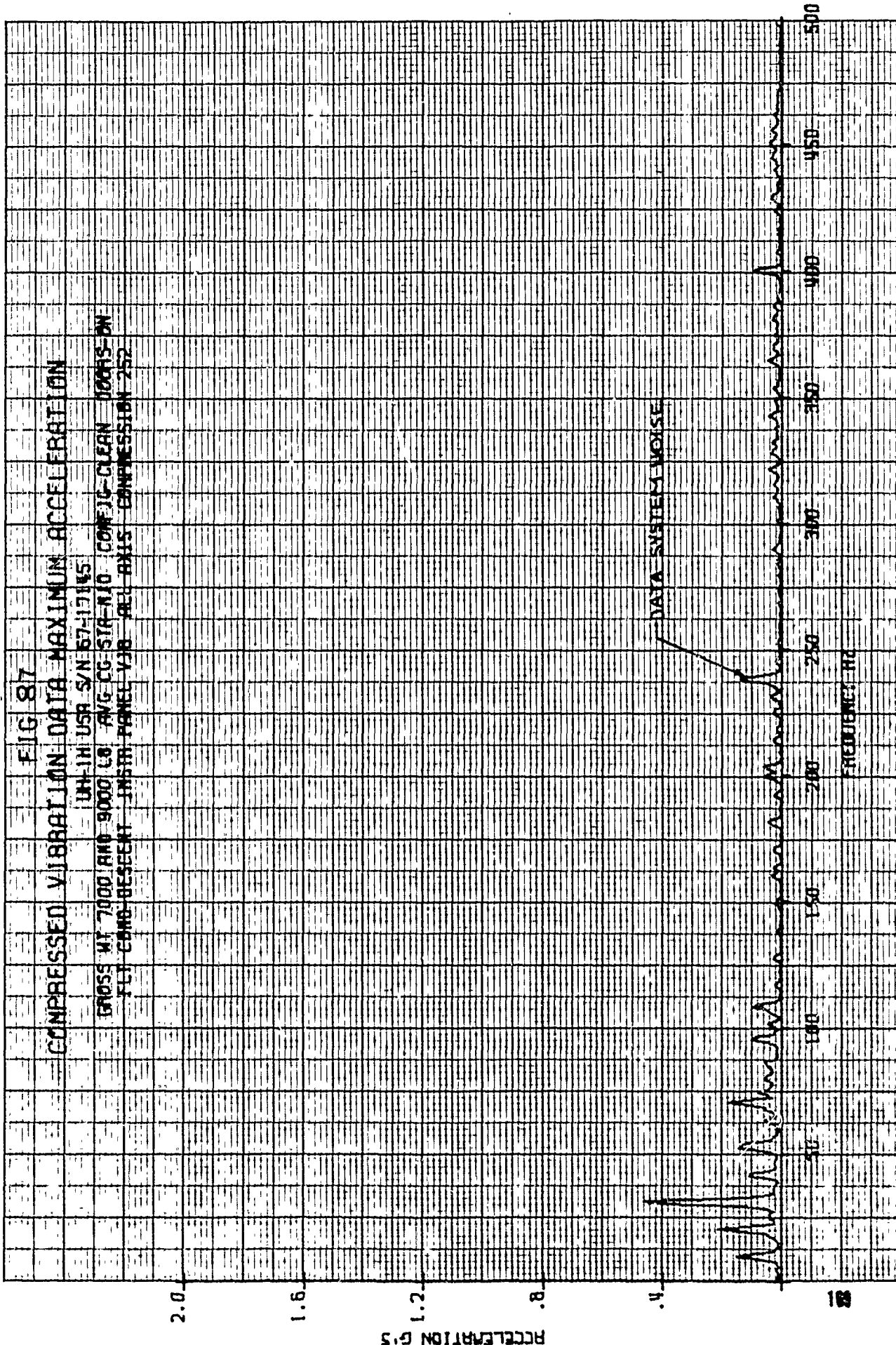


FIG 88

COMPRESSED VIBRATION DATA

CROSS AT 7000 RPM 9000/28 AVG CG STA N10 CONFIO-CLEAN TOURS ON
H11 SOME 720 RPM LOW INSTR PANEL VIB ALL AXIS COMPRESSION 253

UNIT: USA SYN 57-17145

MEAN ACCELERATION
MEAN PLUS 3 SIGMA UPPER RECELERATION LIMIT

ACCELERATION G'S

FREQUENCY HZ

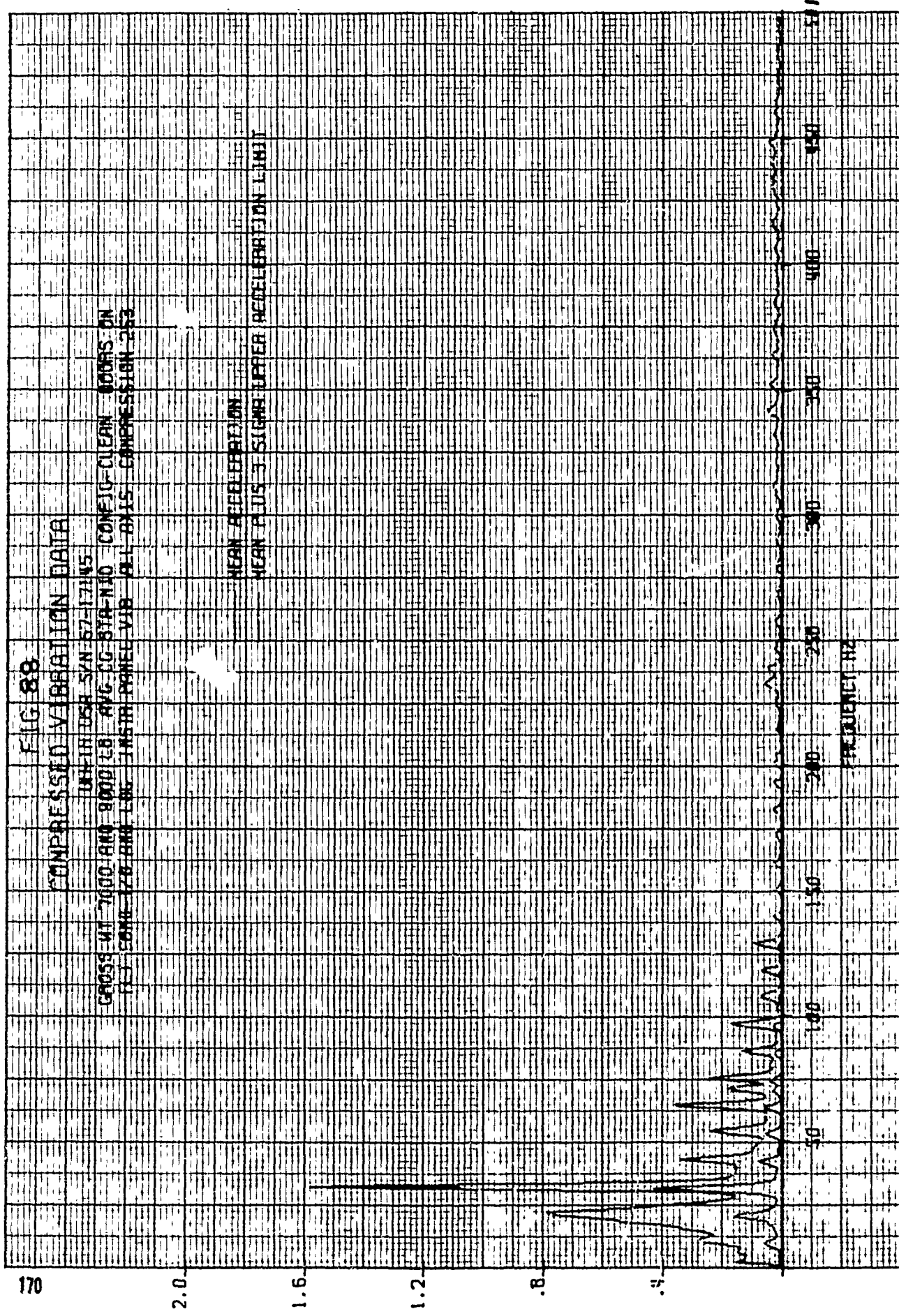
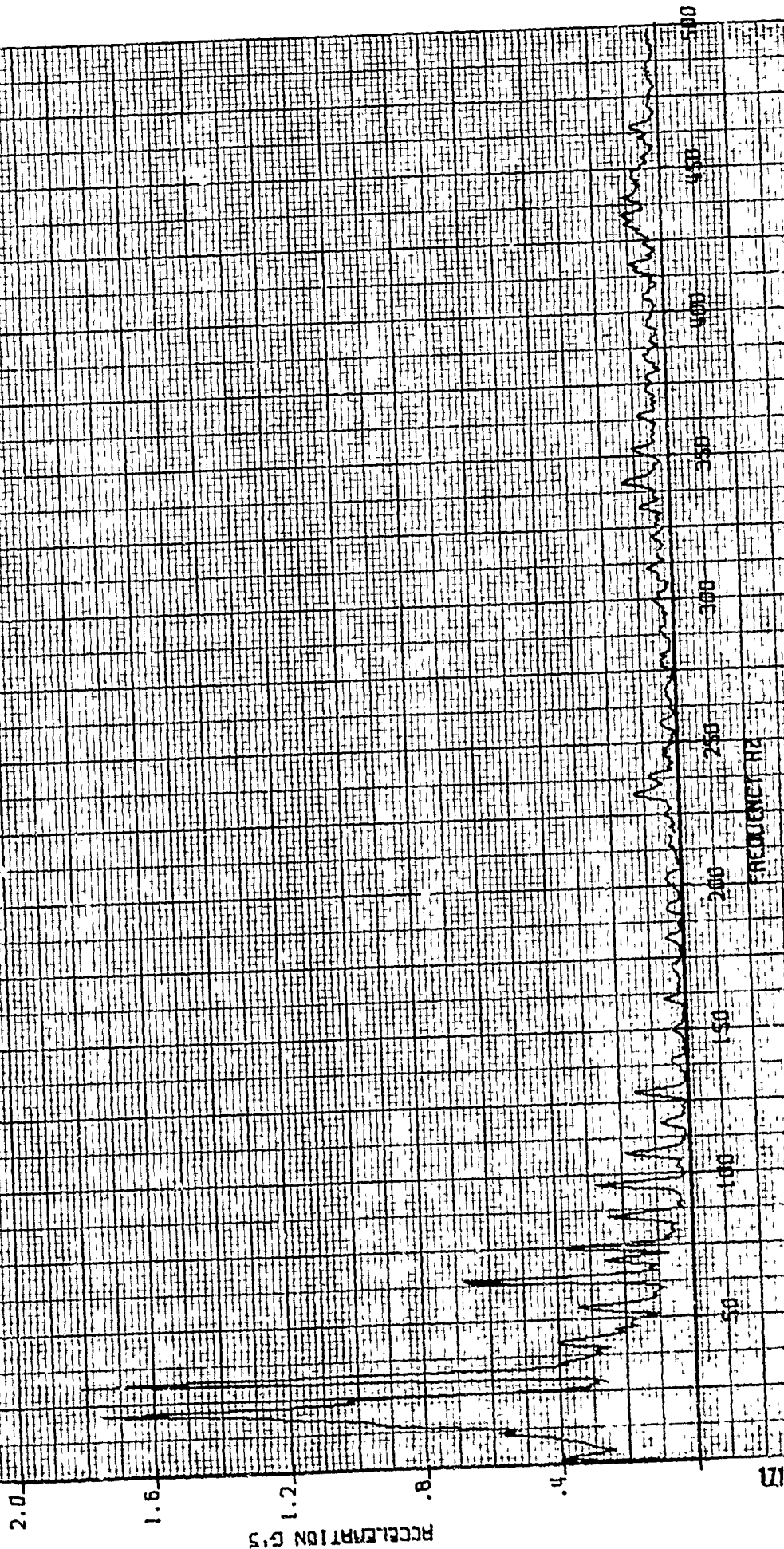
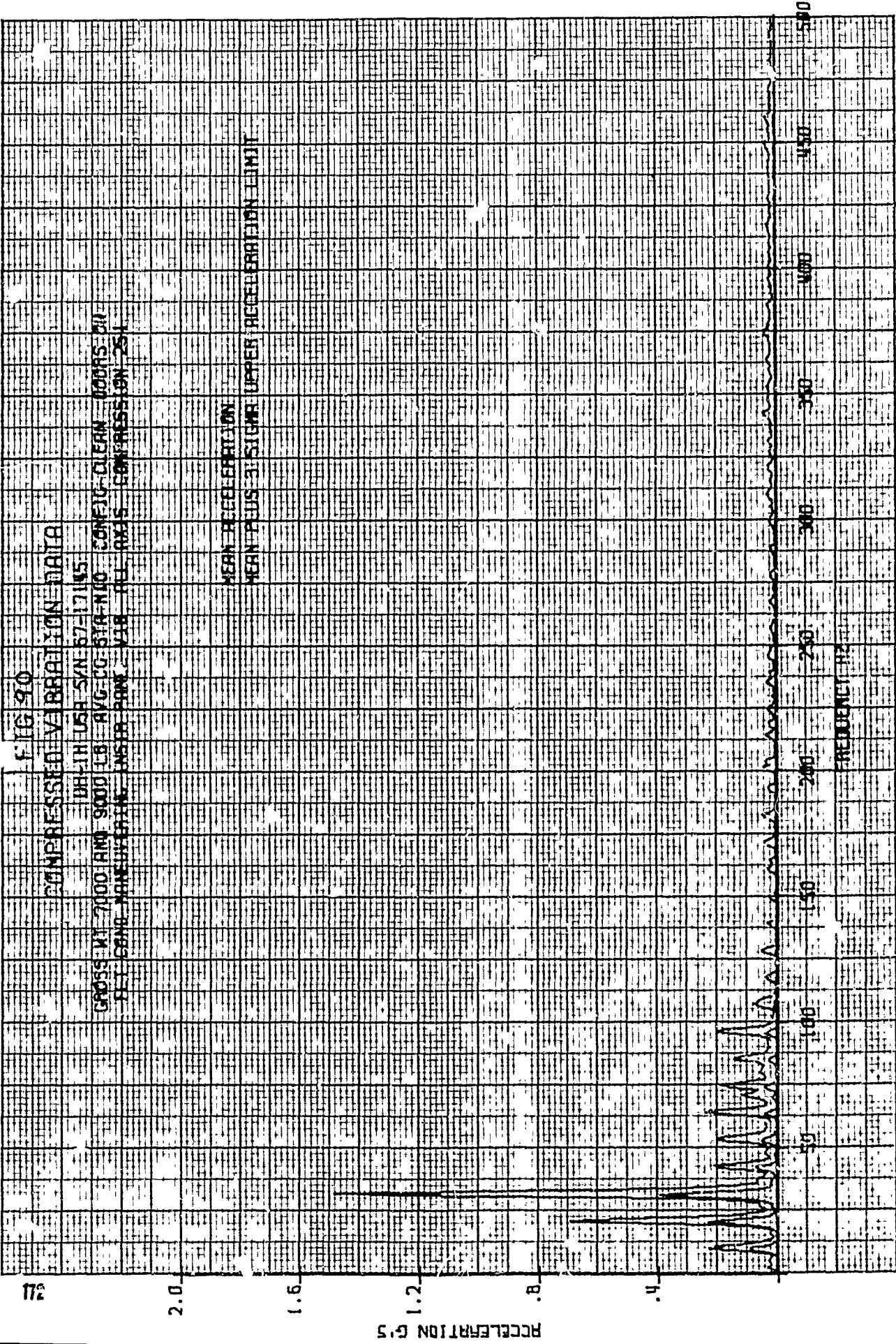


FIG 89

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

DATA DSR SYN 87-131115
 GROSS WT 2000 LBS AVG CG STA N10 CONFID-CLEAN DOORS ON
 FLT COND 1/20 RAN LOG 14578 PANEL VIB ALL AXES EXHIBITION 253





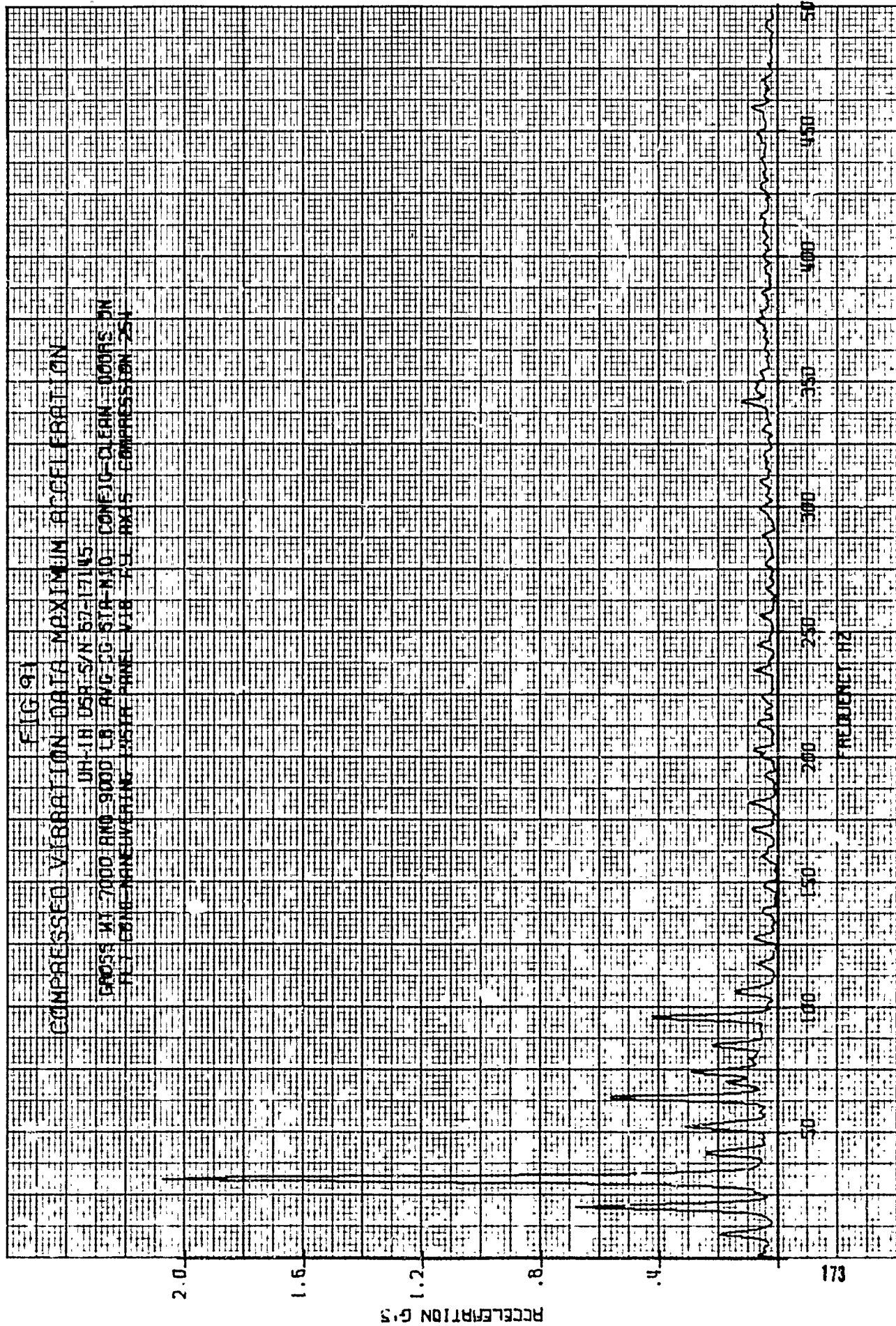


FIG 92

COMPRESSED VIBRATION DATA

IN IN-USE 5A 62-13105

GROSS WT 7000 LBS AVG CG STR 410 COMFLO CLEAN UNDRS ON
AND TEST CONT GND/LET TALE INSTR PANEL VIB REL AXES COMPRESSION 255

2.0

1.6

1.2

.8

.4

ACCELERATION G'S

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER RECELERATION LIMIT

50

100

150

200

250

300

350

400

450

500

FREQUENCY HZ

1.0
 0.8
 0.6
 0.4
 0.2
 0.0

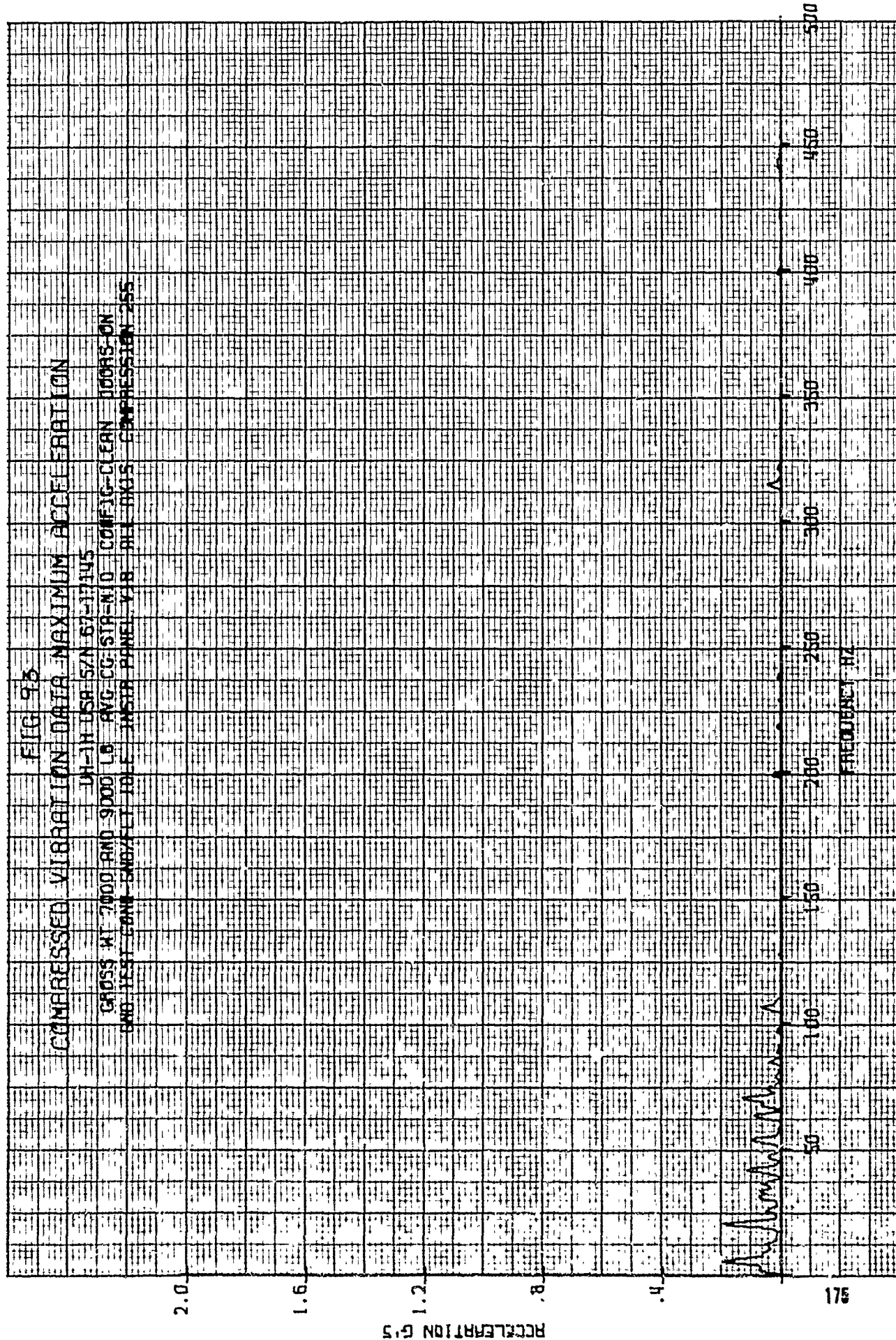


FIG 94

COMPRESSED VIBRATION DATA

02-1A USA-5/N 67-171N5
 GROSS WT 2000 LBS AVG CG 51A-MID CONFIG-CLEAN 1000RS-ON
 FLT CONE-HOVER RV JONES-CONVARIANT V38 TAIL AXIS COMPRESSION 256

2.0

1.6

1.2

.8

.4

ACCELERATION G'S

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER RECELERATION LIMIT

DATA SYSTEM NOISE

FREQUENCY Hz

100

150

200

300

400

500

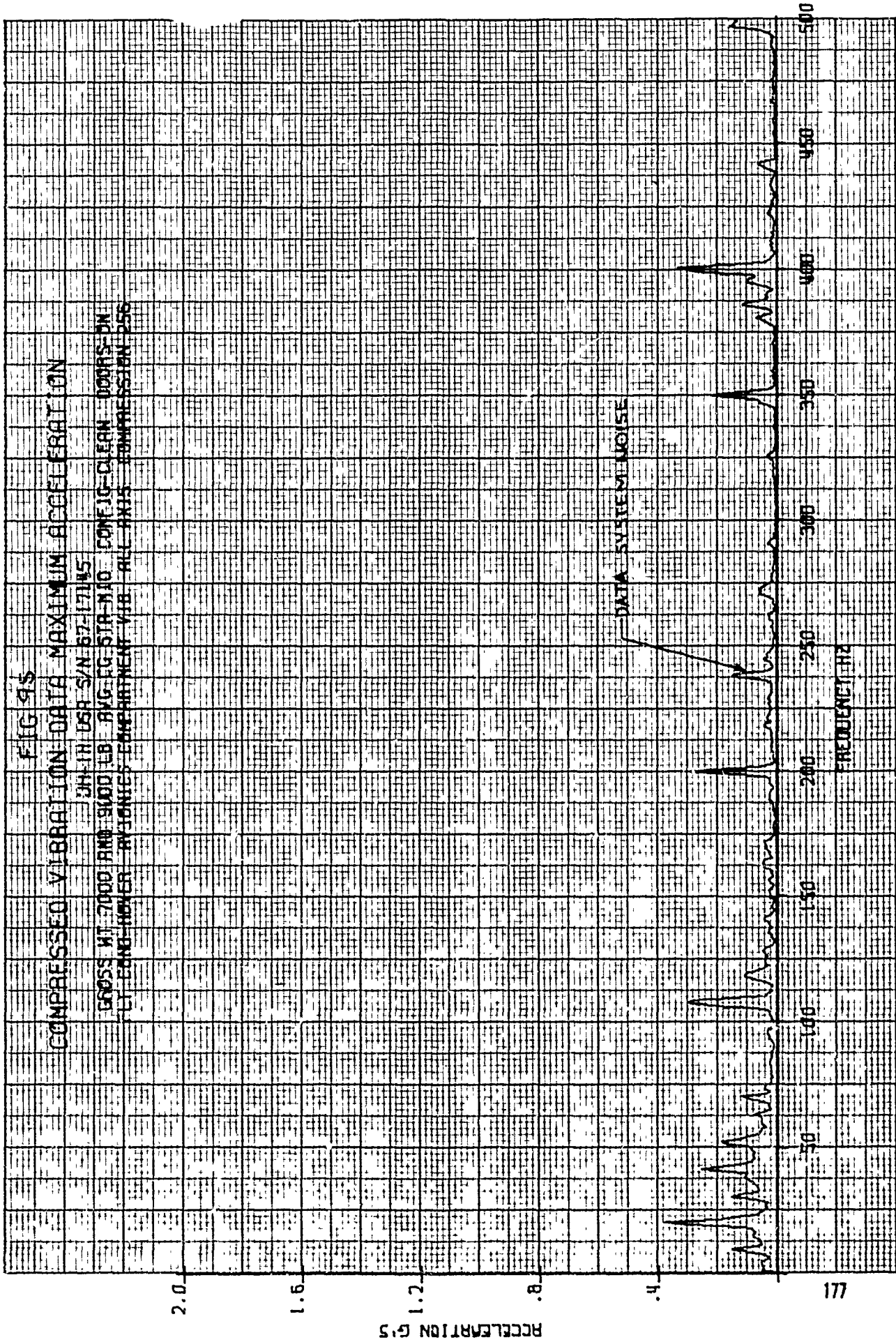


FIG 96 COMPRESSED VIBRATION DATA

UH-1H USA S/N 67-17145
GROSS WT 7000 PWD 9000 LB AVG CG STA-410 CONF IG-CLEAN DOORS ON
RET CONG LEVEL FLT AVIONICS COMPARTMENT VIB ALL AXES COMPRESSION 257

2.0

1.6

1.2

.8

.4

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE

50

100

150

200

250

300

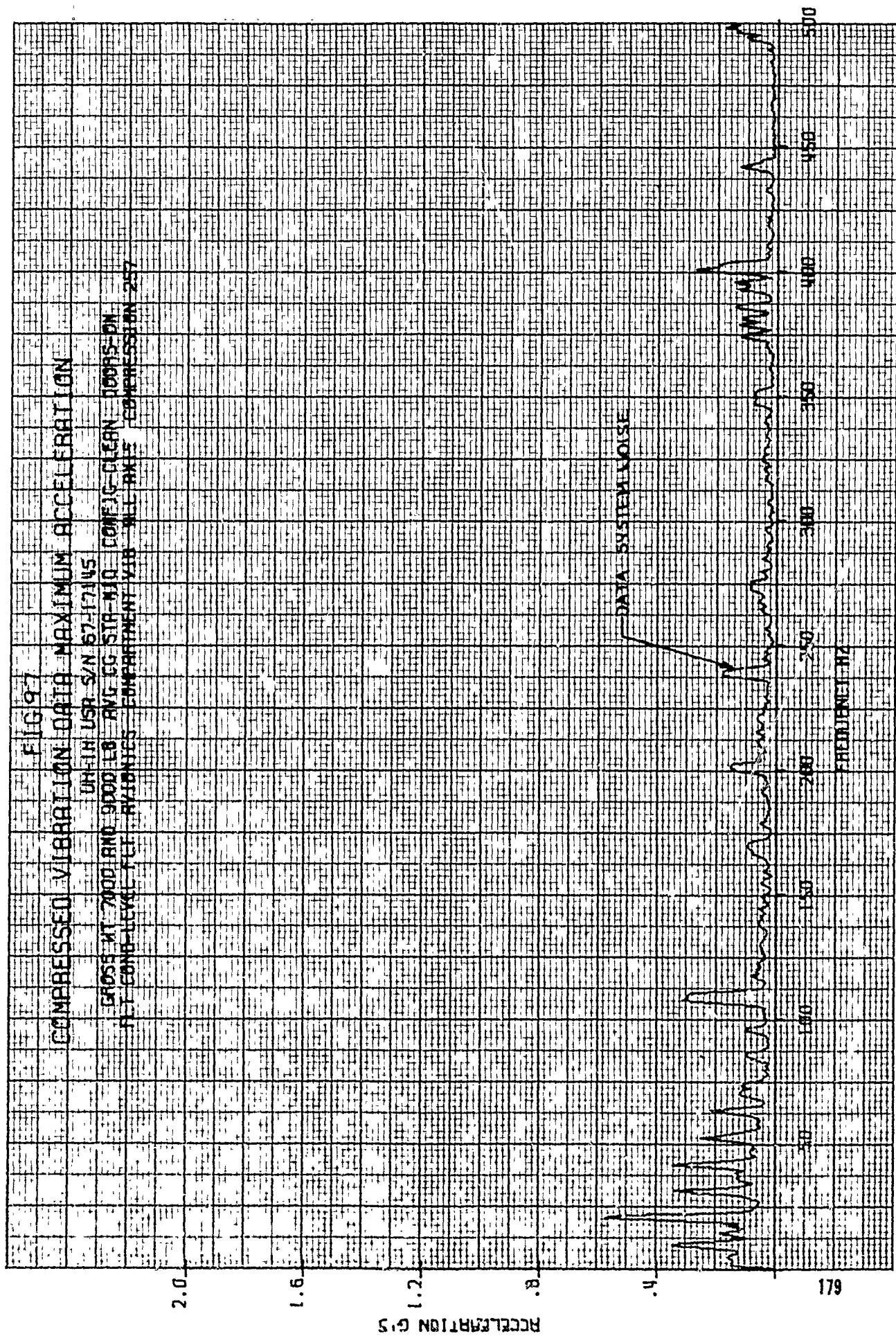
350

400

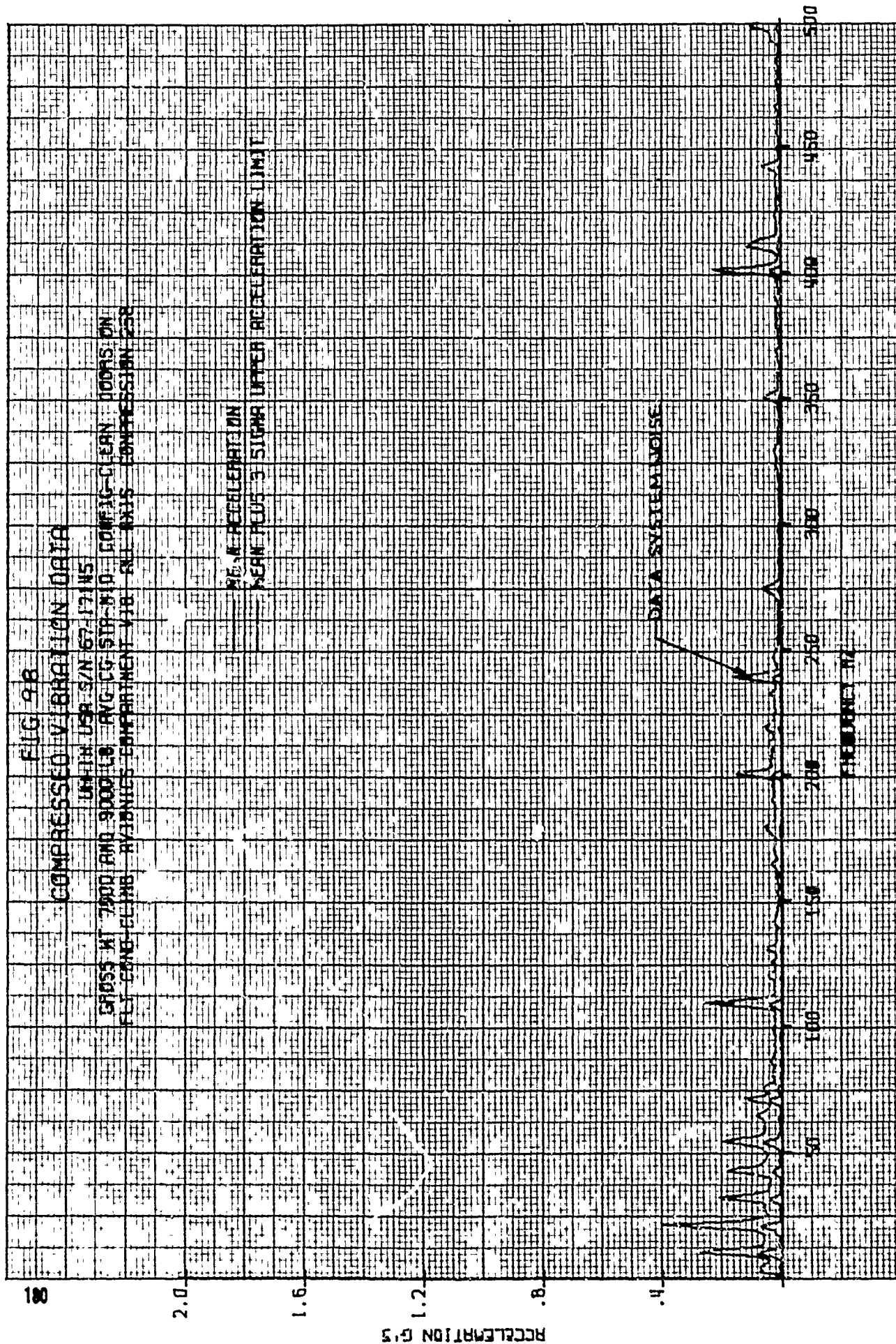
450

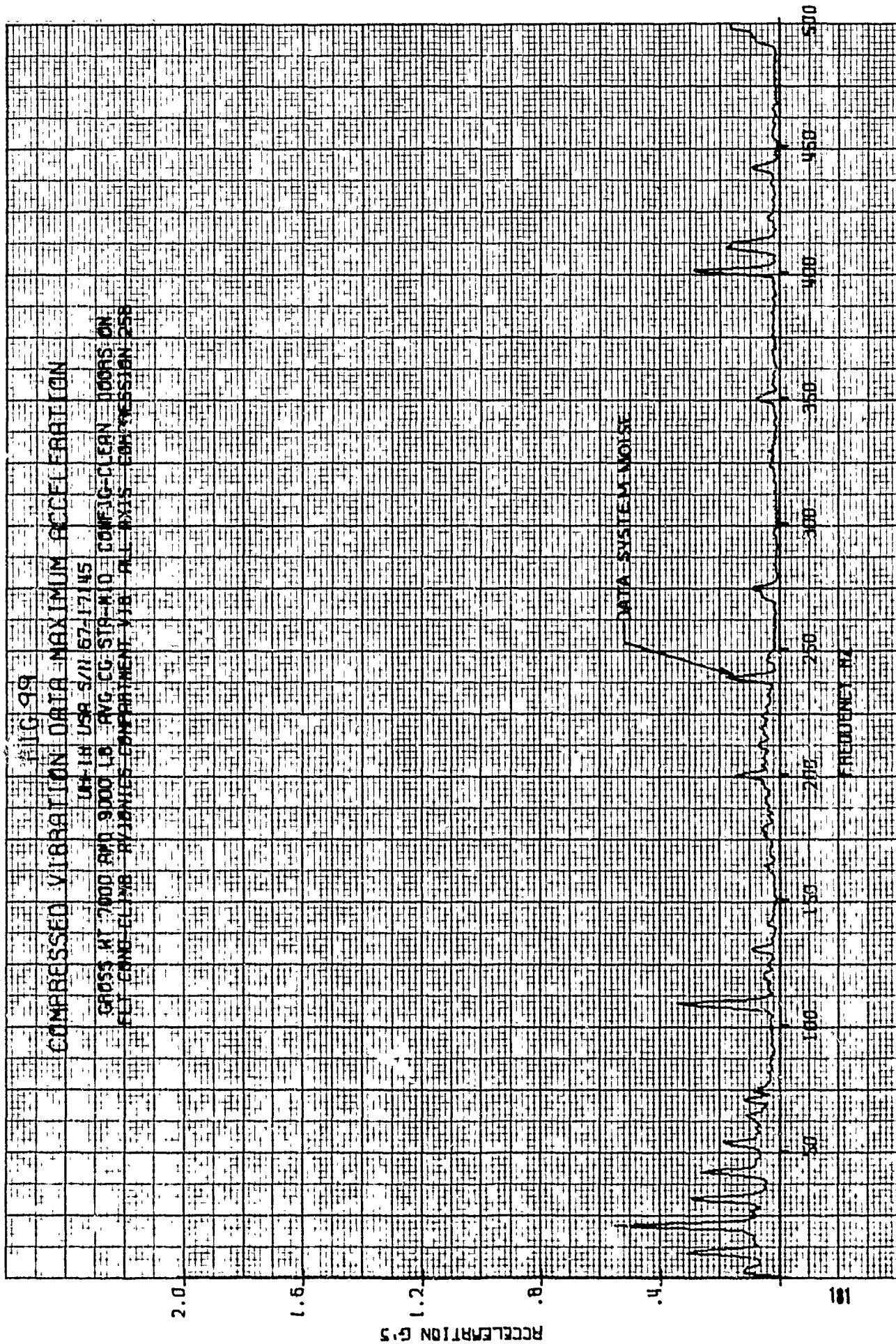
500

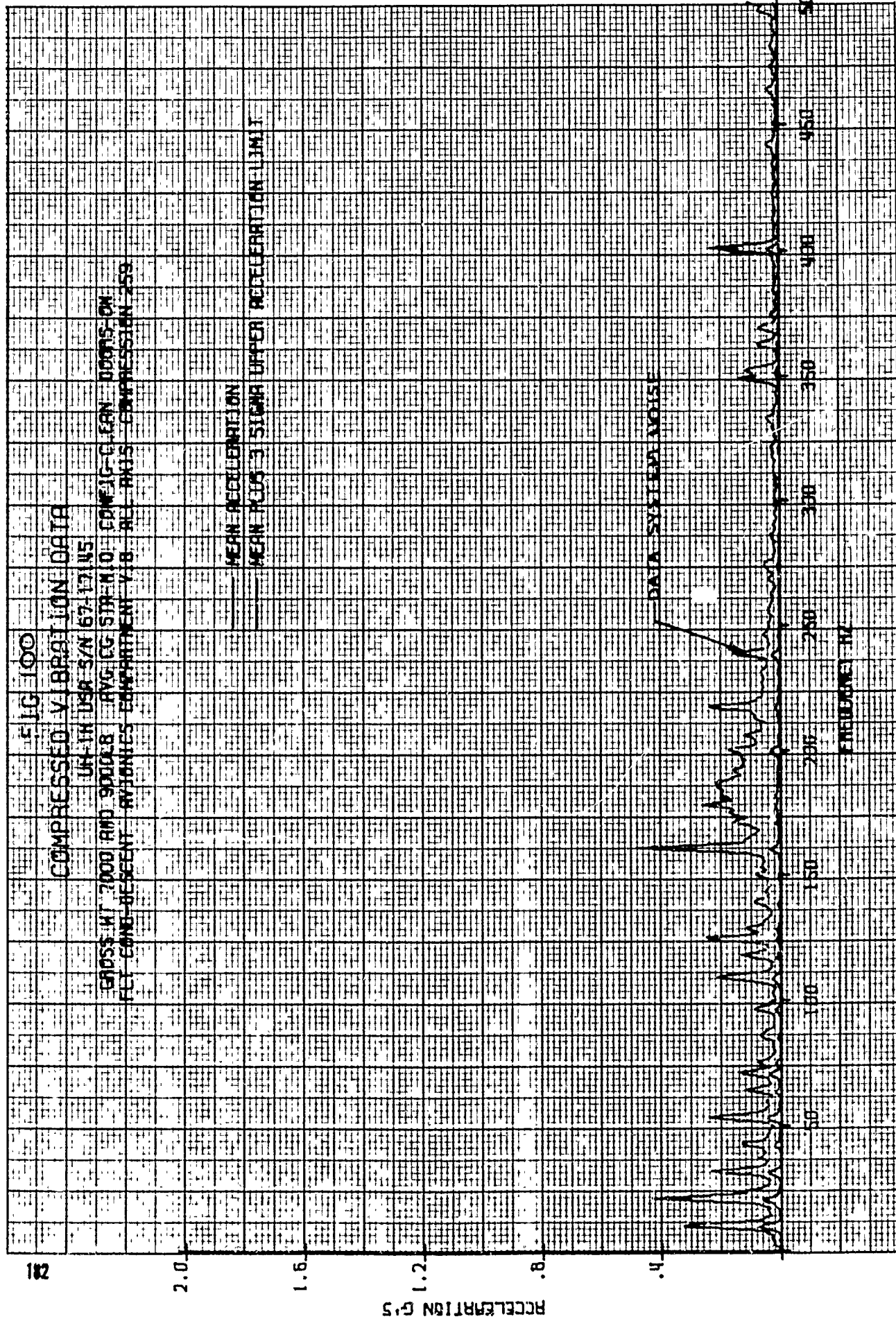
FREQUENCY HZ

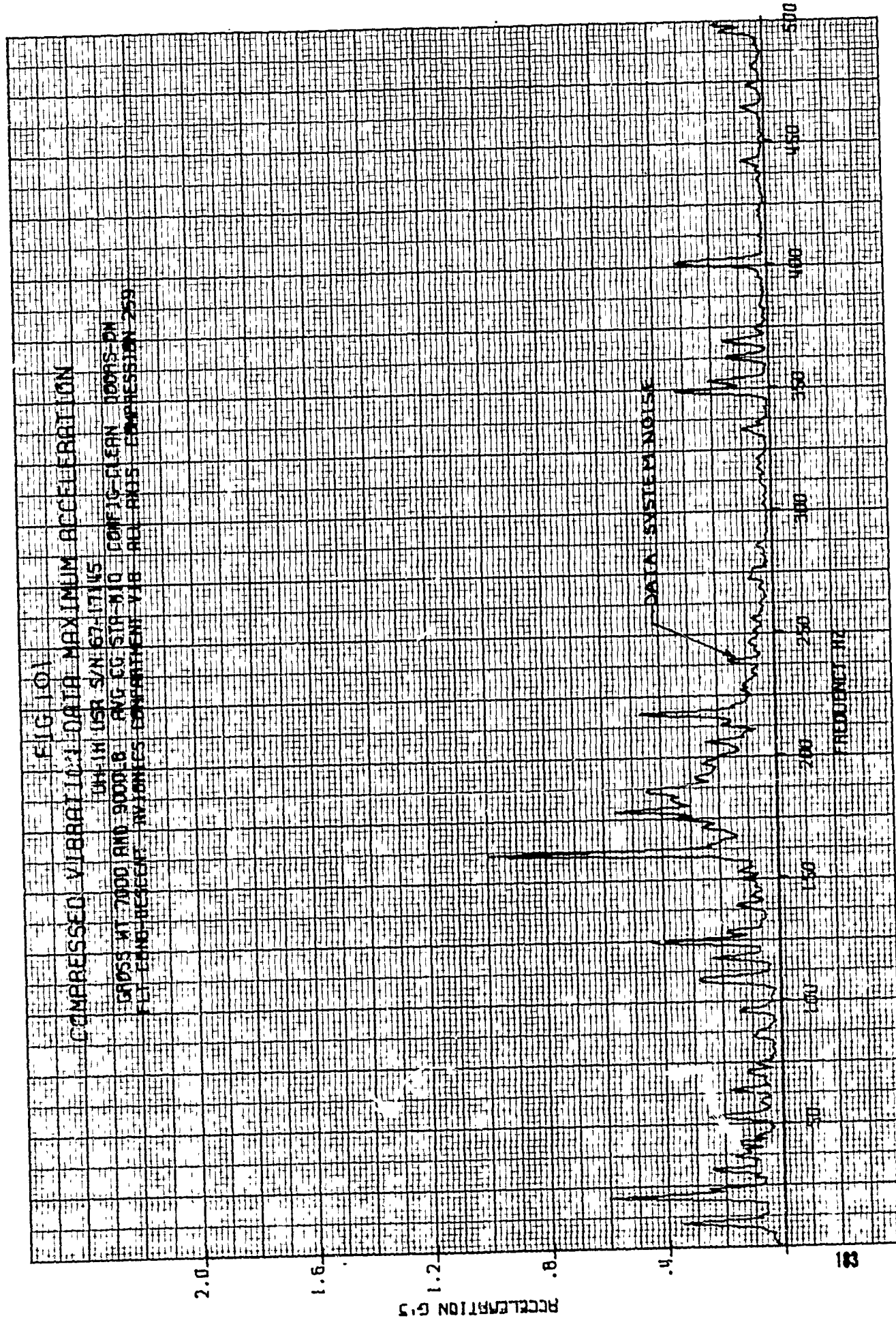


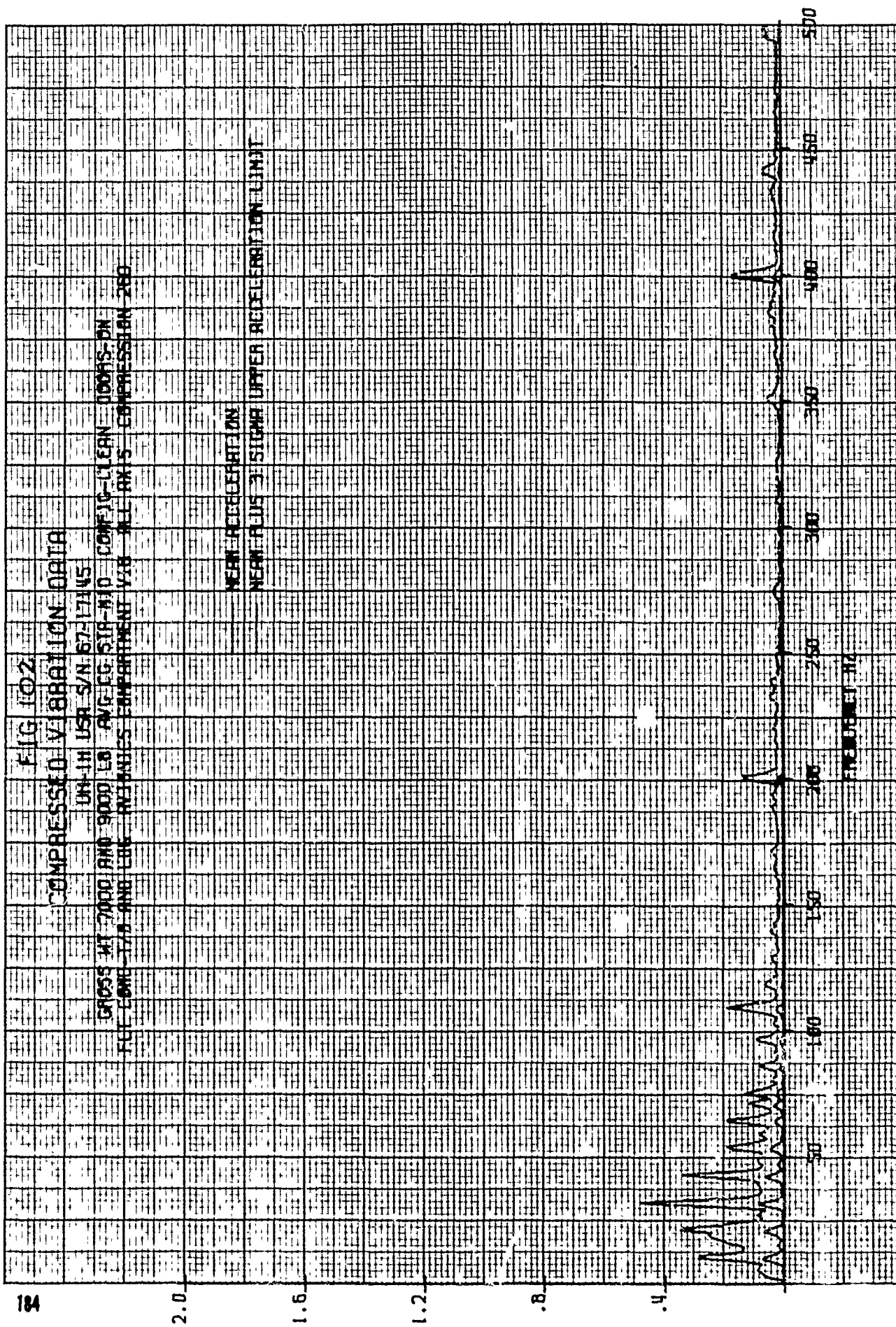
ACCELERATION G'S

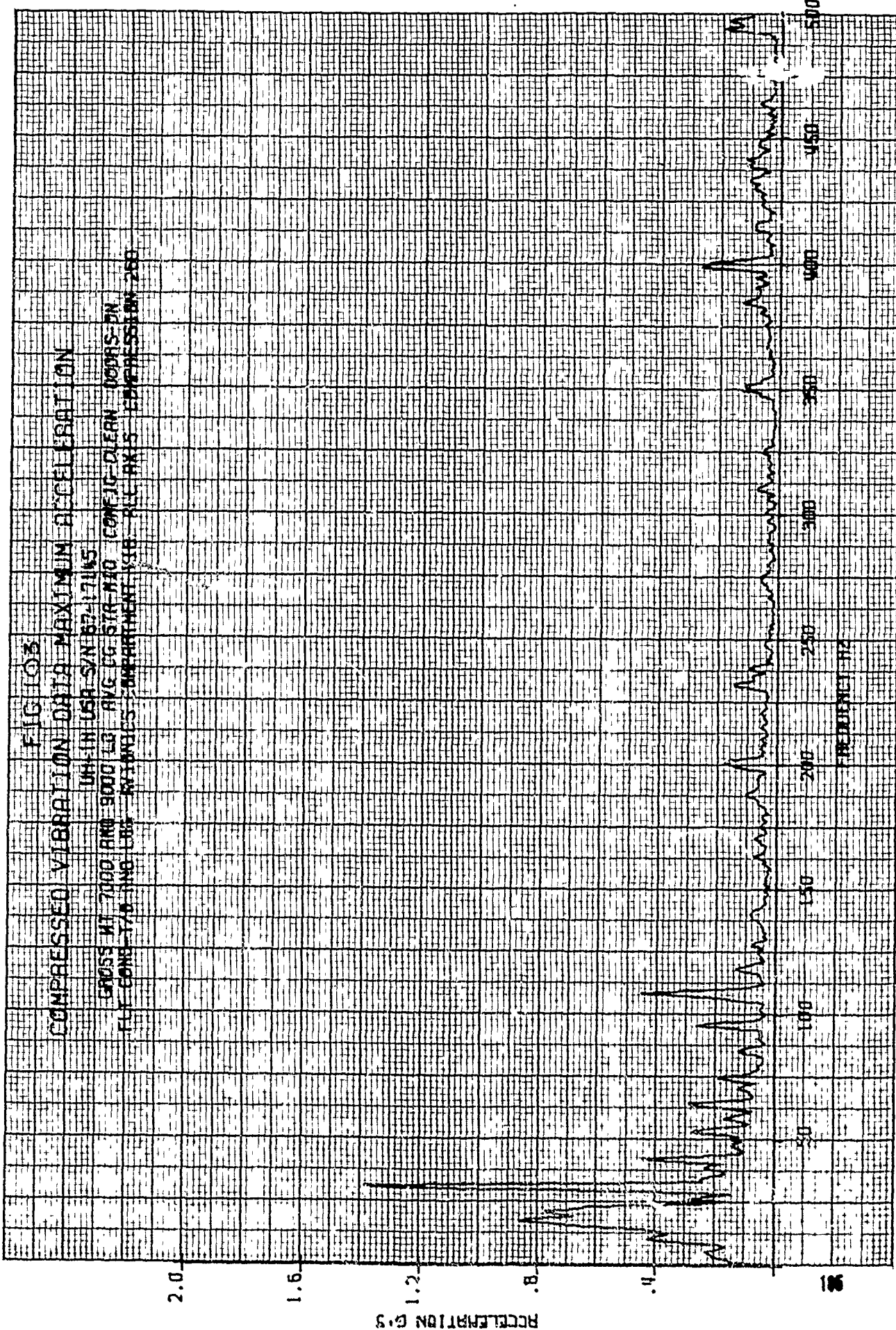












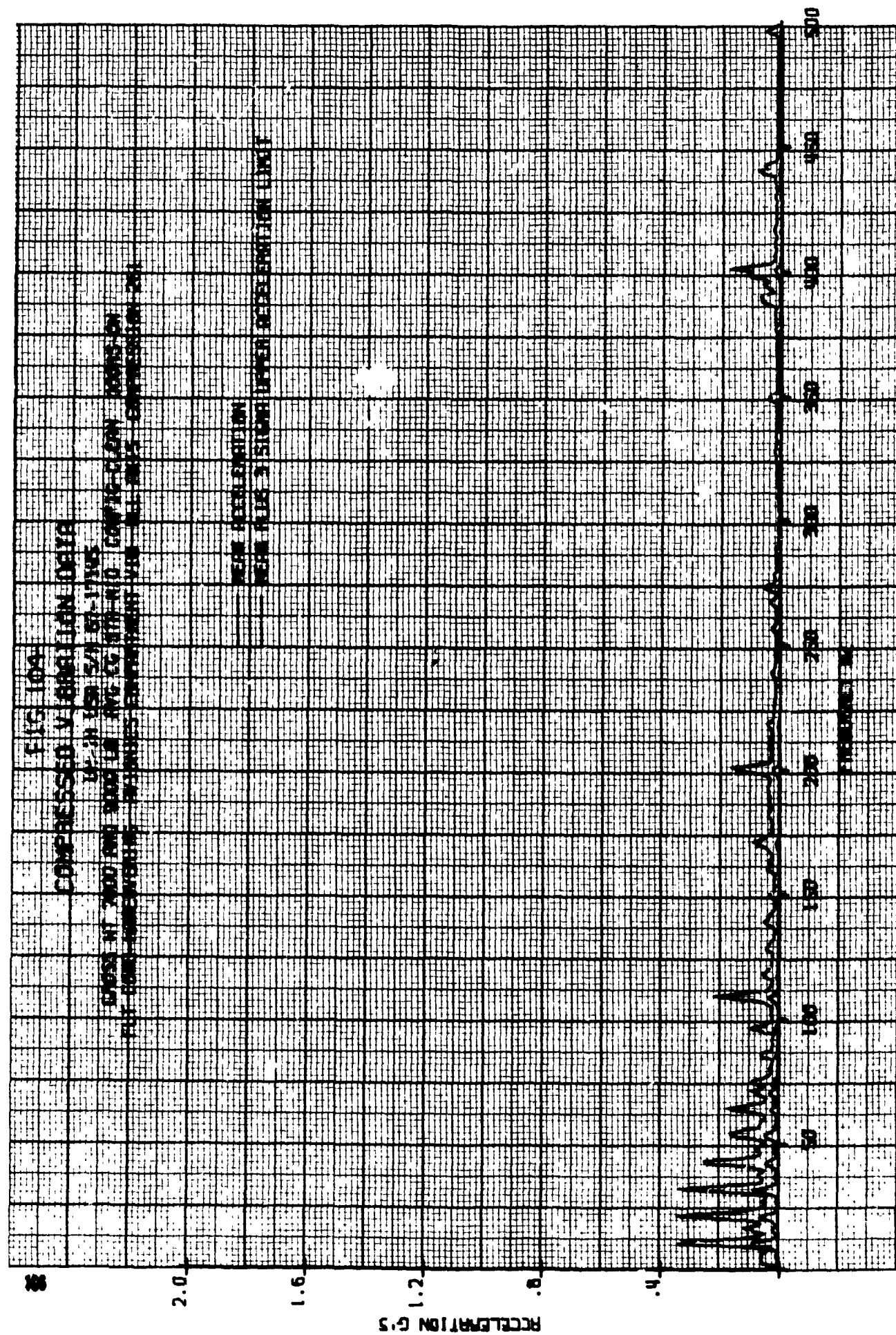


FIG 105

COMPRESSED VIBRATION DATA MEYERIN ACCELERATION

IN IN 150 S/100 1.100

CROSS AT 200 AND 300 LA 100 TO 300 AND COMPRESSION POINTS ON
PULSED VIBRATION IN PULSED COMPRESSION AT 100 200 300 COMPRESSION 200

2.0

1.6

1.2

0.8

0.4

ACCELERATION G'S

100

100

100

100

100

100

100

100

100

100

ACCELERATION G'S

2.0

1.6

1.2

.8

.4

FIG 106

COMPRESSED VIBRATION DATA

UH: IN USA S/N 57-17145
 GROSS WT 7000 AND 9000 LB AVG CG STA N10 CONJUG CLEAN UDDRS ON
 CNO TEST CNO CNO FLT JOLC W/IONICS COMPARTMENT 478 ALL AXIS COMPRESSION 262

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

0

100

200

300

400

500

600

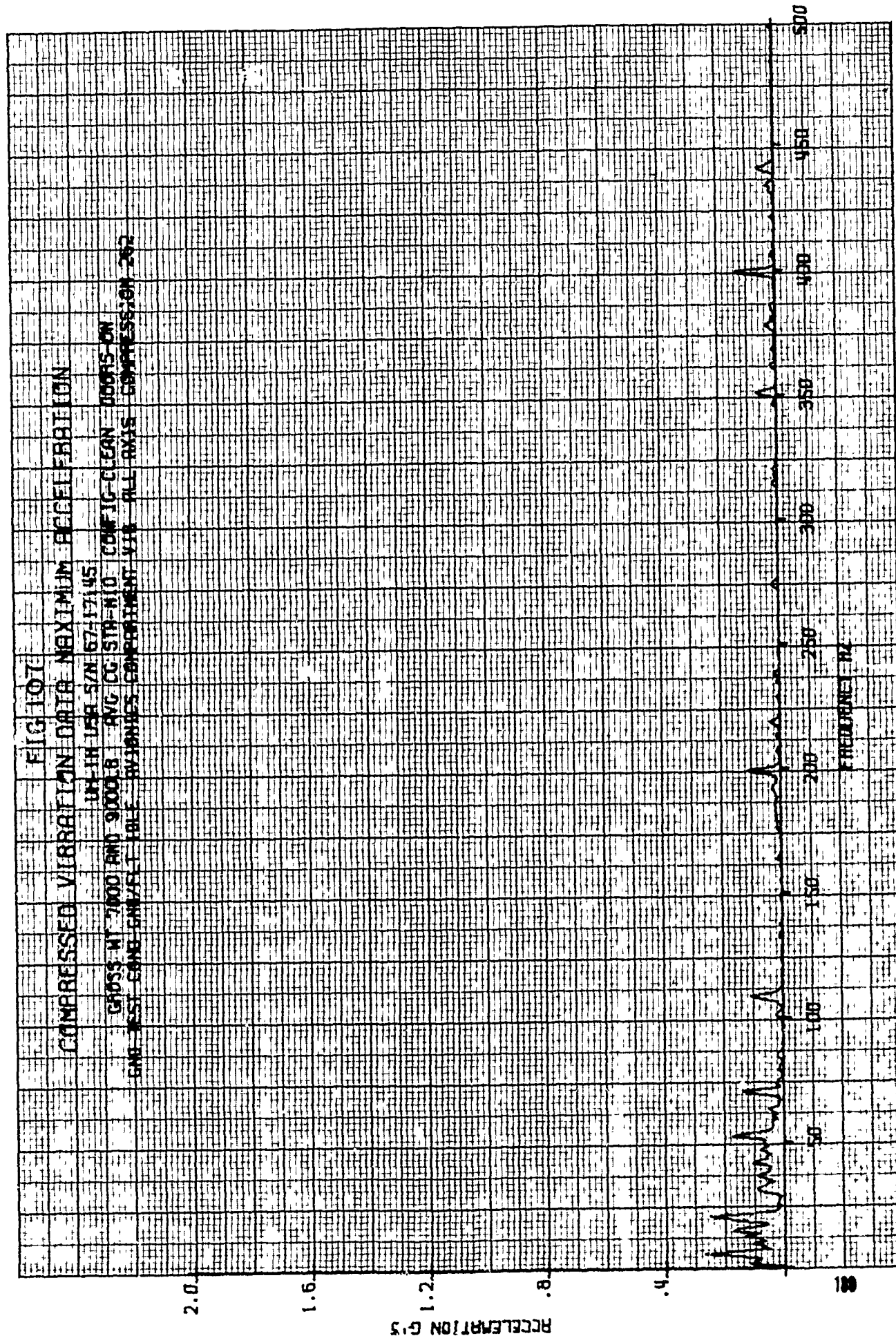
700

800

900

1000

FREQUENCY



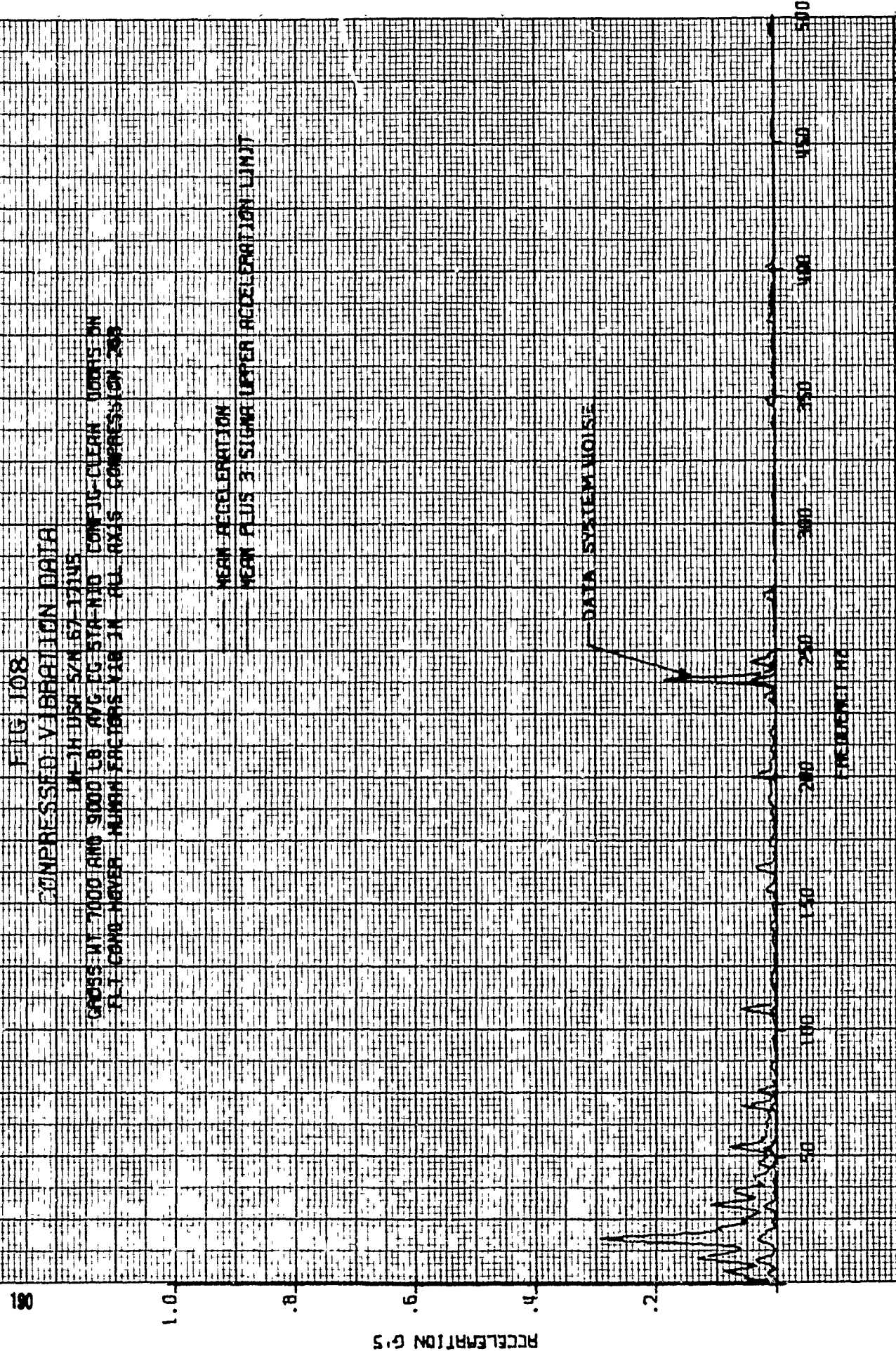


FIG 109

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

IN-11158 S/N 57-17145
GROSS WT 7000 LBS AVG CC STA N10 COMF IG-DEAN DIVISION
ACT COMB POWER NUMBER FACTORS Y18 IN ALL AXIS COMPRESSION 283

1.0

.8

.6

.4

.2

ACCELERATION G'S

191

DATA SYSTEM NOISE

50

100

150

200

250

300

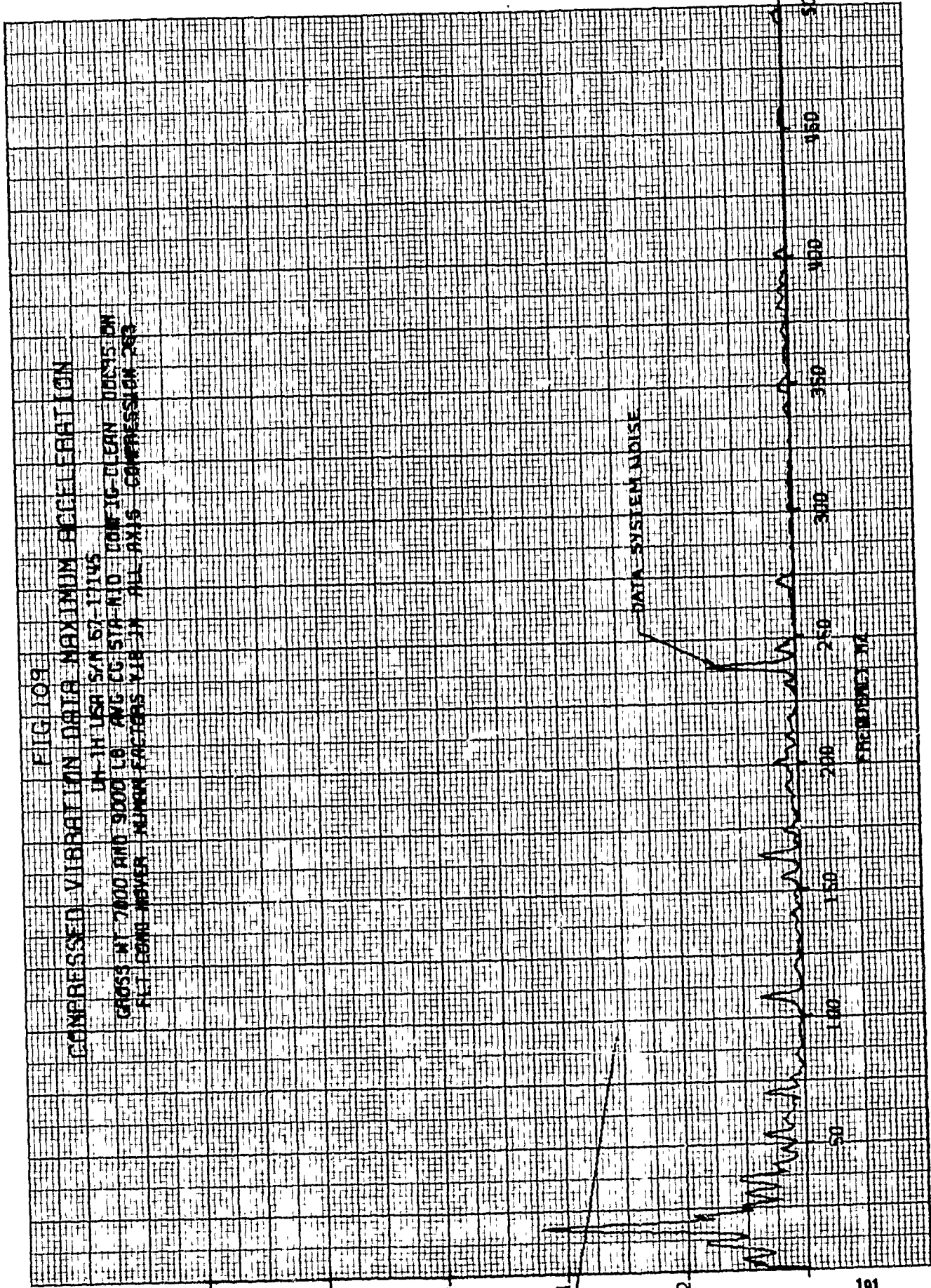
350

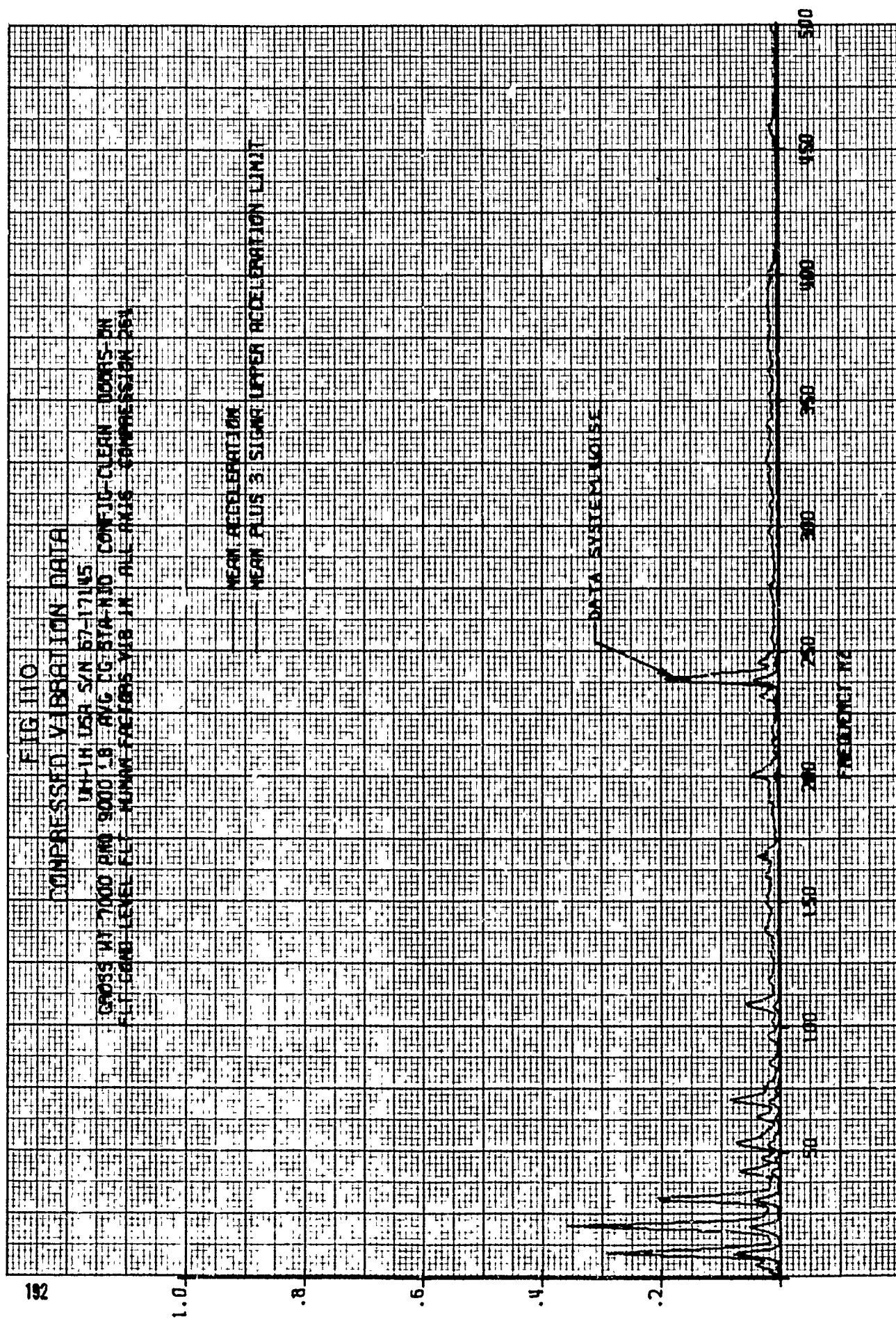
400

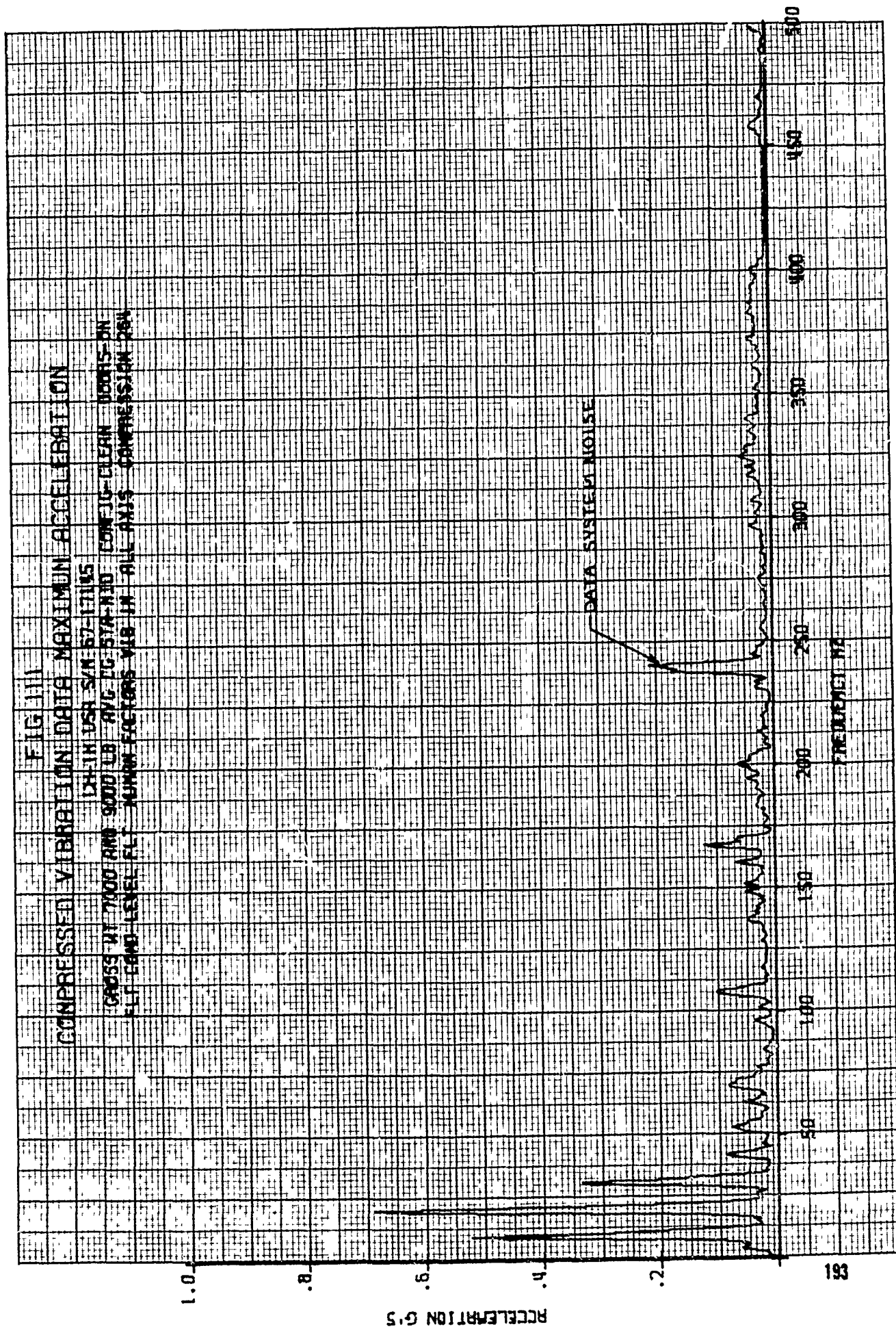
450

500

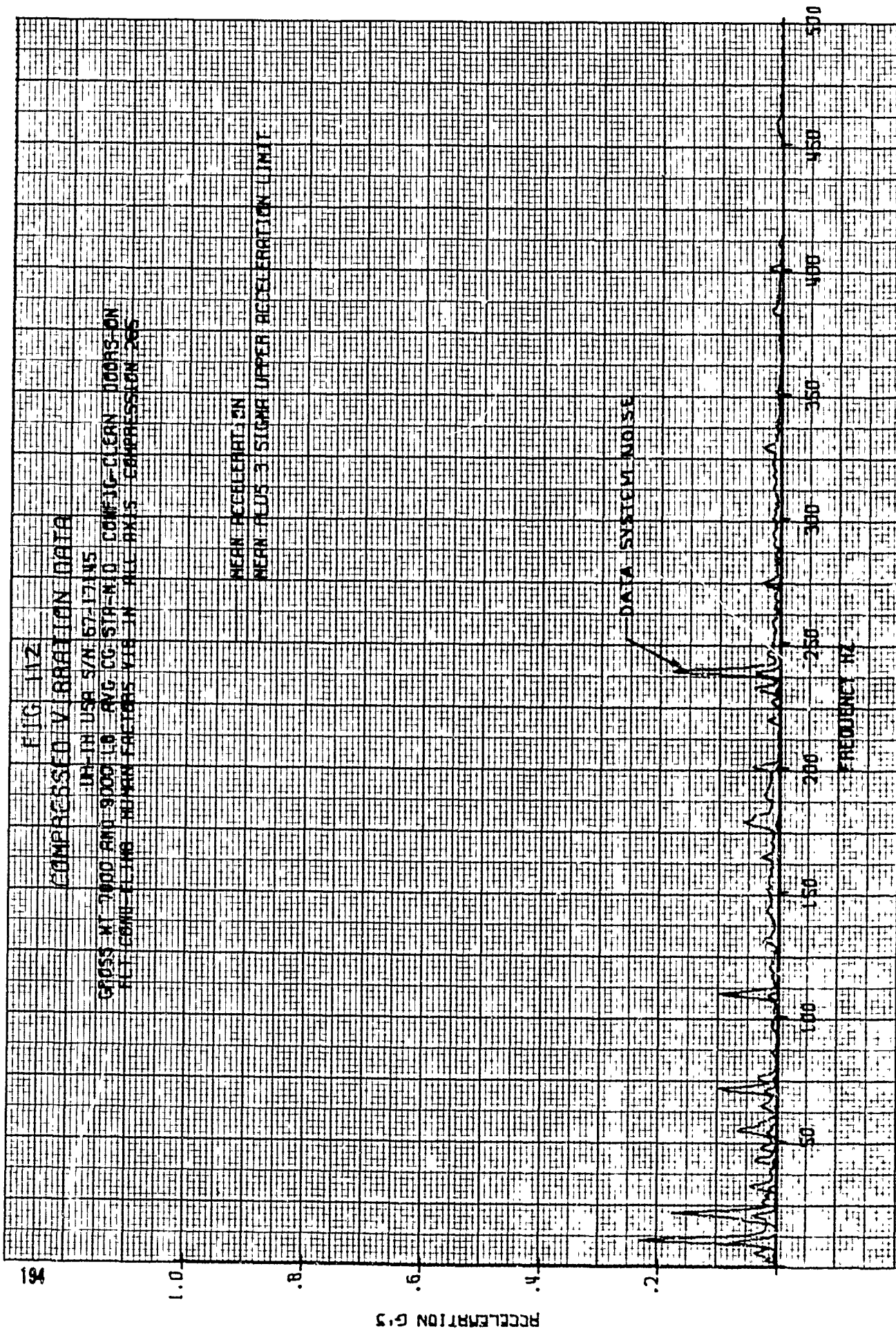
FREQUENCY Hz

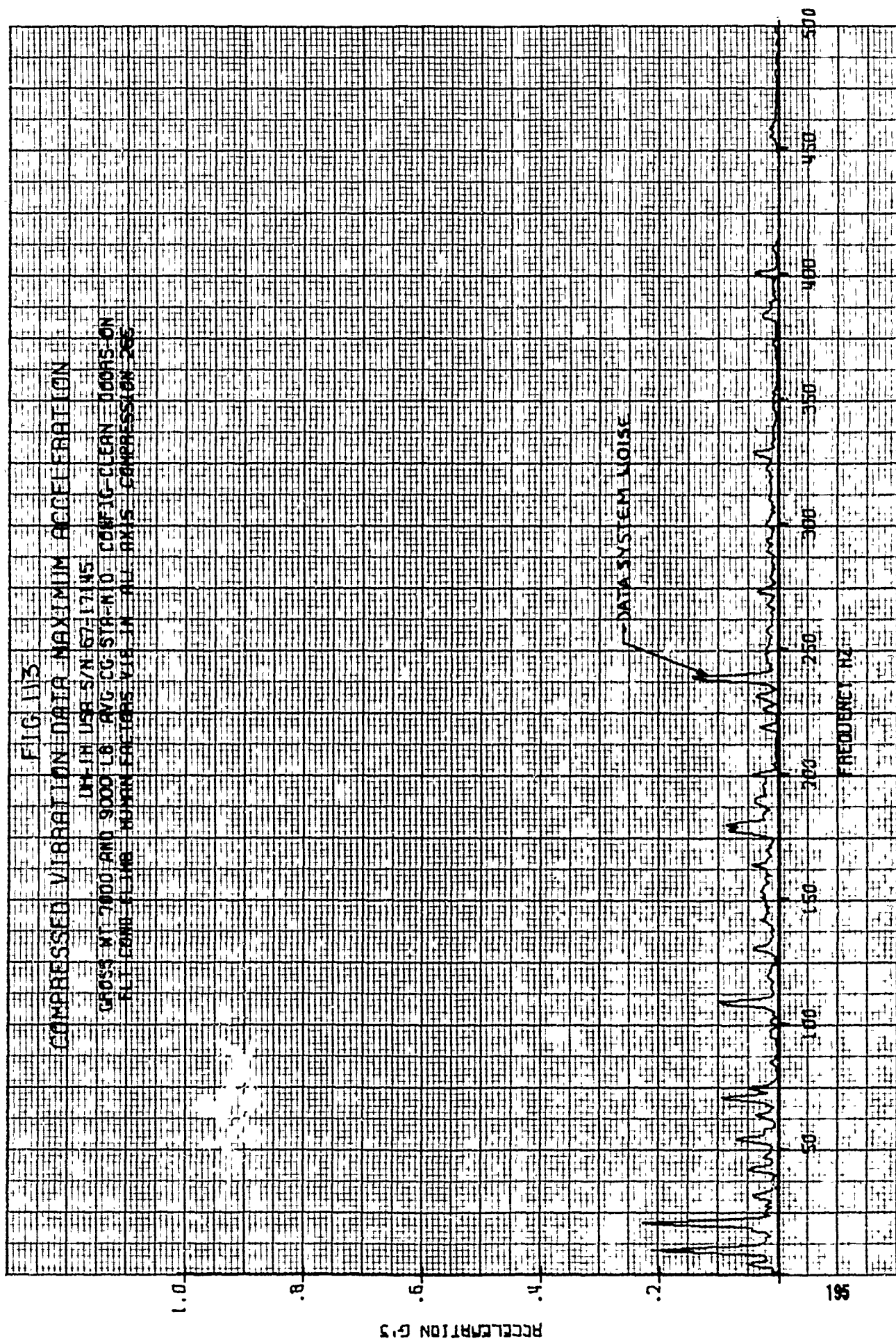






ACCELERATION G'S





COMPRESSED VIBRATION DATA

OROSS MT 7000 AND 9000LB RYG LG STA-NHO CONJUG CLEAN BODIES-DE
 FLT-COND DESCENT HUMAN FACTORS VIB IN ALL 2-1/2 COMPRESSOR 250

1.0

.8

.6

.4

.2

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE

50

100

150

200

250

300

350

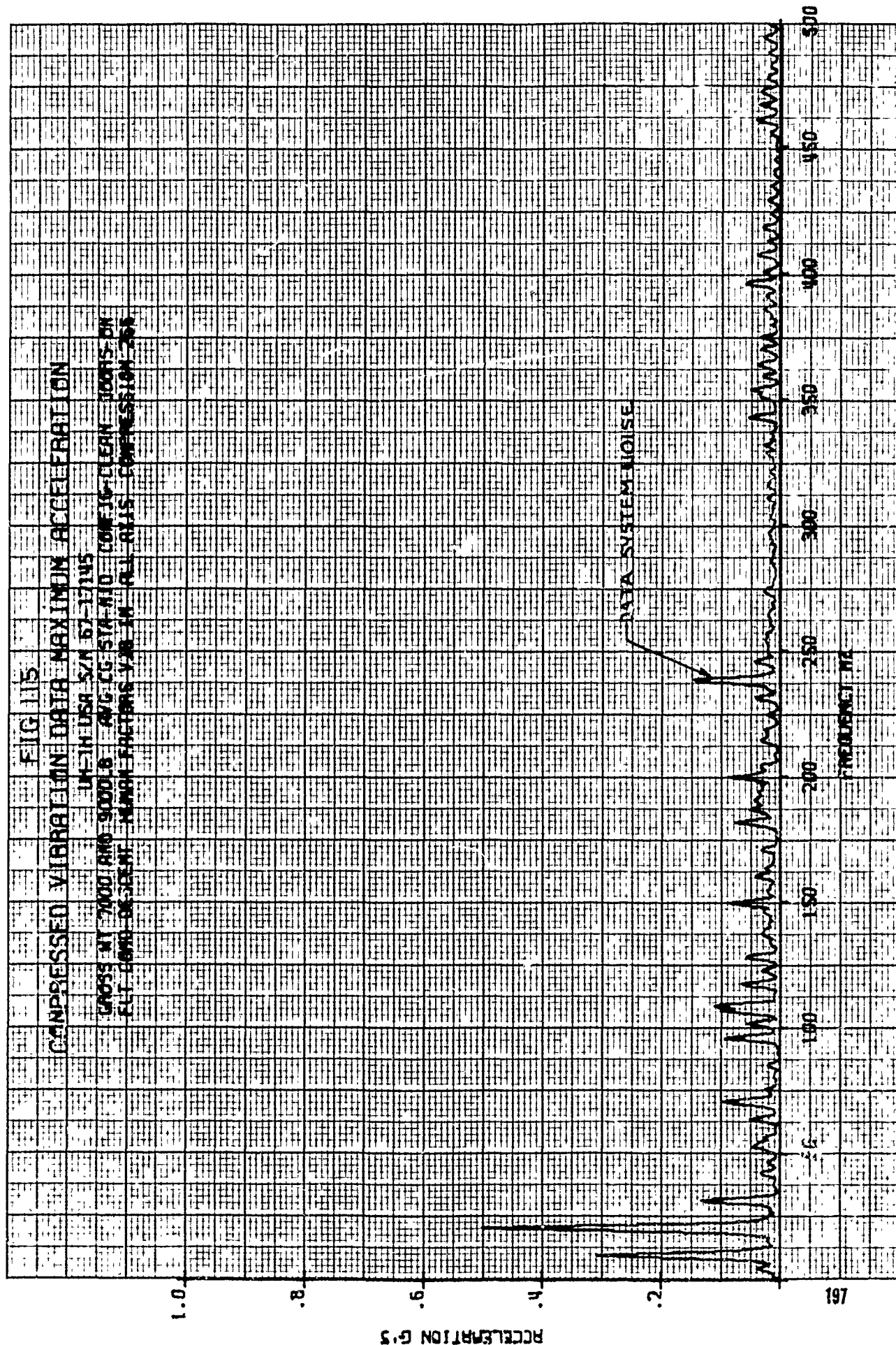
400

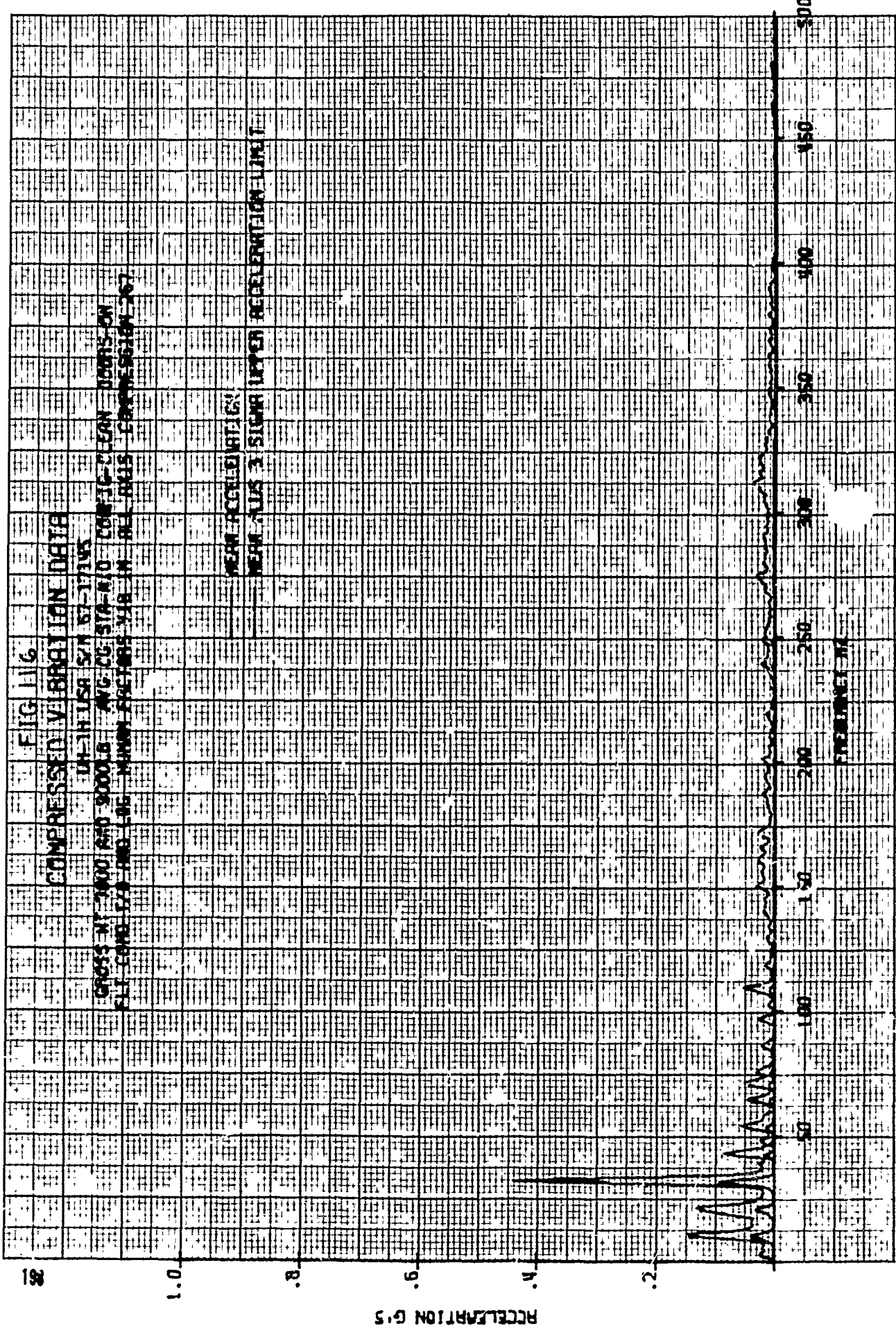
450

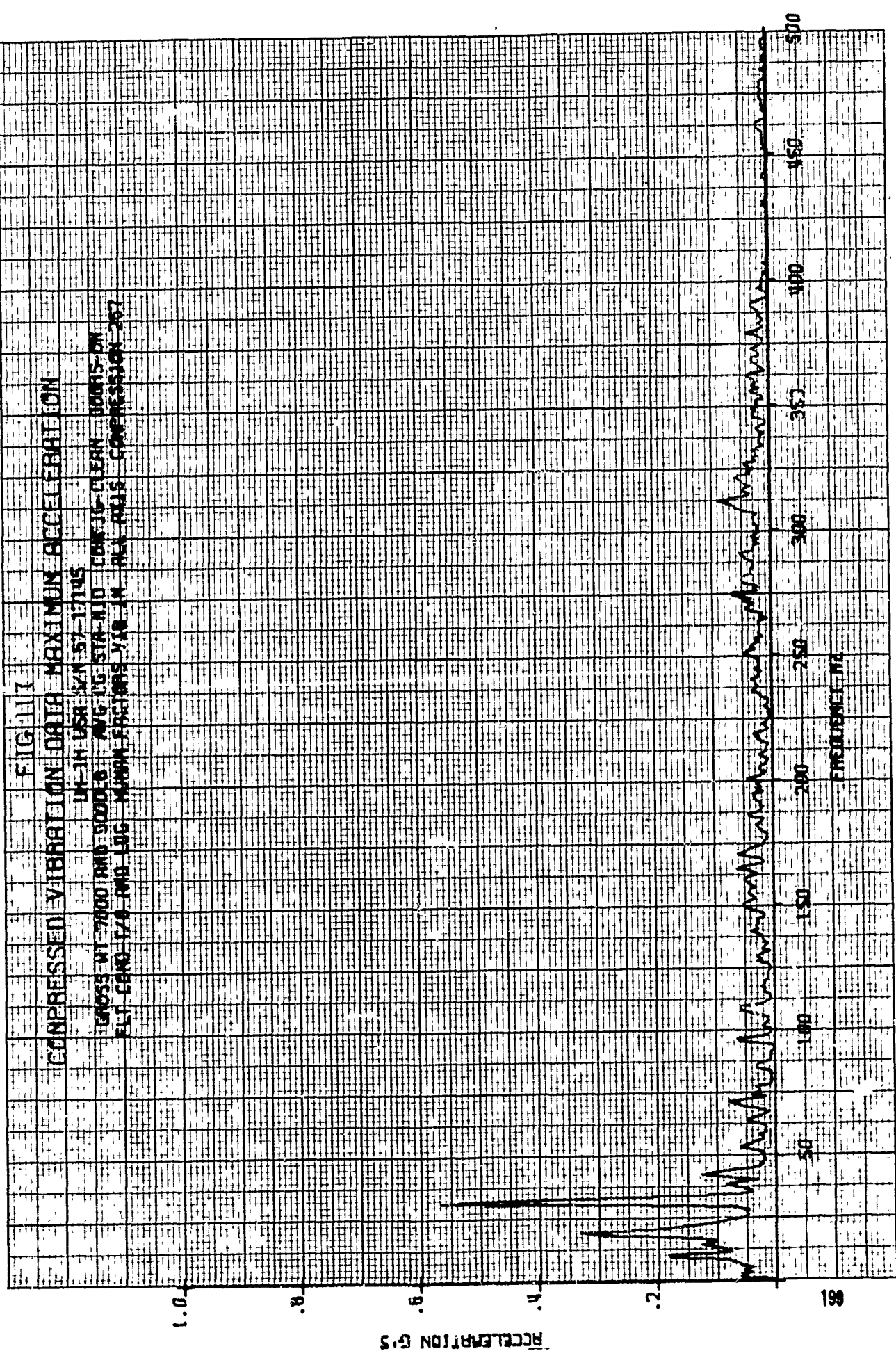
500

PERCENTAGE

ACCELERATION G'S







COMPRESSED VIBRATION DATA

GROSS WT. 7000 RING 8000 LB. AVE. CG. STA. 400 CONJIG. CLEW. DOWNS ON
 LH-1H USR S/N 67-17115
 FLT. CARGO HANDLING MUNCH FACTORS VIB. IN ALL AXES COMPRESSION 200

1.0

.8

.6

.4

.2

ACCELERATION G'S

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

50

100

150

200

250

300

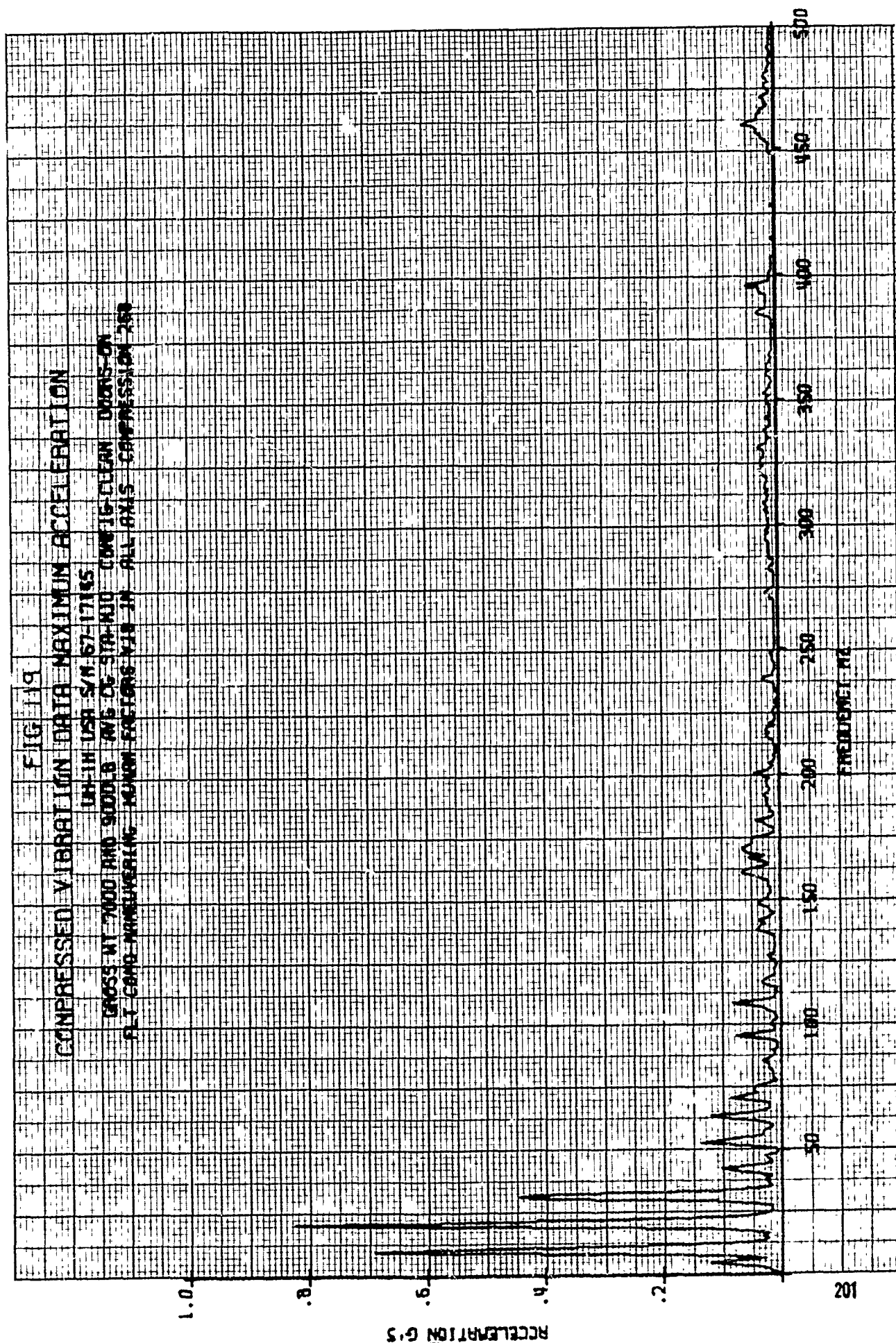
350

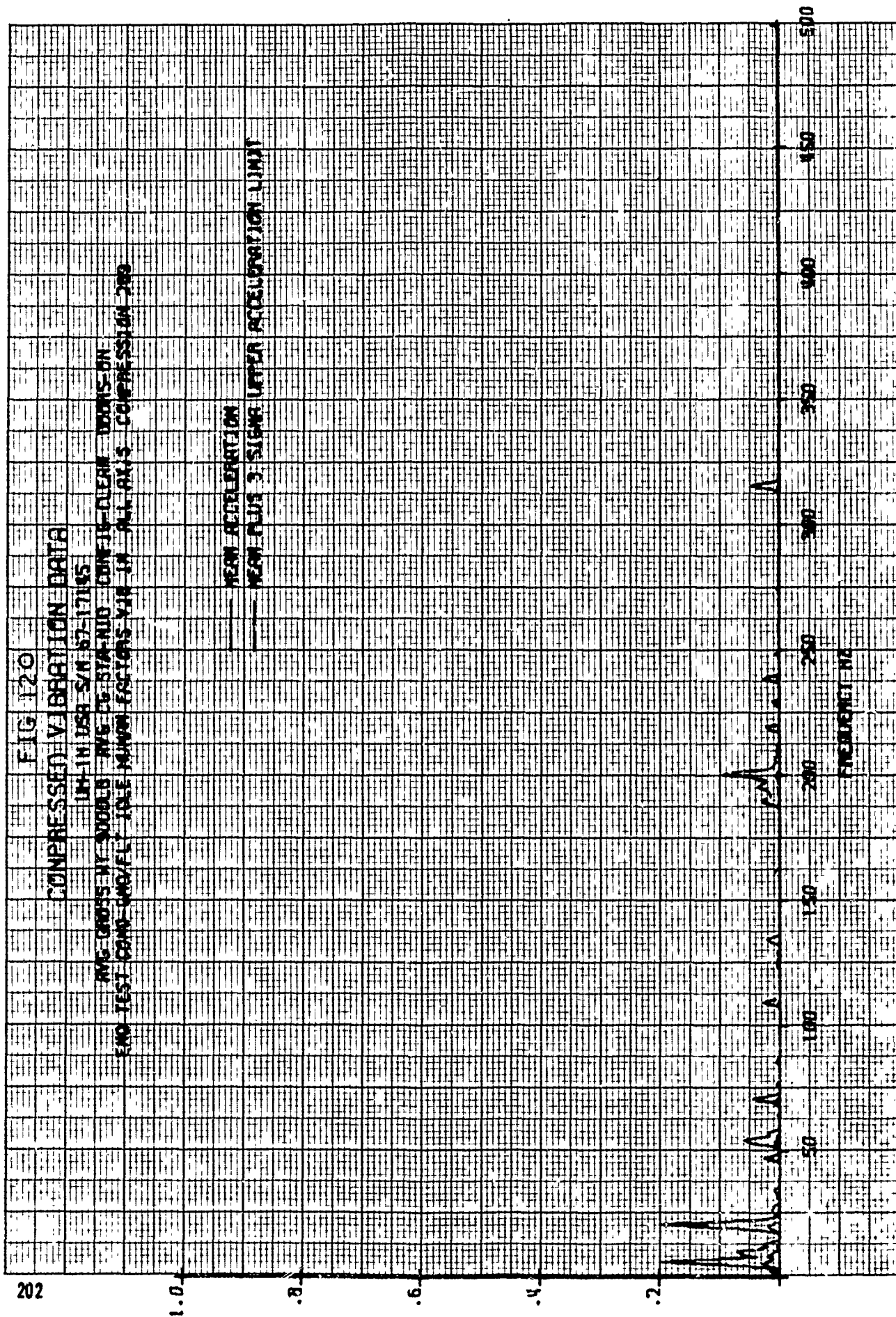
400

450

500

FREQUENCY Hz





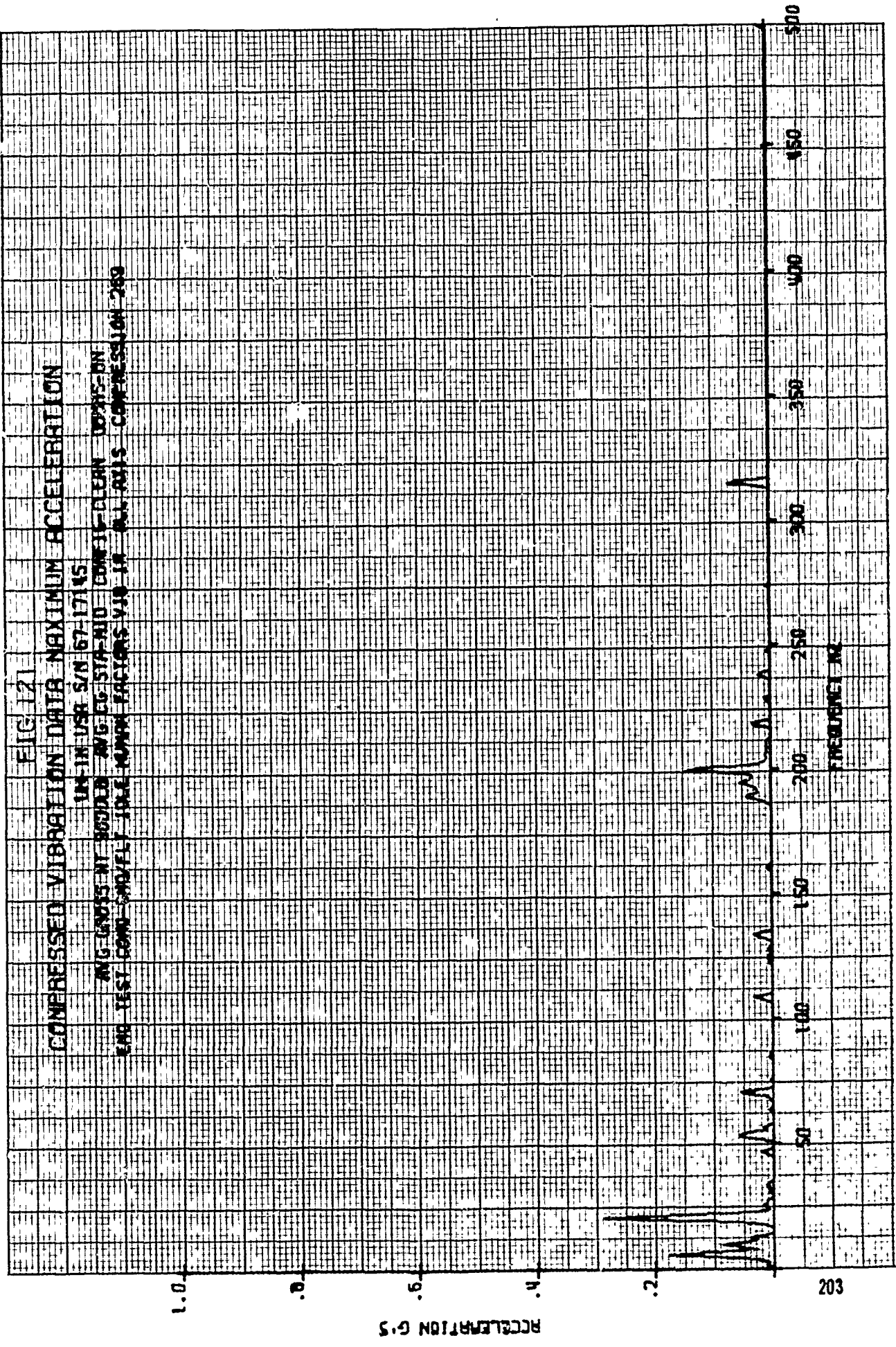


FIG 122

COMPRESSED VIBRATION DATA

LA-24 USA 5/4 67-17115
 GROSS WT 7000 AND 8000 LB AVG EG STA-HED CON-JU-CLEAN BOARDS ON
 FLT CARO-NEVEN MASHM FACTORS 1/8 BUT ALL ALLS COMPRESSION 200

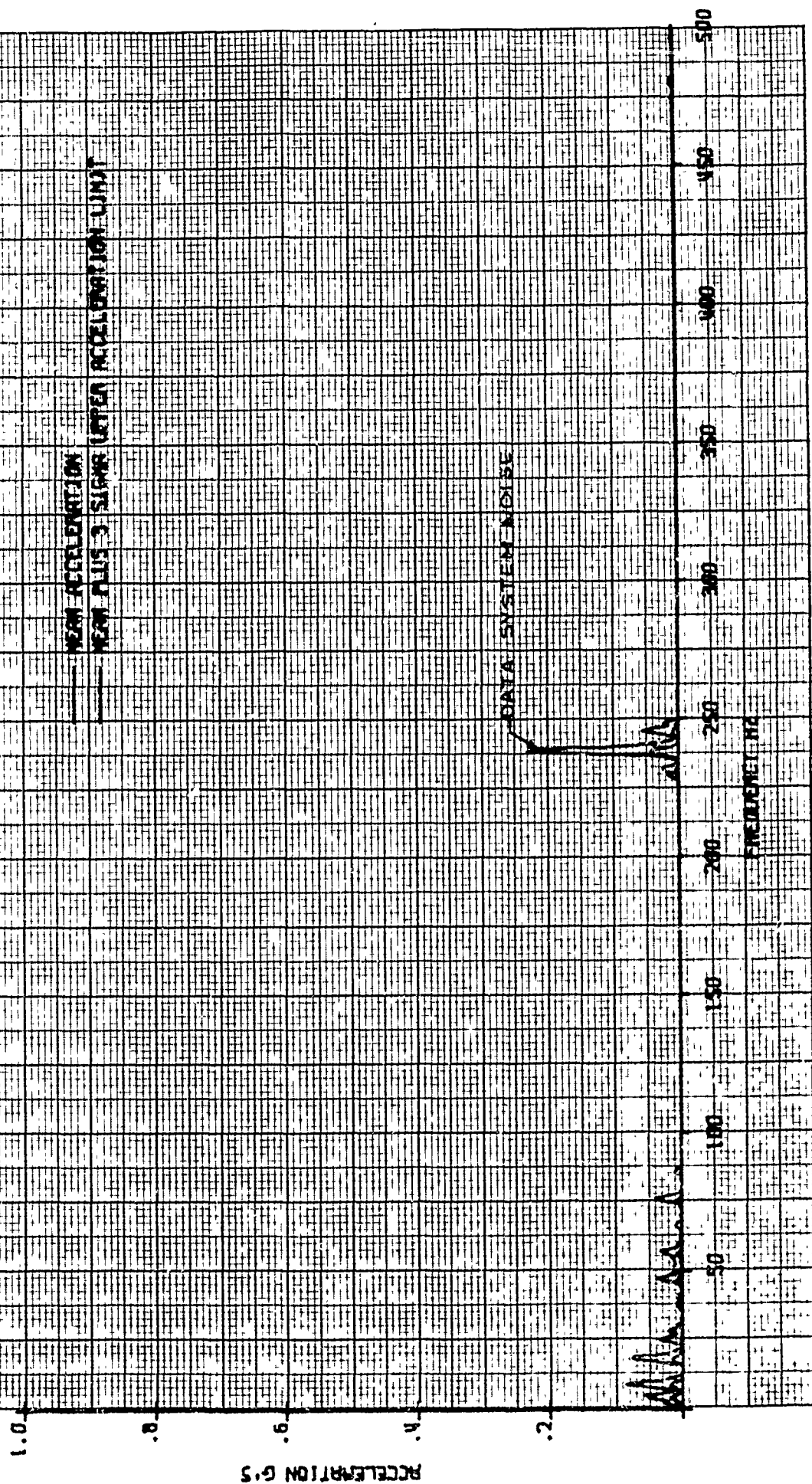


FIG 123

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UN-1N USR S/N 67-172NS
GROSS WT 7000 LBS GROSS LG 245 CG 574-MID EOP-16-ELCHN 080815 ON
ALL COMPRESSION FACTORS 1.18 BUT ALL ALL COMPRESSION 200

1.0

.8

.6

.4

.2

NR

ACCELERATION G'S

DATA SYSTEM NOISE

250

300

350

400

450

500

550

600

650

700

750

800

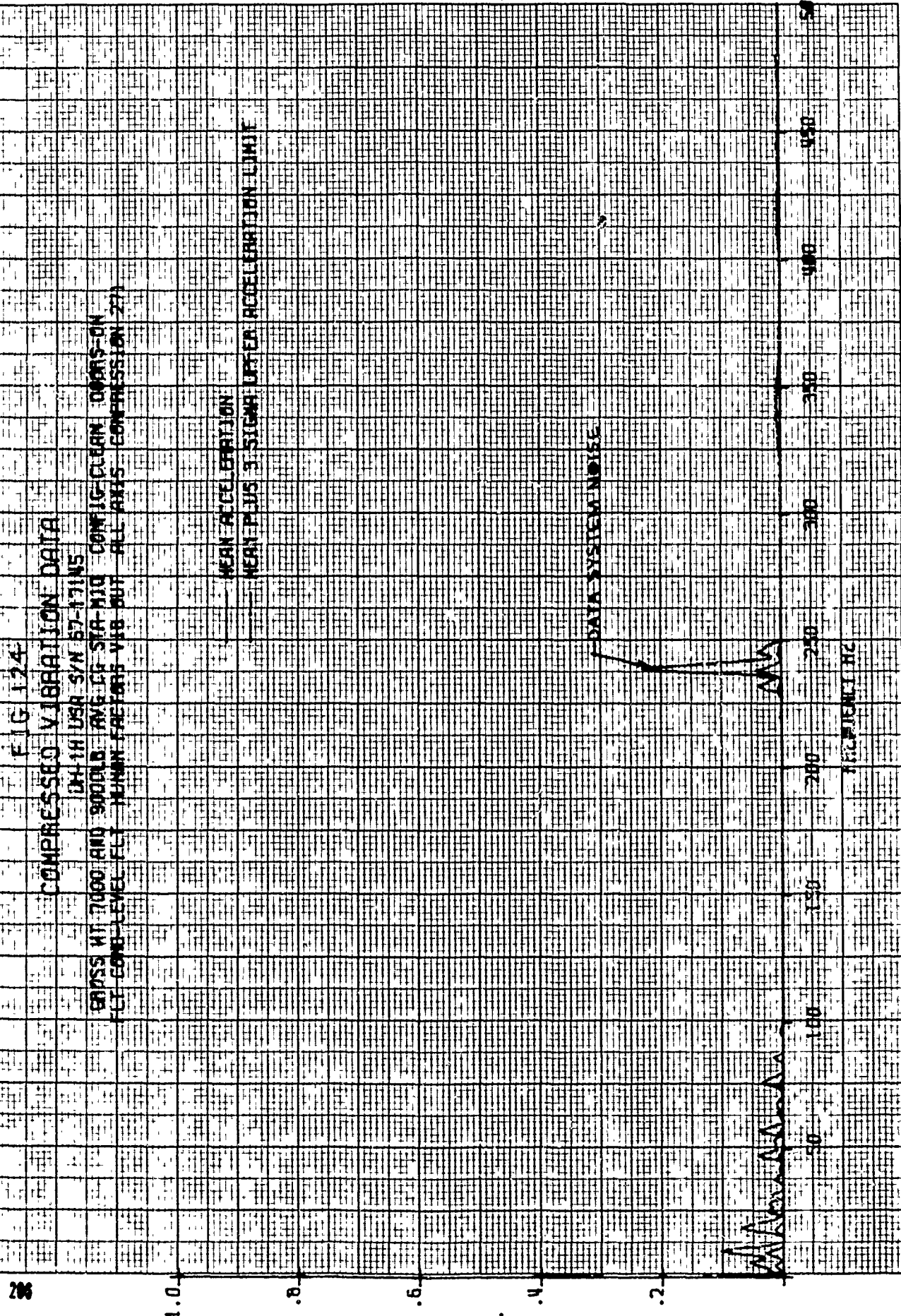
850

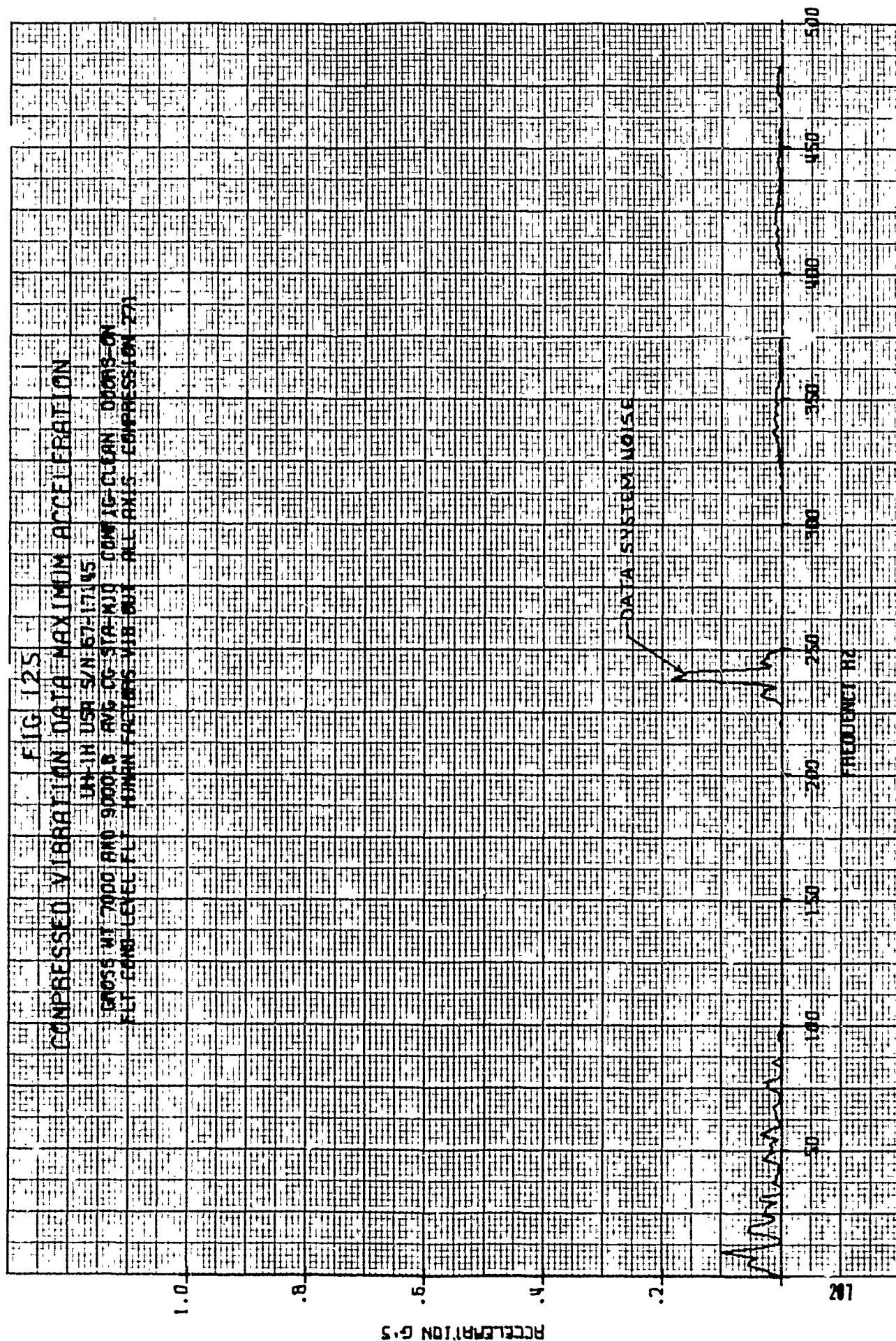
900

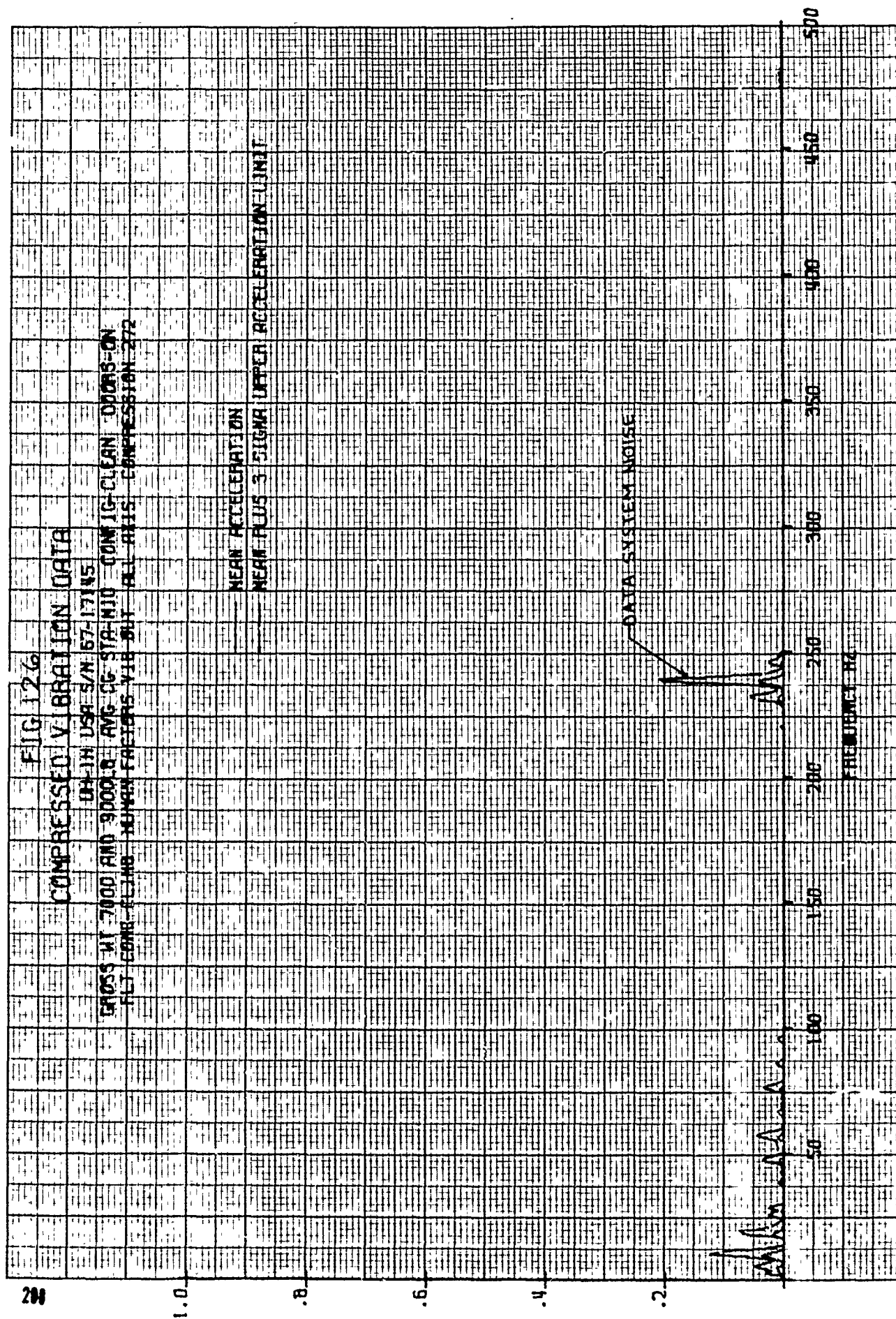
950

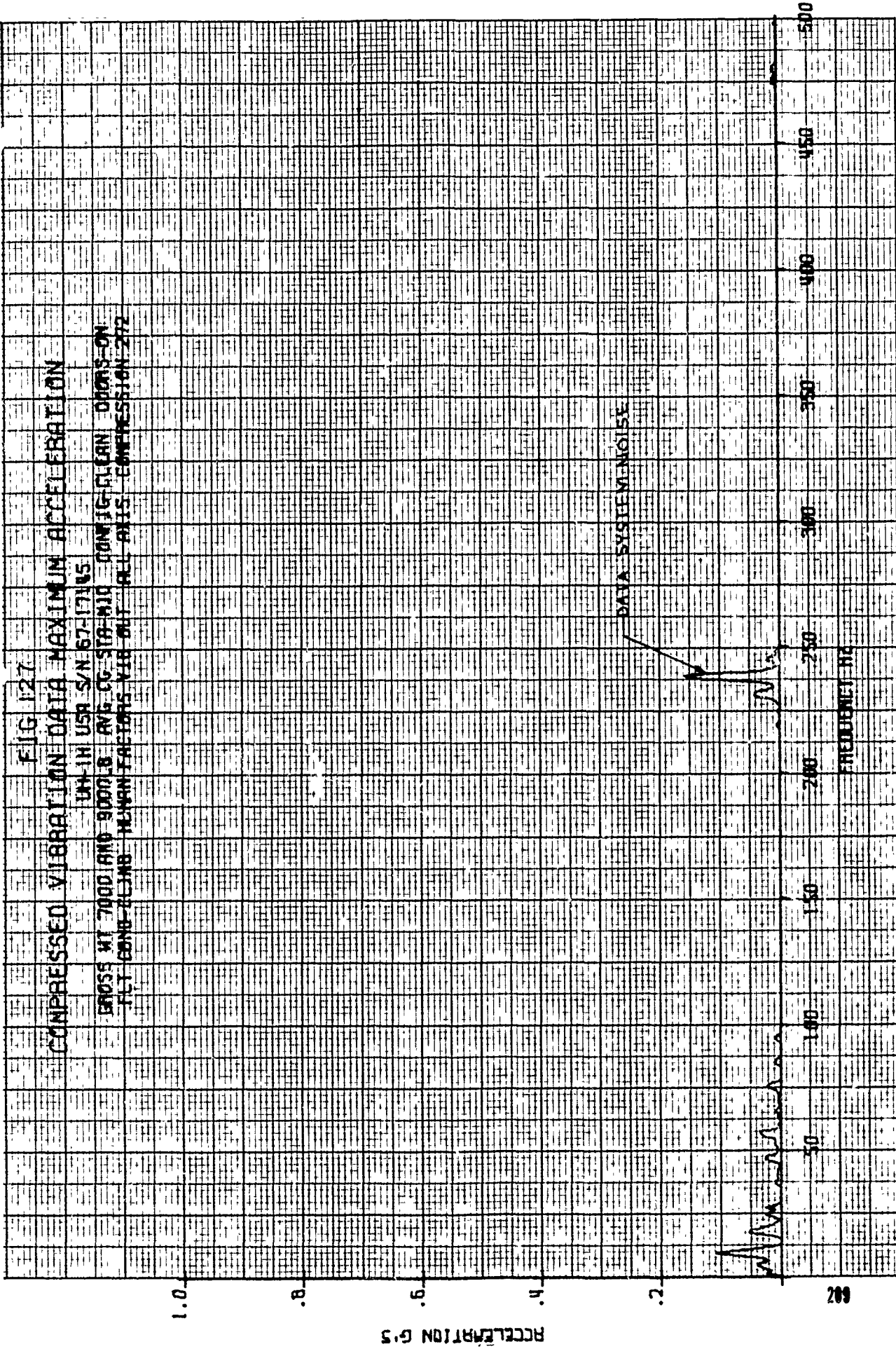
1000

FREQUENCY Hz









210

ACCELERATION G'S

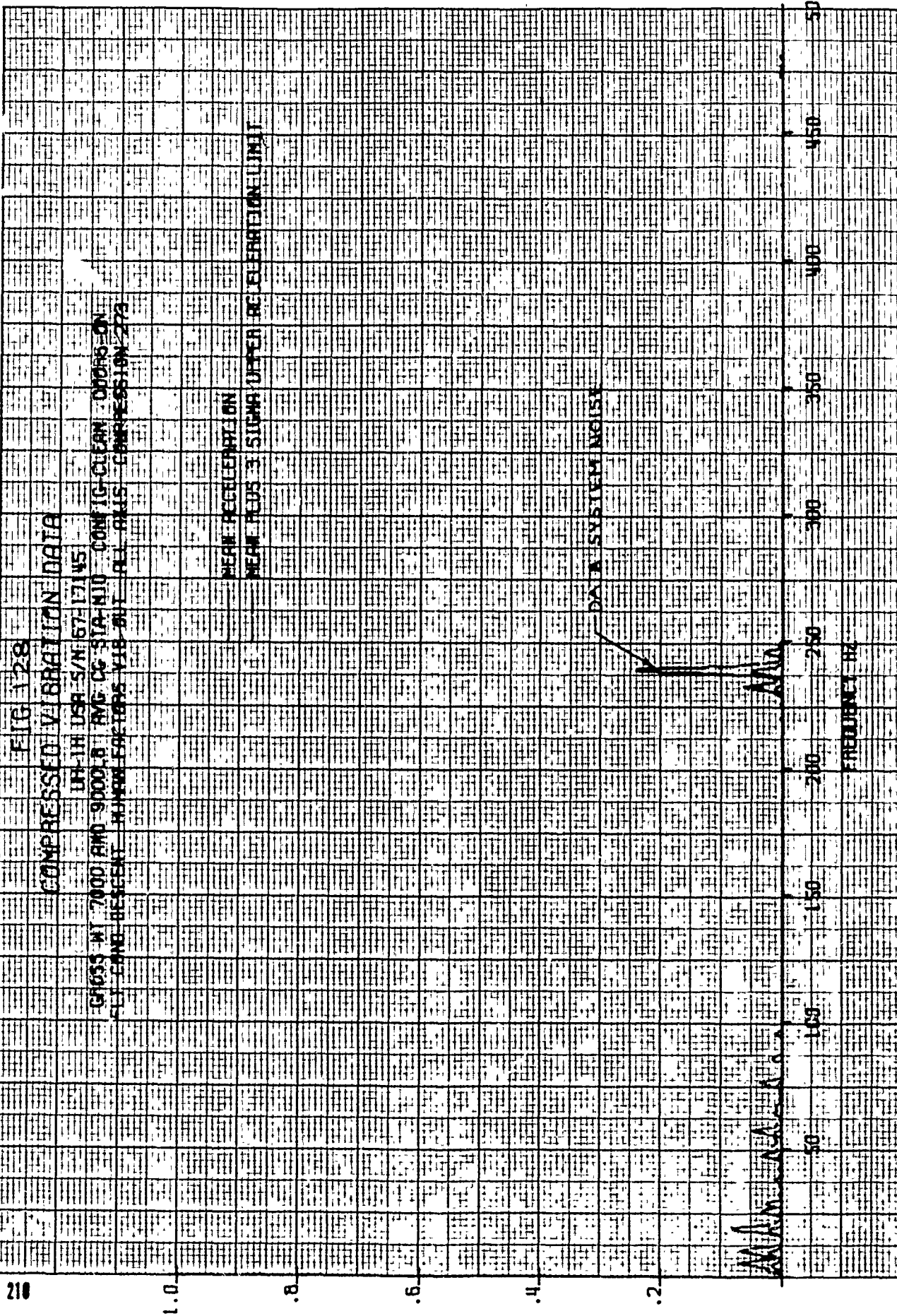
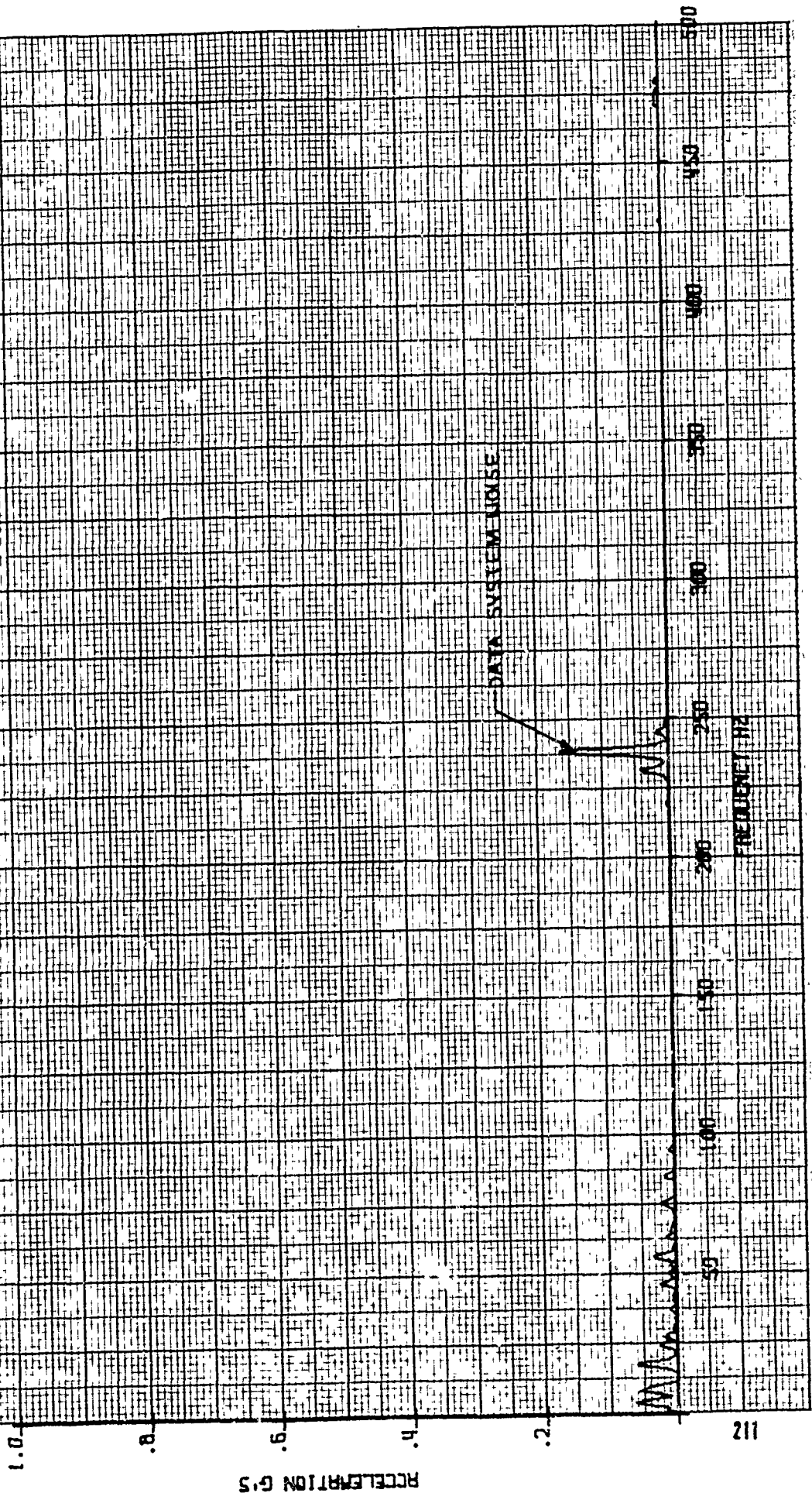
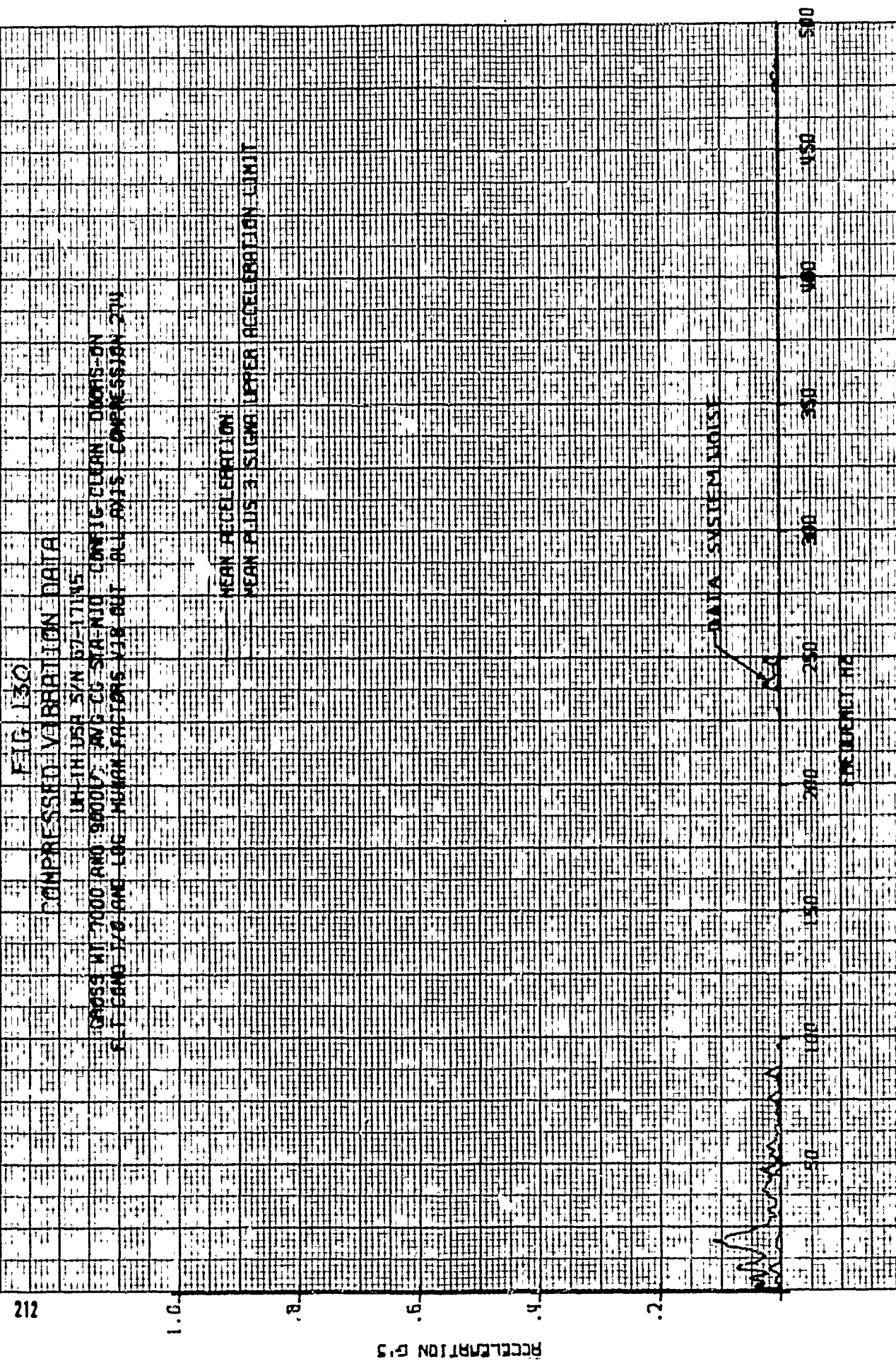


FIG 129

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UH-1H UH-1H UH-1H UH-1H UH-1H UH-1H UH-1H UH-1H UH-1H UH-1H
 GROSS WT 7000 AND 9000 LB AVG CL STA-N10 COMBIC-CLEAN DOORS-ON
 FLT EAND-085000 HEMON-FR-1005 VIB BUT ALL THIS COMPRESSION 273





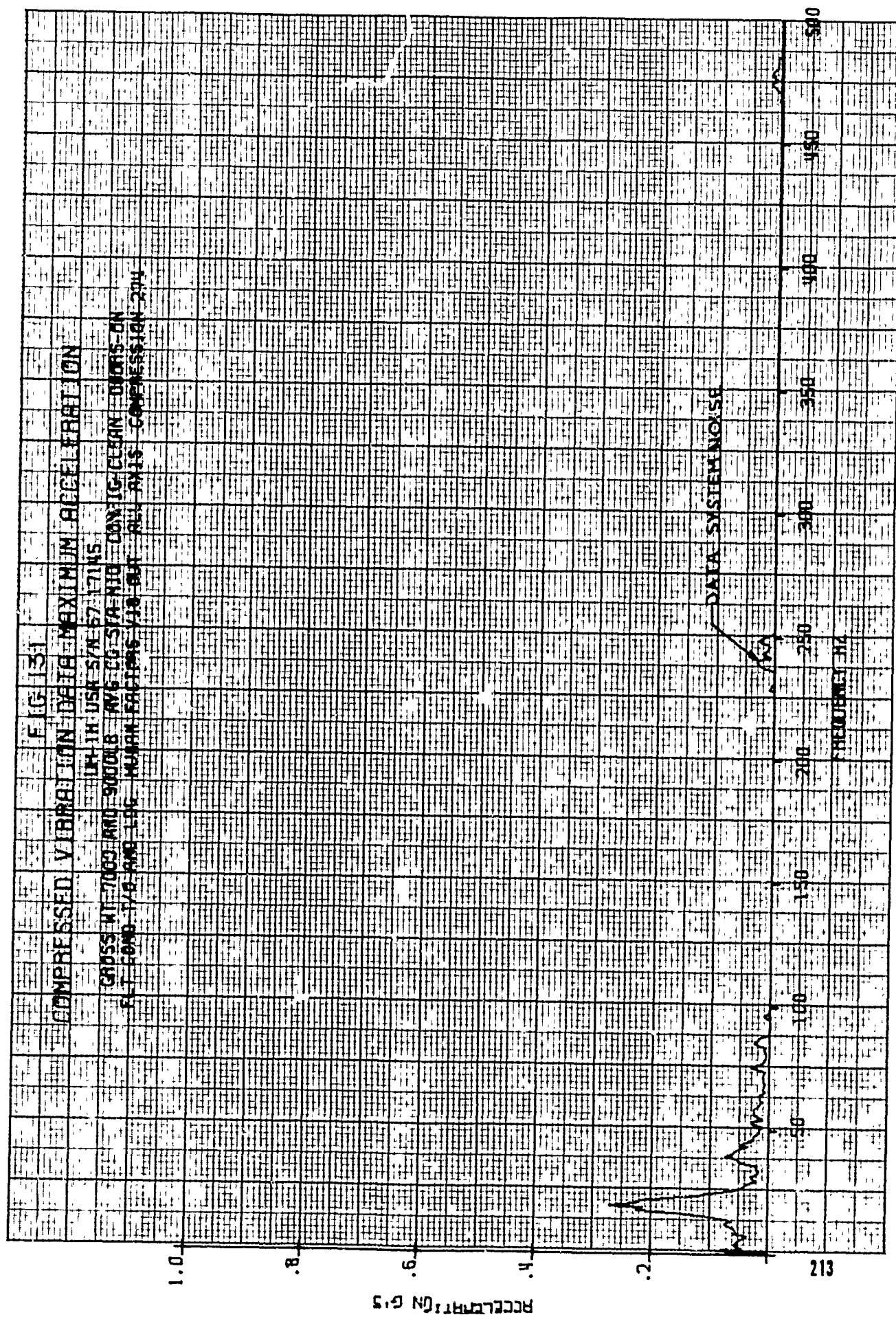


FIG 132

COMPRESSED VIBRATION DATA

UN-1H DSR 5/N 57-171NS
 GROSS WT 1000 AMO 9000LB AVG CG STA-M10 CONTIG-CLEAN UNDRS-ON
 5.1 CAND-NUMBERING HUMAN FACTOR VIB-DUT ALL AXIS COMPRESSION 275

MEAN ACCELERATION

MEAN PLUS 3 SIGMA UPPER ACCELERATION LIMIT

DATA SYSTEM NOISE

FREQUENCY HZ

ACCELERATION G'S

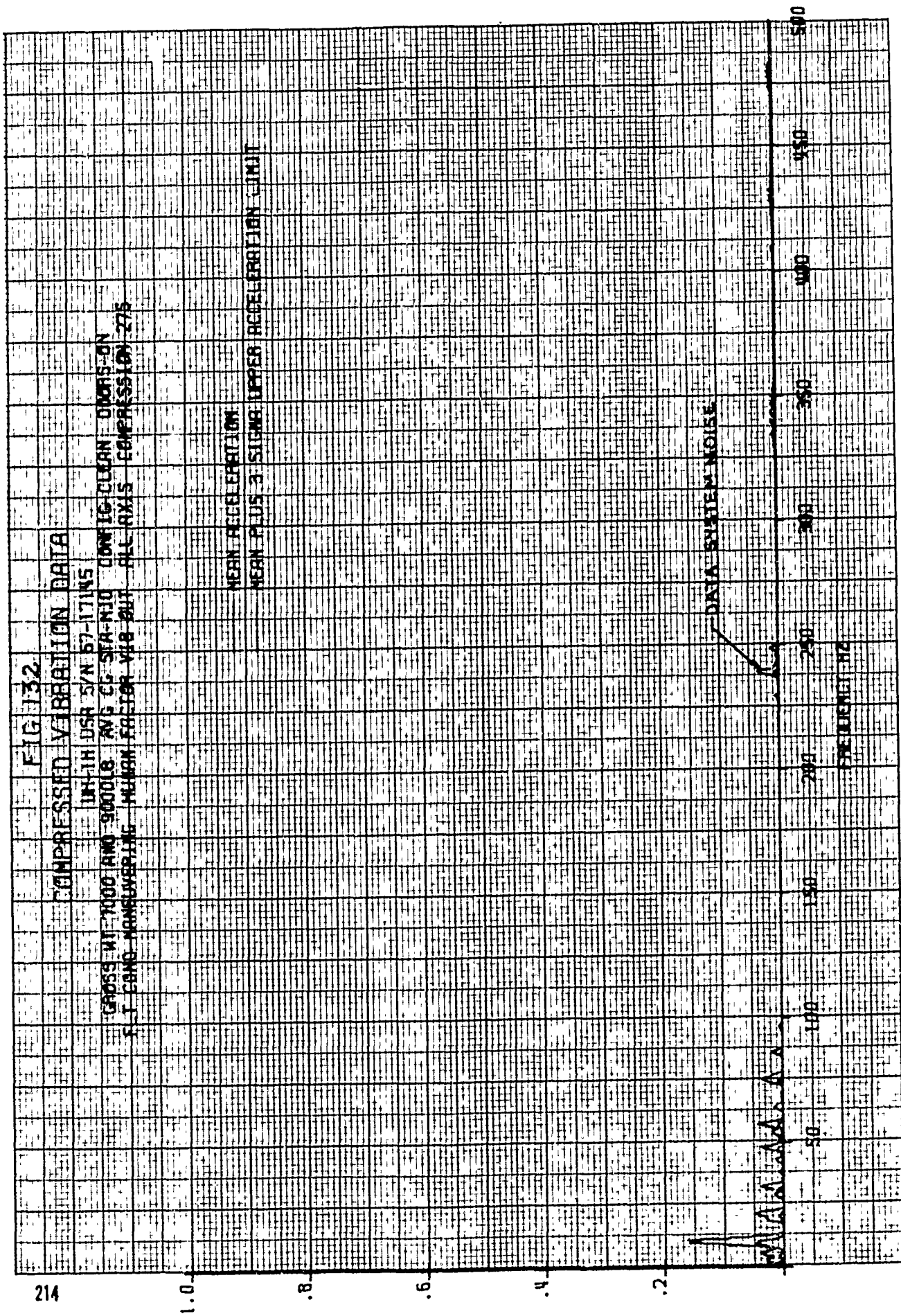
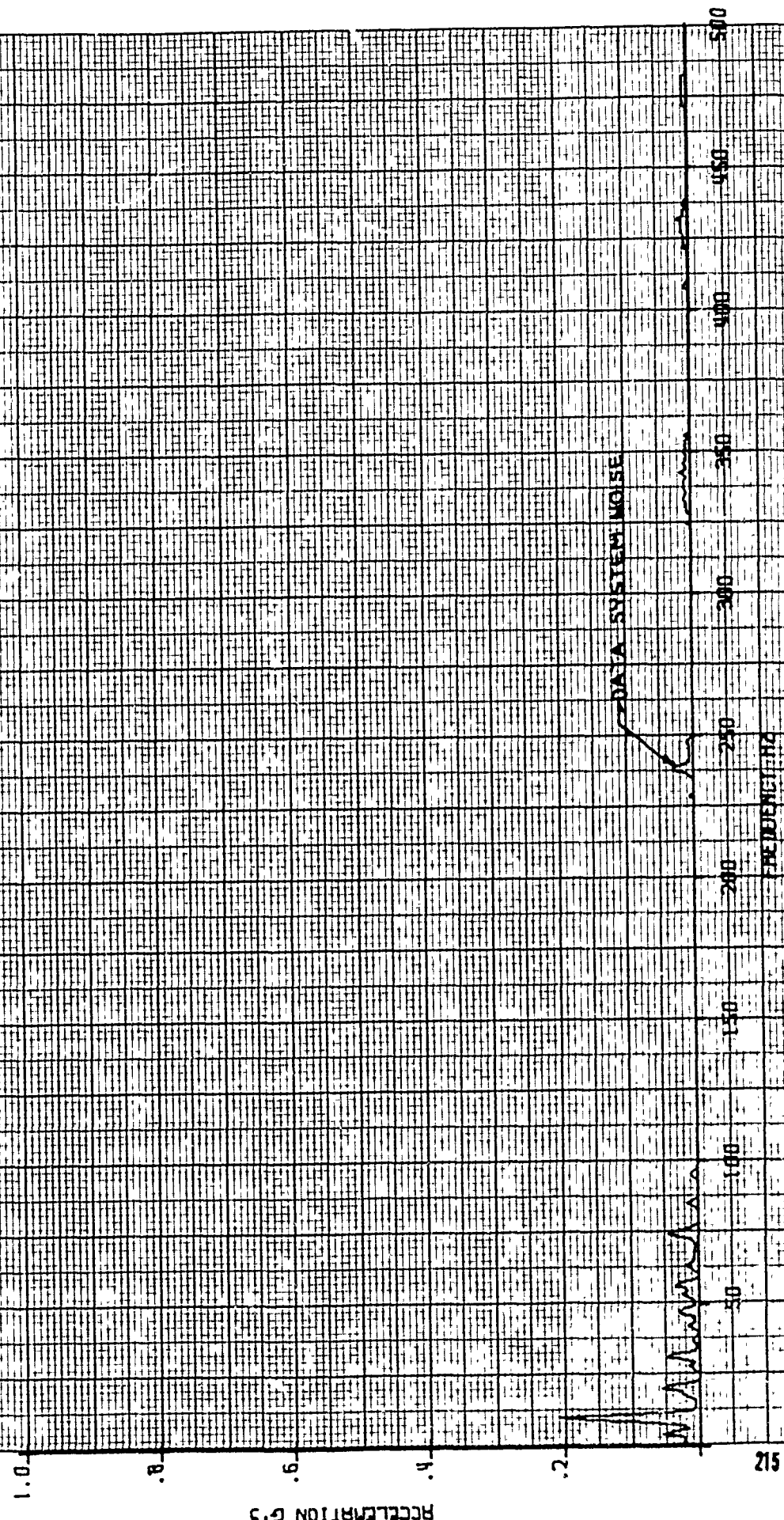


FIG. 133

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

UR-TH USR S/N: 57-17115
 GROSS WT 7000 LBS - 9000 LBS - AVG CG STA-1100 CONFIG CLEAN - OMARS-ON
 REF 1000 - NONOVERLAP - HUMAN FACTOR VIB-OUT REL AXIS COMPRESSION 275



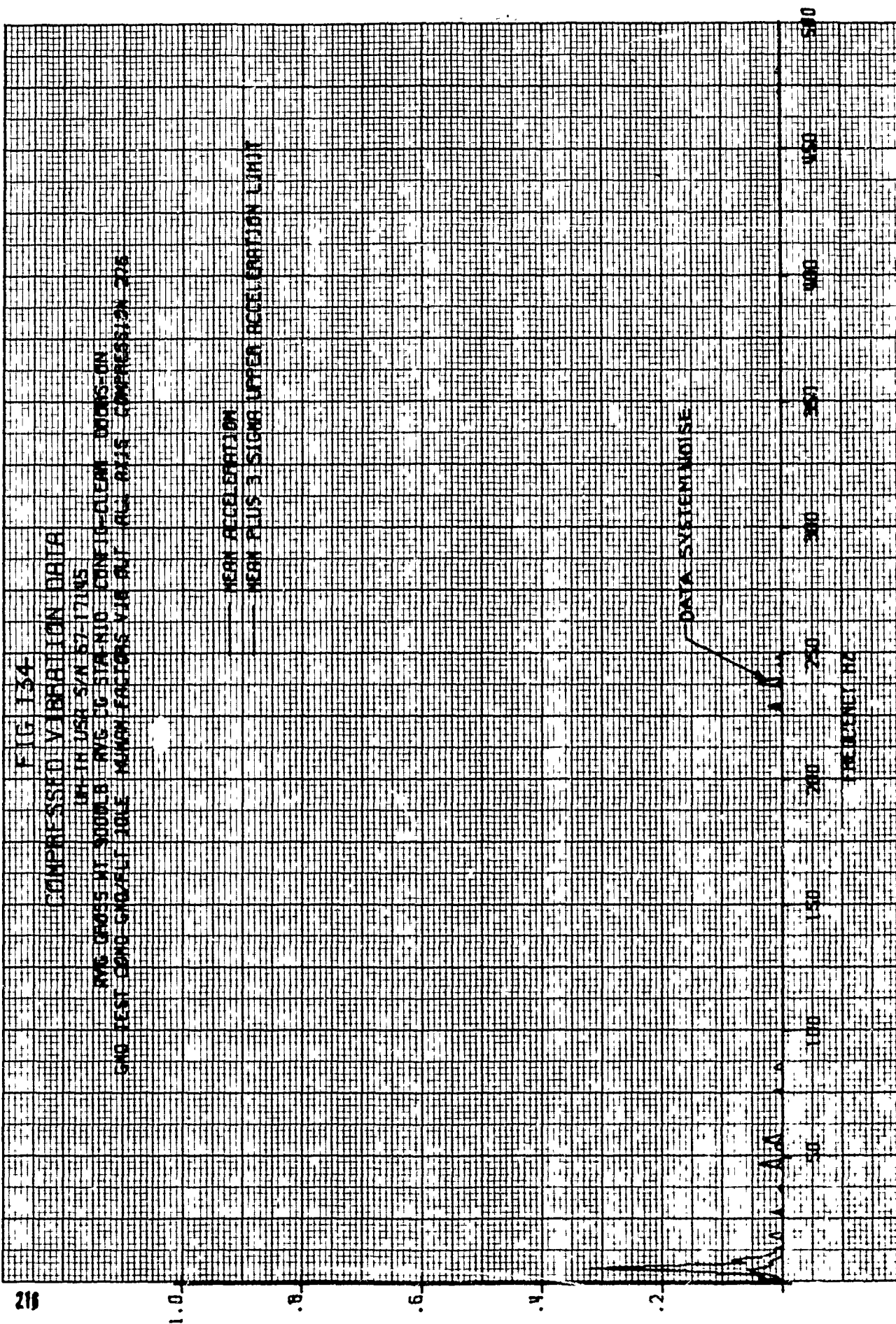


FIG 135

COMPRESSED VIBRATION DATA MAXIMUM ACCELERATION

LR IN USA S/N 57-171N5
 AVG 00019 WT 3000LB A/S CG STA N10 CONE ID-CLEAR BODIES ON
 GND TEST DASH 040/ALT 10LE MINION FACTORS VIB ALT ALL 0116 COMPRESSION 206

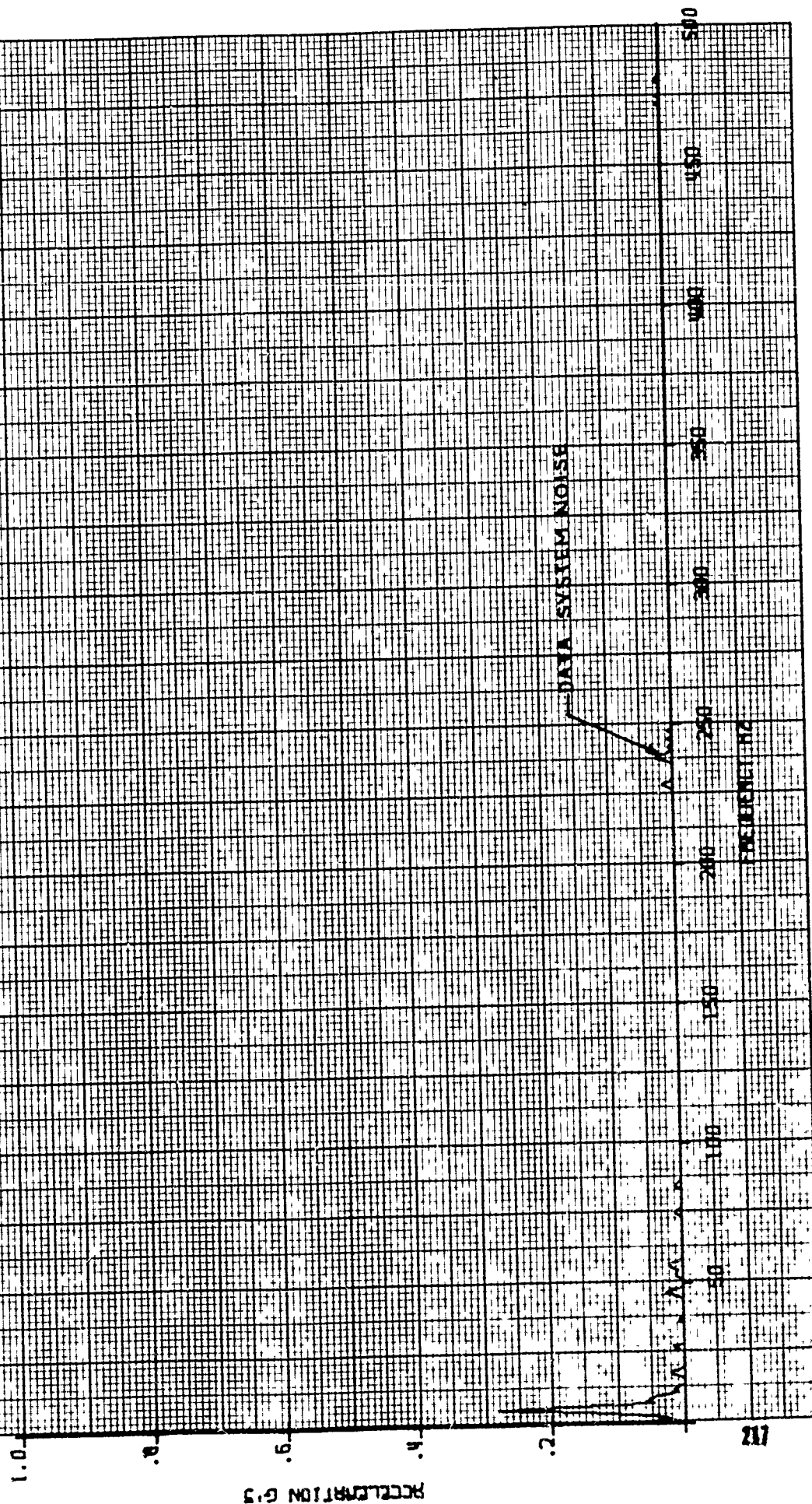


FIGURE 136
 STATIC INTERIOR TEMPERATURE
 ORTH USA 9467-11145
 FORWARD AVIONICS

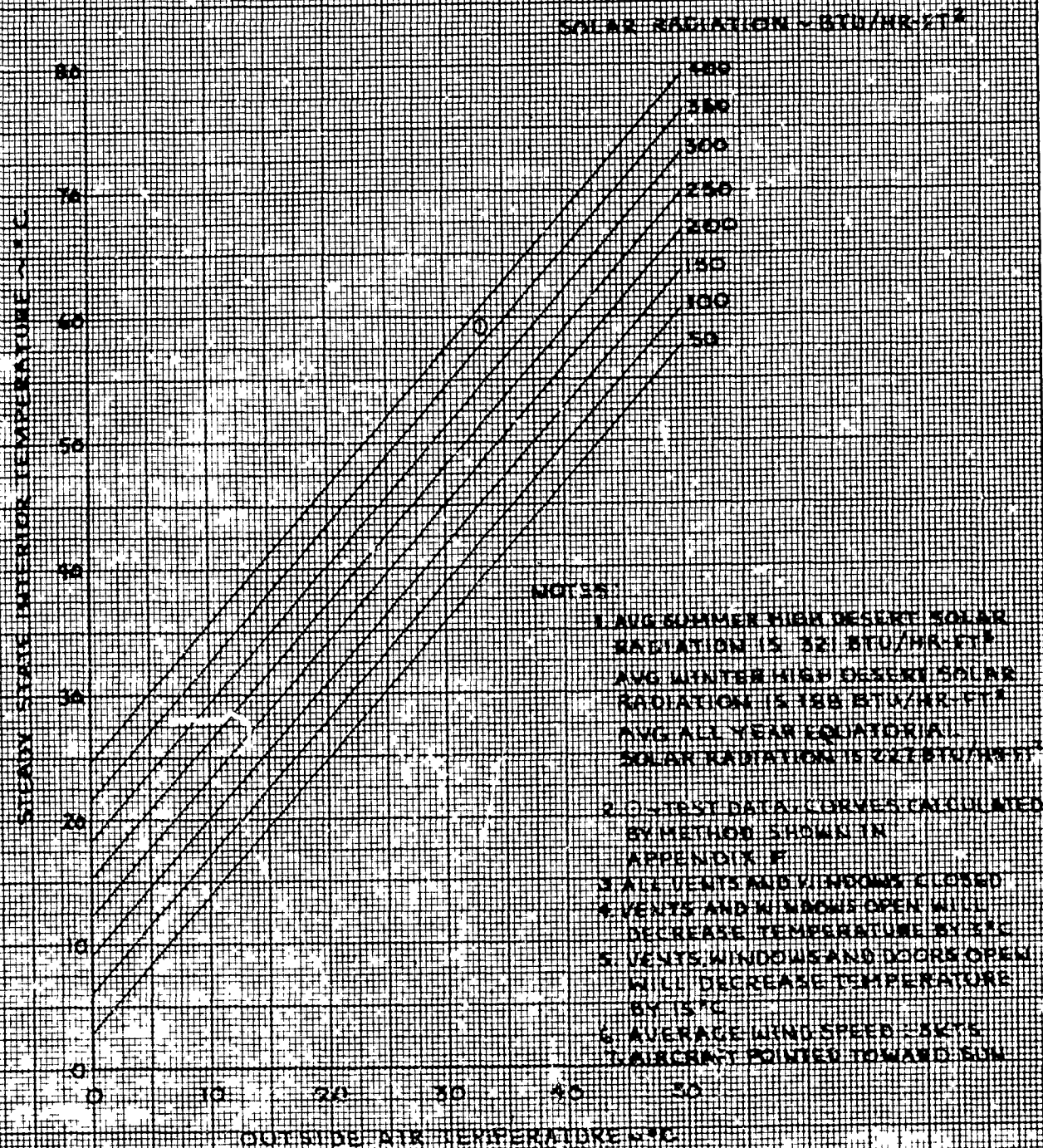


FIGURE 137
 STATIC INTERIOR TEMPERATURE
 OR-1A USA 367-11945
 FORWARD CABIN

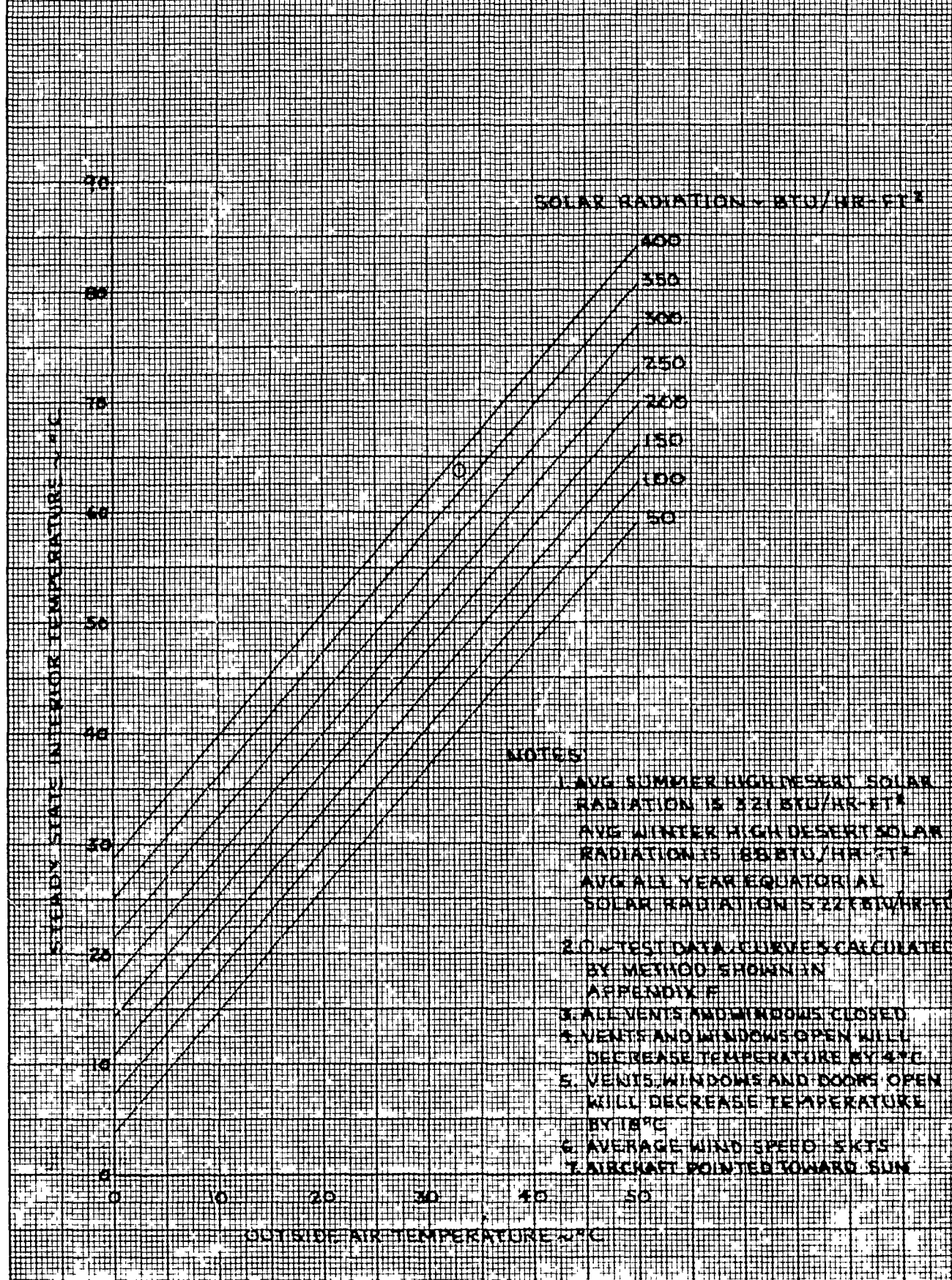


FIGURE 188
 STATIC INTERIOR TEMPERATURE
 ON-TH USA 3/67-17143
 APT CASIN

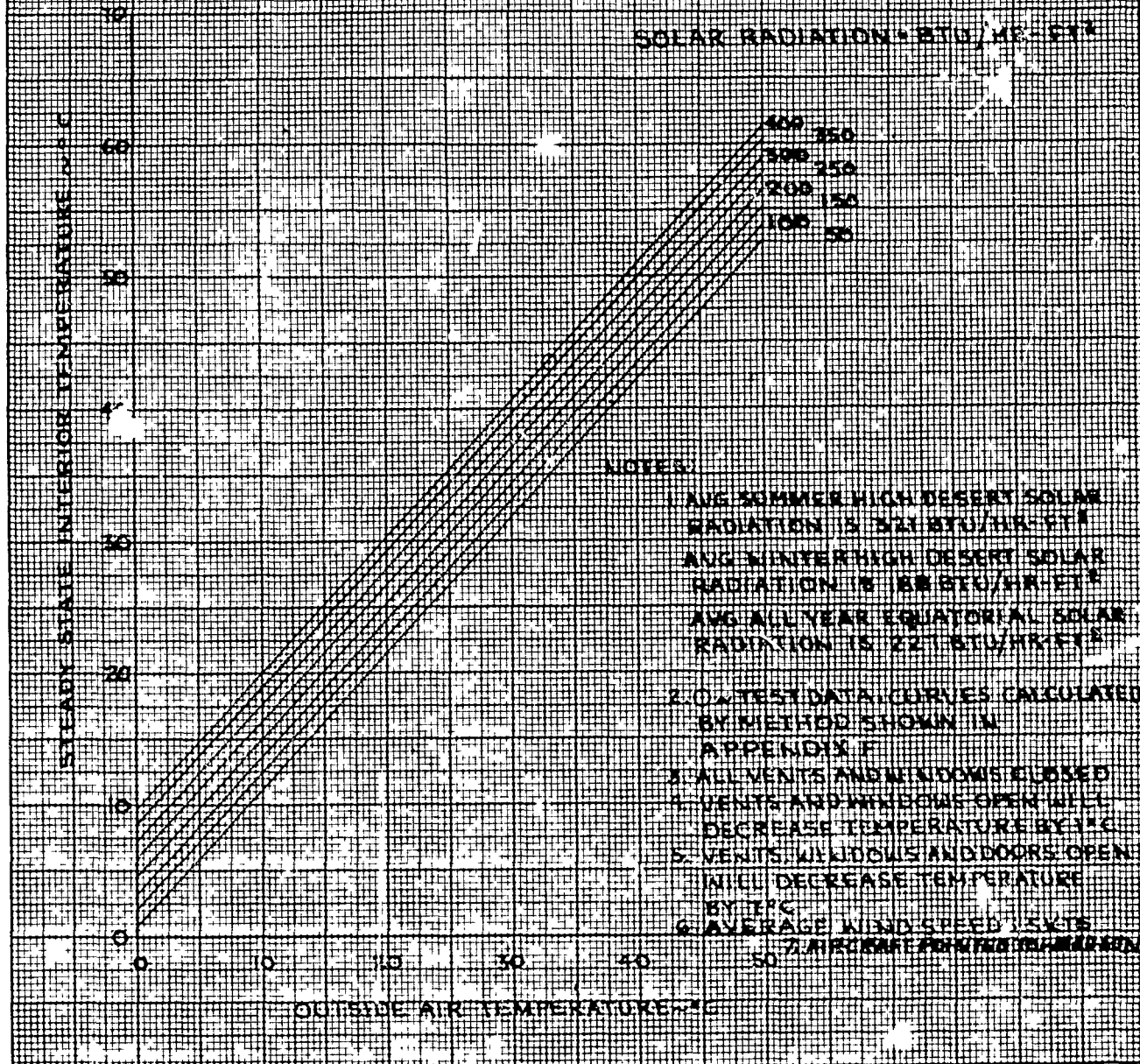


FIGURE 139
 STATIC INTERIOR TEMPERATURE
 ON-14 OSA MGT-17-45
 UPPER ENGINE COMPARTMENT

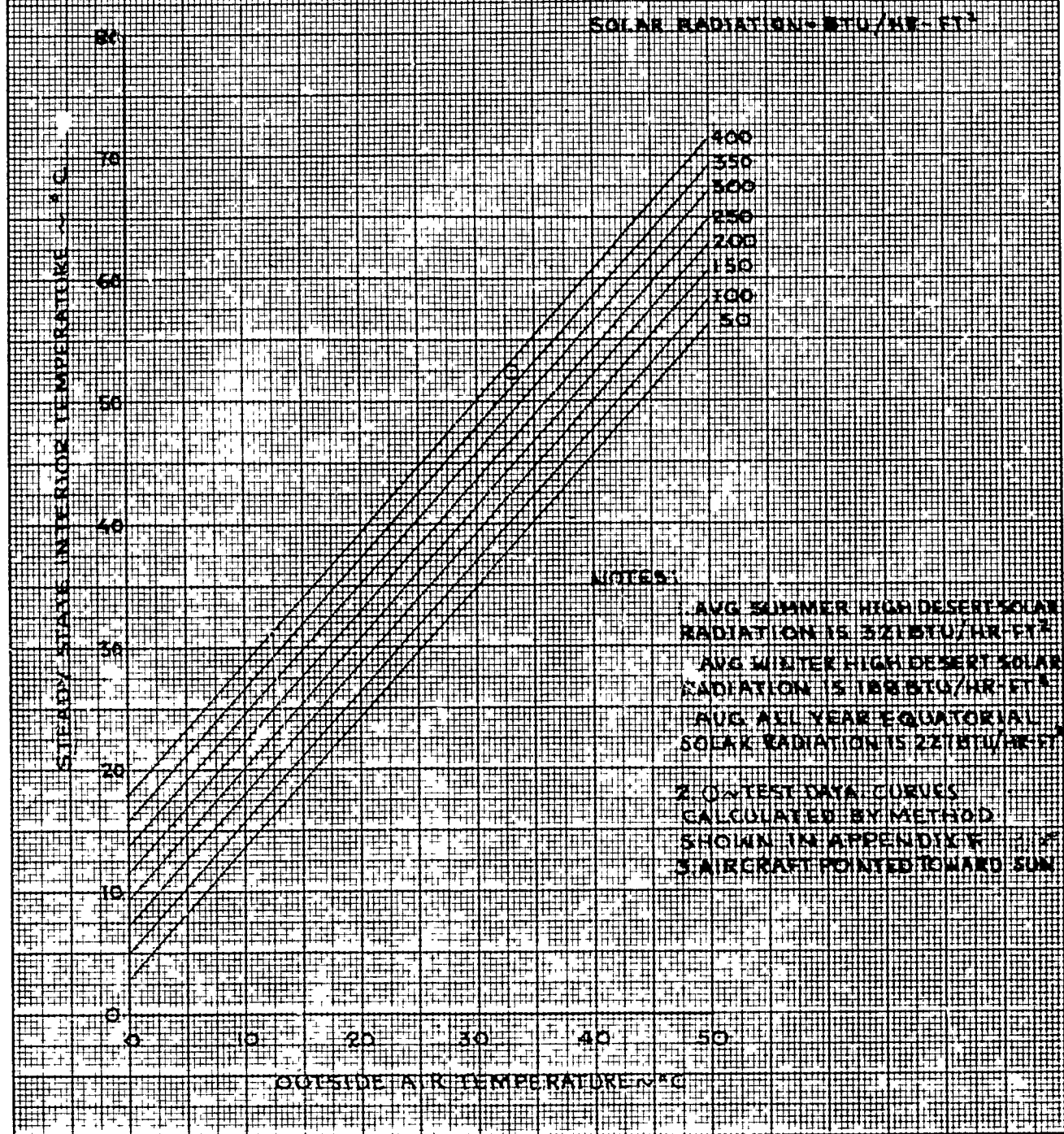


FIGURE 140
 STATIC INTERIOR TEMPERATURE
 DAH-1A USA 3467-17143
 42° CEARBOX

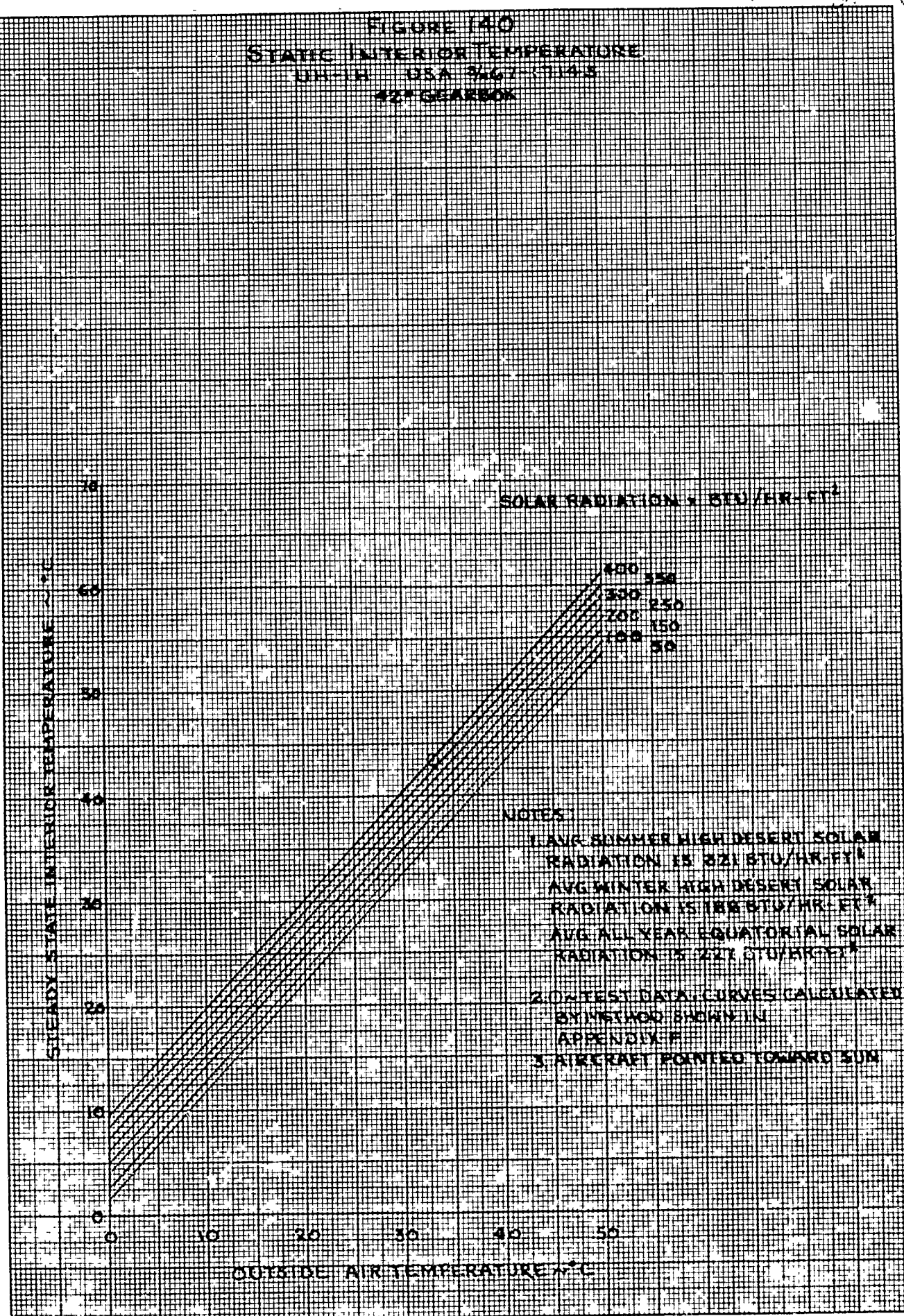


FIGURE 141
 STATIC INTERIOR TEMPERATURE
 GRAIN USA 3467-11145
 AIR HANGER BEARING

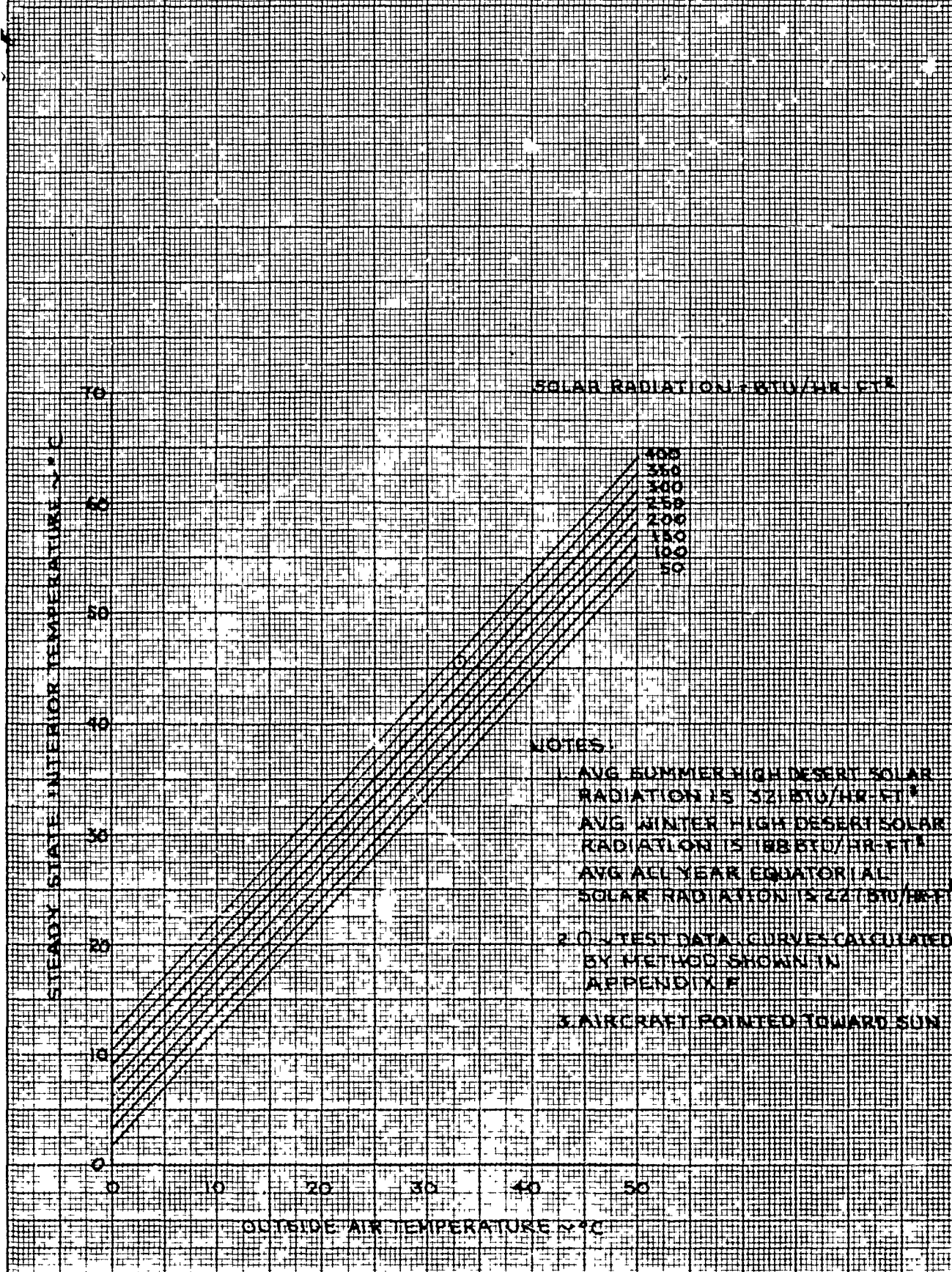


FIGURE 142
 STATIC INTERIOR TEMPERATURE
 OR IN USA NAVY-17145
 *Z HANGER BEARING

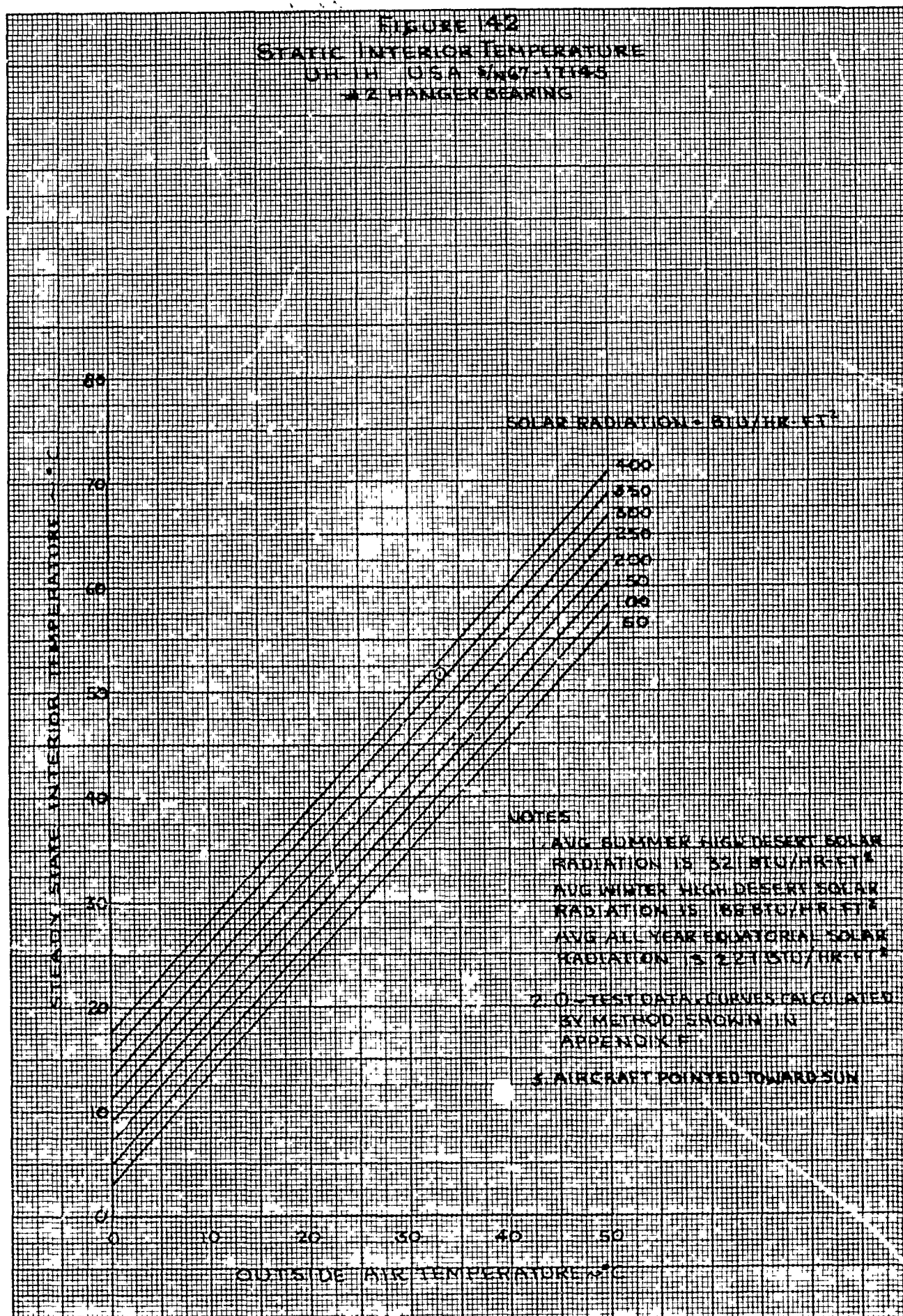


FIGURE 143
 STATIC INTERIOR TEMPERATURE
 ON-14 USA 5467-17145
 * 3 RANGER BEARING

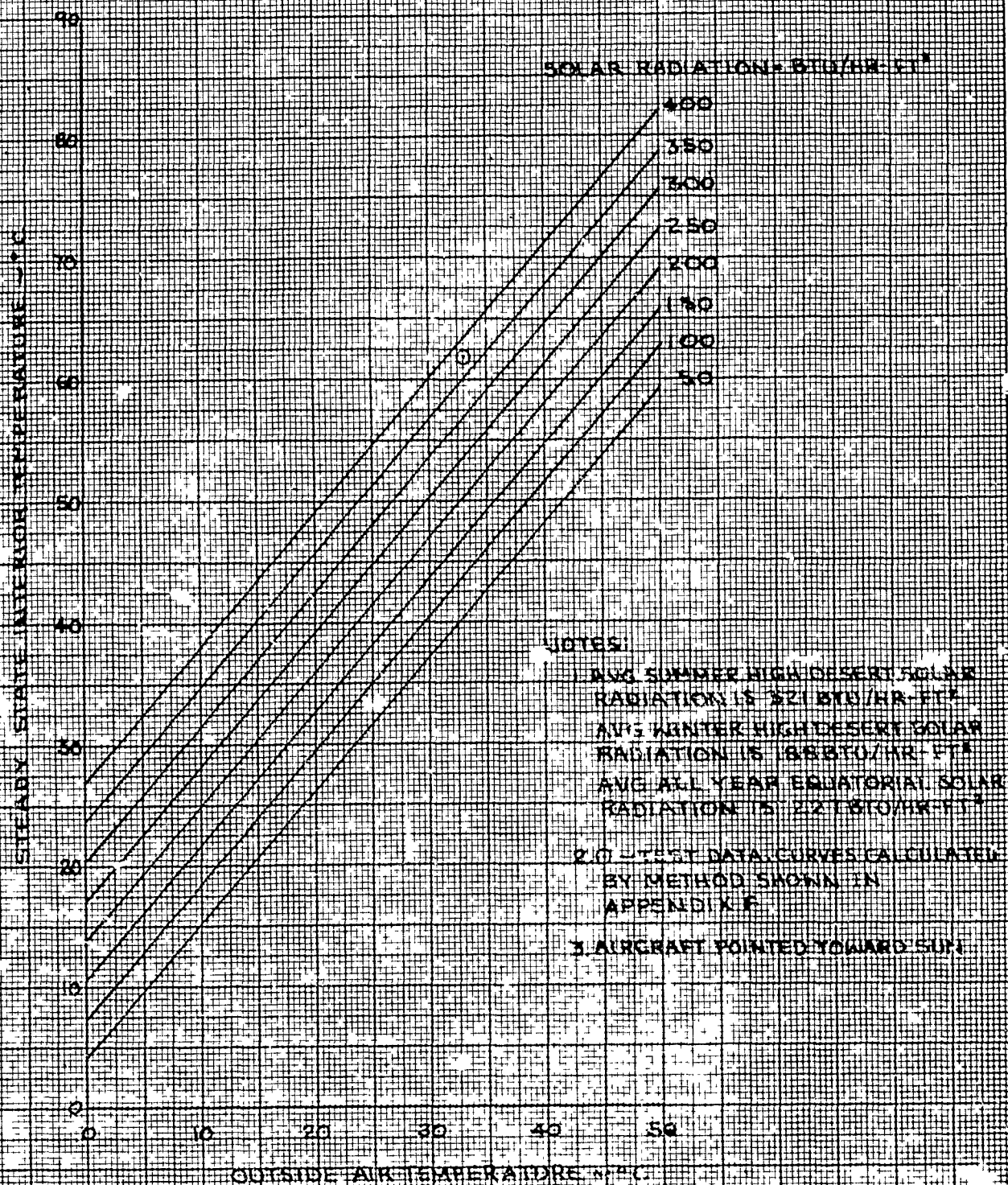
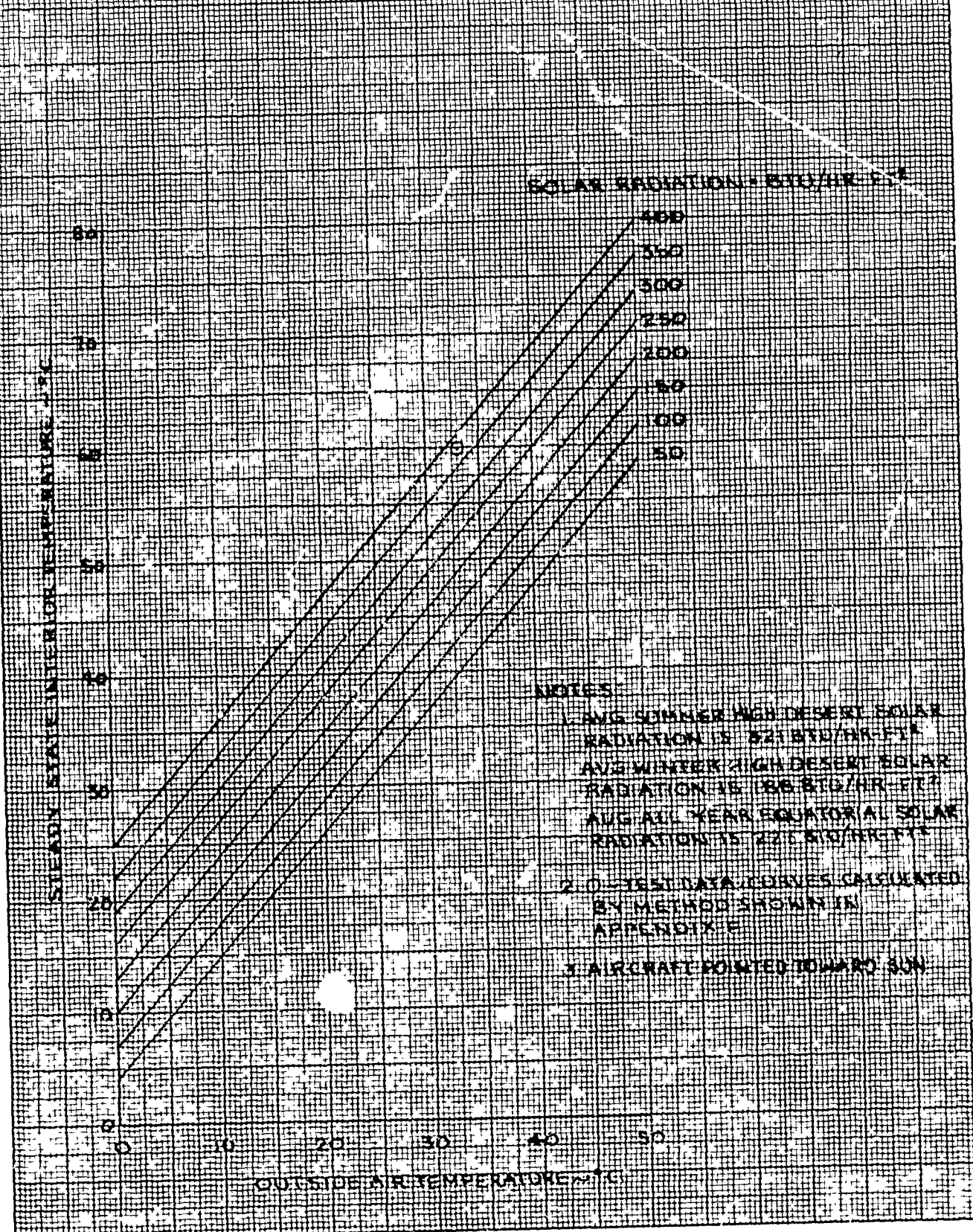


FIGURE 144
STEADY STATE INTERIOR TEMPERATURE
VS. OUTSIDE AIR TEMPERATURE
FOR A HANGER BEARING



NOTES

1. AVG SUMMER HIGH DESERT SOLAR RADIATION IS 521 BTU/HR-FT²
2. AVG WINTER HIGH DESERT SOLAR RADIATION IS 186 BTU/HR-FT²
3. AVG ALL YEAR EQUATORIAL SOLAR RADIATION IS 221 BTU/HR-FT²
4. TEST DATA CURVES CALCULATED BY METHOD SHOWN IN APPENDIX E
5. AIRCRAFT POINTED TOWARD SUN

APPENDIX H. HELICOPTER VIBRATION SOURCES

There are three primary sources of vibration in present-day gas turbine-powered helicopters: the main and tail rotors; all other rotating components; and, if the helicopter is armed, gunfire. The rotor induced vibrations are of a low frequency with the fundamental frequency equal to the rotor speed. In present-day helicopters, the main rotor speed ranges from about 3 to 8 Hz with the rotor speed generally decreasing with increasing rotor diameter. A vibration occurring at the main rotor fundamental frequency is referred to as the one-per-rotor-revolution (1/rev). The rotor also induces harmonic vibrations at frequencies which are integral multiples of the number of rotor blades multiplied by the fundamental rotational frequency. Thus, a two-bladed rotor with a fundamental frequency of 5 Hz induces vibrations at frequencies of 5 Hz (1/rev), 10 Hz (2/rev), 20 Hz (4/rev), 30 Hz (6/rev), etc., and a three-bladed rotor at frequencies of 5 Hz (1/rev), 15 Hz (3/rev), 30 Hz (6/rev), 45 Hz (9/rev), etc. Normally, main rotor induced vibrations beyond the 10th harmonic, 100 Hz for a two-bladed rotor, are not significant. Rotor induced vibrations at harmonics of the rotor fundamental frequency are the predominant helicopter low-frequency vibrations and are caused by dissymmetry of lift over the rotor disc which excite rotor blade structural modes and generally increase with airspeed. Vibrations are induced by all other rotating components in the helicopter. The frequencies range from the fundamental rotational frequency of the component up to geartooth, ball-bearing, and turbine-blade-passage frequencies which may range as high as 20 to 30 kilohertz. Gunfire induced vibrations are caused by recoil forces transmitted through the gun mount and by muzzle blast pressures. They have a fundamental frequency equal to the gun rate of fire and harmonics of this fundamental up to about the 20th harmonic. Typically, the highest vibration level will be at one of the gunfire harmonic frequencies. Fundamental gunfire frequencies range up to about 70 Hz.

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13. ABSTRACT		
<p>Vibration and temperature measurement tests were conducted on a production UH-1H helicopter to define the vibration and temperature environment for instruments, avionics, pilot station, and other component parts during firing and nonfiring flight. Testing was performed by the United States Army Aviation Systems Test Activity, Edwards Air Force Base, California, between 24 March and 16 June 1972. The testing consisted of 19 flights totaling 20 productive testing hours. Vibration data were recorded from 49 accelerometer locations for 55 flight conditions, and narrow-band spectral analyses were performed on the vibration data. The results of the spectral analyses were summarized by use of statistical methods. The primary source of low-frequency vibrations was the main rotor. Gunfire-induced vibrations were less than main rotor-induced vibrations. The highest vibration levels were recorded at the 42-degree gearbox at gear mesh frequencies. There were three shortcomings: amplification of main rotor-induced vibrations by avionics vibration isolation mounts, pilot station vibrations in excess of the military specification limits, and excessively high Wet Bulb Globe Temperature index at the pilot station under certain environmental conditions.</p>		

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Vibration and temperature measurement tests Production UH-1H helicopter Vibration and temperature environment for instruments, avionics, pilot station, and other component parts Firing and nonfiring flight Low-frequency vibrations Main rotor Highest vibration levels 42-degree gearbox						